AMENDED AND RESTATED NI 43-101 TECHNICAL REPORT ON THE VAREŠ MINE, BOSNIA AND HERZEGOVINA

Prepared for

Dundee Precious Metals Inc.

Effective Date: 1 April 2025
Issue Date: 9 June 2025

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Project Number: UK32167

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Amended and Restated NI 43-101 Technical Report on the Vareš Mine, Bosnia and Herzegovina

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Effective Date: 1 April 2025
Issue Date: 9 June 2025

Project Number: UK32167

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Amended and Restated NI 43-101 Technical Report on the Vareš Mine, Bosnia and Herzegovina

ITEM 1. SUMMARY

1.1 Introduction

SRK Consulting (UK) Limited compiled this Amended and Restated NI 43-101 Technical Report (the Technical Report) on the Vareš polymetallic mine (the Vareš Mine or Mineral Property), located in Bosnia and Herzegovina. For reference, the initially issued NI 43-101 Technical Report, has been updated to reflect the change of QP in respect of underground geotechnics from Michael di Giovinazzo to Neil Marshall, and the removal of revenue associated with a minor amount of Inferred Mineral Resource being present in a few mining blocks.

The Vareš Mine is currently under the ownership of Adriatic Metal Plc (ADT) through its wholly owned subsidiary Adriatic Metals BH d.o.o. ADT completed construction of the process plant and most mine infrastructure in 2023. Underground development to access the Rupice deposit commenced 2023, with first ore mined in February 2024. First production of two concentrates for silver, zinc, gold, lead and copper (in order of revenue generation) took place in May 2024.

The Technical Report was prepared for Dundee Precious Metals Inc (DPM) in connection with DPM's proposed acquisition of all of the shares of ADT (the Transaction).

1.2 Setting

The Vareš Mine is located approximately 50 km from the capital city of Sarajevo. The closest town is Vareš, located between the Rupice Mine (8.5 km north-west) and Vareš Processing Plant (VPP) (3 km east).

The Vareš Mine is situated within the Bosnia autonomous entity, and wholly within the Zanica-Doboj Canton and Vareš Municipality. The western boundary of the mineral concession is adjacent to the boundary with Kakanj Municipality.

The Vareš Mine is in a single concession comprising three separate licence areas; one at Rupice in the west and two at Veovaca in the east. Subsequent to the original concession being granted, the concession was extended increasing the overall project area to 869.3 ha.

1.3 History

Early reports dated 1870-1886 from the Austrian- Hungarian occupation refer to the lead-zinc deposits. Significant exploration commenced after 1945; and modern systematic exploration started in the early 1960s through Energoinvest. Detailed exploration at Rupice itself commenced in the 1960s through development of exploration adits and drives followed by a substantial program of trenching and diamond core drilling in the 1980s. ADT has undertaken various drilling campaigns since 2017.

The Vareš Mine was officially opened on 5 March 2024. Underground development commenced in 2023 with some 1.5 km developed and an additional 3 km developed in 2024, to provide access to the deposit. First ore from development was processed in May 2024, with the first stope opened up in August 2024.

The first sale of on-specification grade concentrates was in May 2024, via the port of Ploče. Concentrates have been sold and shipped to European smelters and beyond. Production ramp up with commercial production and nameplate capacity is expected in 2025.

A total of 146 kt of ore was mined in 2024, with 76 kt processed, producing 5.5 kt of Ag/Pb concentrate and 7.1 kt of Zn concentrate. No Q1 2025 production statistics were available at the time of writing, apart from a total of 67 kt ore mined, and 66 kt processed.

1.4 Geological Setting, Mineralization and Deposit Type

The geological setting is a very large-scale deformation belt within which Jurassic, Triassic packages dominated by carbonates and volcano-sedimentary shelf sediment have been thrusted and folded. At Rupice, the Triassic sequence contains layers of iron alteration and one layer in which massive sulphide mineralisation was deposited.

Genetically, the deposit is associated with a shelf zone where volcanic activity generated hydrothermal processes that allowed the scavenging of metals from surrounding crustal material and delivery of this into the submarine environment resulting in formation of a Volcanogenic Massive Sulphide (VMS) deposit with associated breccia-hosted mineralisation.

Base metal massive sulphides were originally deposited in a single layer of lenses which were conformable with the enclosing bedding.

1.5 Exploration and Exploration Potential

Early reports dated 1870-1886 from the Austrian- Hungarian occupation refer to the lead-zinc deposits. General descriptions of the geological structure and mineralization are variously reported in publications dated between 1900 and 1929. Mining is generally understood to have taken place in the area historically.

Significant exploration commenced after 1945; and modern systematic exploration started in the early 1960s. Detailed exploration at Rupice itself commenced in the 1960s through development of exploration adits and drives followed by a substantial program of trenching and diamond core drilling in the 1980s.

The main potential is to extend the Rupice deposit to the northwest where it is open at depth. However, this will require drilling to be done from ground where ADT did not yet have an exploration permit. Furthermore, this is in a different municipality from the current concession areas, which may require different stakeholder engagement and government royalties to proceed with exploration.

There are four main areas of exploration for which USD 5 million is budgeted by DPM to be spent in 2025. This will mainly be for scout drilling of clear geophysical and geochemical anomalies. The QP considers there is merit in covering all of the concession areas with an appropriate airflown remote sensing method.

1.6 Drilling

Drilling at Rupice commenced in the 1980, with a number of subsequent drilling programmes notably since ADT acquired the asset. The current estimate includes underground grade control diamond drilling and surface infill, step-out and twin verification diamond drillholes up to September 2024 (excluding 8 drillholes completed in November 2024 for which assay results were pending at the time of populating the block model).

The QP assessed that the drill spacing and core recovery were satisfactory.

1.7 Sampling, Analysis and Data Verification

Data Quantity and Quality

The model is supported by diamond drillholes, mostly from surface, over 90% of which has been drilled by ADT who reported very good core recovery as observed by the QP in the core shed. The Mineral Resource estimate is based on drilling completed up to September 2024. Drilling intersects the mineralisation with a spacing of 25 m to 30 m on section lines spaced 40 m apart. Where there is apparent structural influence on mineralisation, drillhole intersection spacings were decreased to 20 m.

There is a good quality logging and storage facility used by the geology team, logging is suitably detailed and makes use of a core refence library which allows consist simple lithology codes to be used. Densities are determined for samples taken from every core box using an industry standard method. Densities were related to assays using regression equations which the QP checked in some detail using an alternative robust approach.

A number of sample preparation and assay laboratories have been used since ADT started drilling in 2017, which are run by recognised independent international companies and are accredited. A number of different digest and analysing methods have been used to appropriately cater for the variety of minerals in the deposit and the ranges of the elemental grades. ADT has had in place a rigorous QAQC programme which demonstrates the quality and reliability of the sampling and assaying used in the model.

Geological and Grade Model

The Rupice deposit is located in the Dinarides deformation belt which runs through the Balkans, parallel to the Adriatic coast. The limestones, dolomites and volcano-sedimentary sequences hosting the Rupice deposit are folded and faulted by thrusts and intermediate ramps.

The deposit is a volcanogenic massive sulphide lens comprising mainly galena, sphalerite, chalcopyrite, pyrite and tetrahedrite overlain by a barite layer which, after folding, has undergone a certain amount of recrystallisation and remobilisation of the minerals of interest.

The block model is based on 3D geological wireframes, which generally have a folded lensoid shape reflecting the pinch and swell features to be expected in this environment and observed underground. The main part of the model has generally good continuity. There are several hangingwall and footwall features which are typically less continuous.

Grade estimation domains were generated for each metal of interest and the grade estimation itself involved industry standard methods, including statistical and geostatistical analysis, grade capping, and used ordinary kriging in variably orientated search ellipses to estimate block grade values. The resultant grade was checked visually, statistically and using swath plots.

The QP reviewed ADT's 3D block model and found it to be fit for the purposes of reporting Mineral Resources and supporting the mine plan. Nevertheless, The QP made some recommendations to tidy up wireframing complexity, improve wireframe continuity in places, implement grade estimation normalisation, enhance density estimation, and implement density weighting in the grade estimation method.

Classification

The drilling coverage is comprehensive in most parts of the model which allows for reasonable confidence to be had in the location, geometry and continuity of the 3D model. Combined with the confidence demonstrated in the sampling data, this allows an Indicated classification to be conferred to the majority of the Mineral Resource, with some less well drilled and isolated areas being appropriately classified as Inferred.

Mineral Resource Reporting

The RPEEE for the MRE statement is based on the positive cash flow model, which used the technical and economic parameters described in this report. The cash flow model was used to determine overall net revenue factors applicable to each of the revenue deriving metals, which were applied to the respective metal content in each block and multiplied by the respective metal prices.

The metal prices used are the same as those in the cash flow model except that, for the purposes of reporting Mineral Resources, a premium of some 25-30% was applied in line with common industry practice. A cut-off value of USD 100/t was used, reflecting mine site operating costs as represented in the cash flow model.

ADT's block model was depleted to 31 December 2024. The QP further depleted the model to 1 April 2025 using the Q1 2025 production tonnage and estimated grades. No stockpiles were included in the QP's MRE. These are not expected to contain a material quantum of ore.

The Mineral Resource statement is presented in Item 1.9.

1.8 Mineral Processing and Metallurgical Testing

Testwork programs in support of the development of the Vareš Mine were undertaken in three campaigns at the laboratory of Wardell Armstrong International (WAI) in Cornwall, UK: Preliminary (2019), PFS (2020) and DFS (2021), at a range of sample and composite grades.

The testwork relating to comminution and flotation is of sufficient breadth and depth to inform a Feasibility Study level of project definition, leading into detailed design and construction. However, for other aspects, notably dewatering (thickening and filtration), testwork was conducted on only one sample in each case (i.e. both concentrates and the flotation tailings) – this represents a risk to the robustness of the ensuing plant design and operation.

Recovery relationships were developed by Ausenco during the PFS, based on the PFS locked cycle test results. These equations were not updated to include the DFS testwork results, due to time constraints during finalisation of the DFS. Comparing the grades and recoveries using these equations for all of the published LCT results indicates that the equations developed based on the PFS testwork results are consistent with the DFS testwork results.

1.9 Mineral Resource and Mineral Reserve Estimates

The Mineral Resources and Mineral Reserves were reported in accordance with the CIM Definition Standards on Mineral Resources and Reserves and National Instrument 43-101.

Mineral Resource Statement

The Rupice Mineral Resource Statement is dated 1 April 2025. The Indicated Mineral Resources stated are inclusive of those modified to produce the Mineral Reserve.

Those Indicated Mineral Resources that were not modified to produce the Mineral Reserve do not have demonstrated economic viability. There is no guarantee that further work will be able to increase confidence of the Inferred Mineral Resource to Indicated Mineral Resource.

Table 1-1 provides the QP's Rupice Mineral Resource statement, reported above a cut-off MRE_NSR value of USD 100/t. It is a direct report from the ADT block model without consideration of mining shape optimisation. The MRE_NSR value resulting from the average metal grades in the MRE (approximately USD 540/t above a cut-off value of USD 100/t).

Table 1-1: Rupice Mineral Resource Statement – 1 April 2025

Mineral Resource	Tonnage (Mt)	Ag (g/t)	Zn (%)	Pb (%)	Au (g/t)	Cu (%)	Sb (%)
Indicated	10.7	264	7.4	4.8	1.9	0.65	0.22
Inferred	0.9	150	3.5	2.8	0.8	0.37	0.15
Rupice Mineral Resource Accompanying Notes							

Basis of Mineral Resource estimation

- The QP responsible for the Mineral Resources is listed in Item 2.2.
- The stated Indicated Mineral Resources are inclusive of those Indicated Mineral Resources that have been modified to produce the Mineral Reserves.
- Indicated and Inferred Mineral Resources are not added and presented as a total, following the CIM Definition Standards.
- The Mineral Resources are reported above a cut-off MRE_NSR value of USD 100t. It is a direct report from the ADT block model without consideration of mining shape optimisation. The MRE_NSR value resulting from the average metal grades in the MRE (approximately USD 540/t above a cut-off value of USD 100/t).
- The Mineral Resources are reported on the basis that they are planned to be mined via long hole open stoping, processed via a known demonstrated process route, and sales concentrate delivered to market. At presented this is supported by technical studies perceived to be at PFS or FS level of confidence. Risks associated with the technical feasibility and economic viability of extraction remain, relating to unknowns, though these are greatly reduced as mining has commenced, the process plant has been commissioned, and early concentrate sales have taken place, thereby shedding light on numerous previous unknows have now been identified and are being addressed.
- Mineral Resources may further be materially affected by any known environmental, permitting, legal, title, taxation, socio-economic, marketing, political, or other relevant factors.

Mineral Reserve Statement

The Rupice Mineral Reserve Statement and Accompanying Notes dated 1 April 2025 are presented in Table 1-2. The QPs deem the level of confidence supporting the Mineral Reserve to be at pre-feasibility, with some components at feasibility level. Whereas pre-feasibility is a lower confidence level of study than the DFS issued in 2021, DPM now has the benefit of construction and initial production having identified a number of unknowns, which are being addressed.

Table 1-2: Rupice Mineral Reserve Statement – 1 April 2025

Mineral Reserve	Tonnage (Mt)	Ag (g/t)	Zn (%)	Pb (%)	Au (g/t)	Cu (%)	Sb (%)
Proved	-	-	-	-	-	-	-
Probable	9.5	228	6.8	4.3	1.7	0.57	0.18
Total	9.5	228	6.8	4.3	1.7	0.57	0.18
Rupice Mineral Reserve Accompanying Notes							

Basis of Mineral Reserve estimation

- The QPs responsible for the Mineral Reserve are listed in Item 2.2.
- The Mineral Reserves were derived from the Mineral Resources dated 1 April 2025, presented in Table 14-7.
- The entire Indicated Mineral Resource was considered for the Mineral Reserve. Therefore, the only opportunity to increase the Mineral Reserve is to increase the Indicated Mineral Resource through upgrading of Inferred to Indicated or further exploration.
- To enable the depletion of the Mineral Reserve to the date of 1 April 2025, the QP used the Q1 2025 production tonnage and estimated grades. Actual production will differ, which is not deemed material to the Mineral Reserve Statement. No stockpiles were included.

- The Mineral Reserve is reported on a 100% attributable basis. The QP notes that a local DPM subsidiary company remains to be setup and transfer of the concessions and licences to such company is yet to be undertaken.

Hydrogeology

- There are gaps in the hydrogeological understanding that present a risk to mine production and project costs, if dewatering inflows exceed currently planned capacity. Additional drilling and testwork is required to manage these risks.

Geotechnics

- As ADT advanced underground development and stoping, the geotechnical conditions are now better understood. Whereas the ore is mostly competent rock, the waste rock is variable with some weak to very weak zones. ADT has put much effort into improving ground support and demonstrated that this can be adequately managed. The QP considers that the measures put in place by the mine operations team to deal with the geotechnical challenges are appropriate and conform to industry best practice. The impact on cost has been material / significant and is included in the economic analysis. DPM intends to further change the mining method, which the QP expects to have a positive impact.

Mining

- The mining method and design is expected to change under DPM ownership, from longhole open-stopes mined underhand, downwards, from upper levels, to longhole open-stopes mined overhand, upwards, from lower levels. Some mechanised cut-and-fill stoping will also be introduced. The QP deems that the mine plan generated by DPM is achievable and meets a pre-feasibility level of confidence as a result of the designs and scheduling being preliminary, and cost estimation limited. The QP notes that the geometry of the deposit and applicable mining method result in a mine plan that will require fine attention to multiple well sequenced activities.
- Modifying factors for unplanned dilution and loss (external to stope shapes) were determined for each stoping type and average 12.5% and 6.5% respectively.
- NSR cut-off grades of USD100/t for longhole open stopes and USD120/t for mechanised cut-and-fill stopes were used to select designs for inclusion in the Mineral Reserve. The long term commodity prices applied in the estimation of the Mineral Reserve are: zinc USD 2,661/t, lead USD 2,064/t, copper USD 9,348/t, gold USD 2,212/oz, and silver USD 28/oz. In order of priority, revenue is generated from silver, zinc, followed by lead and gold, and minor contributors from copper and antimony.
- The QP notes that the projected steady state ore treatment rate is 850 ktpa, with no planned expansion. Underground development for the change in mining methods is yet to commence. To steadily ramp up to full production, stoping activities and production rate are dependent upon the permitting and commissioning of the paste backfill plant. Delays in permitting of the paste backfill plant remain a key risk and will have a direct impact on production.

Processing

- The process plant flowsheet as built is consistent with the design as per the DFS. The recovery relationships used in the NSR calculation were derived from the PFS testwork. However, the subsequent DFS testwork results were consistent with these relationships. Ramp up to full steady state production was not yet achieved. The metal recoveries are well supported by test work. However, actual metal recoveries are not yet known with confidence, and meaningful reconciliation is some time away.

Tailings Management

- The Veovaca TSF is being constructed within the historic Veovaca open pit and is designed as a filtered stack to store tailings not required for stope backfilling. The tailings have been classified as potentially acid-forming, with the potential to leach metals and sulphides if exposed to atmospheric conditions. To mitigate environmental risks, the TSF is lined to prevent groundwater contamination, and contact water will be collected in a catchment pond and reused in the VPP. Progressive closure of the TSF involves capping it with an impermeable clay layer, waste rock and topsoil to promote natural vegetation growth. Prior to the completion of the Veovaca TSF, a temporary lined TSF was developed north of the VPP to accommodate tailings during initial mining operations. Once the Veovaca TSF is operational, the tailings from the temporary facility will be relocated to the Veovaca TSF.

Water Management

- The water treatment and sediment management capacity is being increased. The surface water management at the mine site is being changed and will be able to inform a more robust water balance that incorporates aspects like climate change.

Infrastructure

- The mine infrastructure is mostly built.
- The haul road to transport tailings needs to be built as the temporary road could only be used until 2 June 2025.

Processing

- An understanding of waste rock geochemistry is available through previous testwork but the waste management strategy needs to be re-visited for the revised LoM plan by DPM.

Permitting

- There are uncertainties relating to the status of permitting and compliance. DPM is an operator in the Balkans and is focused on putting commensurate effort to address permitting shortcomings in collaboration with the appropriate regulatory authorities.

Costs

- Initial capital costs amounting to USD 76 million and sustaining capital costs amounting to USD 133 million were projected (excluding USD 24 million as a closure cost allowance), along with life of mine operating costs totalling USD 1,050 million.

Economics

- The economic analysis undertaken results in a positive NPV of USD 1,608 million at a discount rate of 5%.

Integration Plan

- DPM is developing an Integration Plan as part of DPM taking over ownership and operation of the Vareš Mine. This is a short term plan, which will be deployed until the point at which the Vareš Mine is projected to achieve full production (Dec 2026). The QP expects the Integration Plan to address DPM's planned change to the mining method, mine ventilation, revision to paste backfilling and reticulation, waste rock disposal, remediation of the temporary tailings storage facility, improvements to the power supply (notably to underground operations and the process plant), increase in water treatment capacity, and the condition of the haul road.

1.10 Mining Operations

The Vareš mine commenced production in 2024. Challenging ground conditions were encountered during the initial phases of development and ore mining. Successful methods of ground support have since been developed using extensive surface support, cable bolting and spiling, in conjunction with drilling short rounds, so development advance is now consistent and predictable. Stoping is still in its infancy and extensive use is made of stope surveys and reconciliation to develop design parameters to manage the impact on stope production of dilution and ore loss. As mining continues and deposit knowledge increases, stope and support design can be optimised to improve stability and reduce dilution. As a result of this over time, the geotechnical risk to the operation will be reduced.

The current dewatering design assumes very low groundwater inflows. This assumption is uncertain given that hydrogeological investigations at the mine site to date are limited in coverage. Gaps in the hydrogeological understanding present a risk of sudden inrush due to intersection of karstic features and high storage compartmentalised blocks, with limited controls currently in place, e.g. cover drilling.

The Vareš mine uses modern mobile equipment to extract the orebody through bulk longhole open stoping and mechanised cut-and-fill stoping. Two orebodies will be mined, Rupice and Rupice North West. The mine is accessed through two declines, with the upper decline providing the main route for the transport of broken ore and waste to surface and the nearby run-of-mine pad stockpile and crushing facilities. Fresh air is drawn into the mine through the upper decline and is exhausted by fans drawing from the lower decline.

The DPM design follows a bottom-up sequence using electro-hydraulic longhole percussion drilling and blasting methods, with longhole stopes with 20 m lifts, 20 m wide and 15 m long. Depleted stopes are filled with cemented paste fill to ensure stable conditions are maintained and to establish working platforms for future lifts. Cut-and-fill stoping has not yet commenced but will involve taking horizontal slices of ore using development scale percussion drill jumbos. The void resulting from the extraction of each slice will be filled with cemented paste or development waste fill to provide a working platform for the next lift.

Blasted stope ore is extracted using 15 t capacity load-haul-dump machines and loaded into 45 t capacity articulated dump trucks for haulage to the surface stockpiling facilities. The maximum mining fleet reaches 4 twin boom development jumbos, 3 longhole production drill rigs, 5 load-haul-dump machines and 6 dump trucks in 2026.

The production schedule is prepared as a sequence of primary stopes which are extracted from undisturbed rock before filling, and adjacent secondary stopes which generate wall exposures of backfill and are filled after extraction. The scheduled production cycles include time allowances for the development and extraction of the stopes, and deposition and curing of the fill.

Mine production is scheduled to reach 850 ktpa inclusive of development ore, supported by up to 2.97 km of waste development per year.

The technical and design work for the mine plan is completed to a prefeasibility level of confidence, adequate to support the declaration of Mineral Reserves. Further work is required on developing the mine plans and schedule, the backfill and ventilation system, hydrogeology and mine dewatering design, and waste management and storage, to improve the status of the mining studies to the higher confidence feasibility level.

1.11 Processing and Recovery Operations

The Rupice site is a greenfield location and consists of three differently graded stockpiles from the underground mine that are reclaimed by means of front-end loaders into a three-stage crushing plant. Waste rock is processed through the same crushing plant to produce the required aggregate materials for the paste backfill operation. Crushed ore and aggregate material are loaded onto trucks and transported to the Vareš Processing Plant and paste backfill plant respectively. The paste backfill plant and associated stockpiles and ancillary facilities are located near the underground mine portal at the site. A haul road connects the Rupice site to the Vareš Processing Plant site.

The Vareš Processing Plant is located on a brownfield site. Existing infrastructure was either demolished or repurposed for future use. The process plant includes the following process circuits: crushed ore handling and storage, ball mill grinding circuit, flotation (sequential silver-lead followed by zinc flotation), concentrate handling (thickening, filtration and loading), tailings handling (thickening, filtration and loading), reagents handling and storage, and plant services. The plant has a design capacity of 800 ktpa.

Following commissioning of the plant, ADT committed to adding a further stage of flotation into each of the cleaner circuits, using a Jameson (pneumatic) flotation cell in each case, acting as a first cleaning stage, producing final grade concentrate. The tailings filter is also understood to represent an impediment to the plant achieving capacity. While ADT has implemented a modification to add additional plates to the existing filter, DPM plans on installing a duplicate tailings filter to eliminate this potential bottleneck.

The available historical production data shows that the plant has not achieved its design production rate. While the monthly reports issued by ADT list the tonnes processed, they do not show operating hours. Therefore, it was not possible to assess whether the plant had been achieving its design instantaneous capacity when it was running – a lack of available ore is understood to have resulted in a significant shortfall in operating time for the plant to date.

Regarding the metallurgical performance, the results (both grade and recovery) for Ag are in line with, if not slightly ahead of, the expected performance based on the regression equations developed from the testwork. However, the results for Pb and Zn to date (both grade and recovery) fell short of the expected performance.

Overall, the plant appears to have been built in accord with the design as described in the DFS report, which itself was soundly based on the testwork. As only a very limited amount of testwork was undertaken on thickening and filtration, this has likely resulted in the apparent undersizing of the as built tailings filter. With a design capacity of 800 ktpa, it seems reasonable to expect that the plant will be capable of processing 850 ktpa, as per the DPM LoMP.

1.12 Tailings Disposal

This Technical Report provides a comprehensive review of the Tailings Storage Facilities (TSFs) associated with the Vareš Project, focusing on the Temporary TSF and the Veovaca TSF.

The Temporary TSF, located adjacent to the processing site, was used for short-term tailings storage but exhibited significant stability concerns, including active slope failure, tension in the HDPE liner, and risks to public safety and community relations. Immediate recommendations include halting further tailings placement, isolating the area, and initiating an investigation to address these deficiencies.

The Veovaca TSF, designed as a fully lined, dry stack facility, is located within the historic Veovaca II Open Pit. The facility is designed by Wardell Armstrong to store up to 5.1 Mt of filtered tailings in two phases, with most tailings used as underground backfill. The design adheres to the Global Industry Standard on Tailings Management (GISTM) and incorporates robust drainage, capping, and monitoring systems to ensure stability and environmental compliance. However, technical risks were identified, including slope stability concerns, inadequate drainage in critical areas, and potential tension in the HDPE liner due to settlement. Recommendations include remediating the topographic bowl behind the starter dam, enhancing drainage provisions, and implementing strict placement and compaction procedures to mitigate these risks.

The report also highlights the geotechnical and hydrogeological conditions of the Veovaca site, including shallow groundwater levels, variable tailings properties, and potential acid generation risks. Stability and seepage analyses confirm that the facility meets required Factors of Safety (FoS) under static, seismic, and extreme rainfall conditions. However, sensitivity analyses underscore the importance of achieving specified tailings compaction and density to maintain stability and storage capacity. Cost estimates for the TSF, including capital costs, operating costs, and closure costs, are deemed reasonable but require additional contingency to account for potential reworking of out-of-specification tailings and enhanced compaction efforts.

In conclusion, while the Veovaca TSF design is broadly reasonable and meets capacity requirements, addressing the identified technical risks and implementing the recommended measures are critical to ensuring the facility's long-term safety, stability, and environmental compliance.

1.13 Project Infrastructure and Logistics

The project incorporates two separate sites for mining and processing respectively, an access road and a concentrate logistics system as follows:

- The Rupice Site near to Borovica Gomja is where mine and surface infrastructure is located;
- The Veovaca Processing Plant which is located at Tisovci;
- A 25 km access road connecting the mine to the VPP, which is used for transporting of run of mine material to the plant for processing in 8x4 rigid on-highway construction trucks carrying 25 tonne payloads; and
- A rail loading siding for storage of containerised concentrates and loading to rail wagons for export via the national railway systems and Ploce Port on the Croation Coast.

The current production demonstrates that infrastructure is in place to support operations. However, during the site visit and review, a number of previous or on-going challenges were recognized which are known and being addressed.

The main challenge is specific sections of the access road between the mine and plant. The 25 km haulage route was constructed (or upgraded) as part of the capital investment and the alignment negotiates some high relief terrain. At full production, mine traffic will be intensive and ordinarily, this would not be an issue except for the series of slope failures which have occurred that impacted road operations. There are also concerns around the robustness of other aspects of the road design coupled with the road being used by both mine and non-mine traffic (sections being public road). A detailed review is required to better understand which sections of road present the most risk and DPM will likely undertake design and upgrade works to sections of the road.

Other issues to be addressed include:

- Electrical distribution design particularly related to feeders to the major equipment at the VPP and feeders to underground (bulk power supply from the grid appears to be sufficient);
- The condition of the mainline railway and potential for issues resulting in a need to truck concentrate further than planned impacting logistics costs; and
- Suboptimal drainage design on earthworks at the Rupice site causing ponding.

In terms of capital and operating costs, the QP noted in the monthly reports a USD 28 million capital still to be spent covering various cost items. Some of this capital cost is attributed to the completion of the haul road with a USD 0.7 million for rectification of the slope failure(s). Justification of this value was not provided and there is a high likelihood that more work is required.

While a detailed review by DPM of the various challenges is required, the QP does not believe the outcome would impact the statement of Mineral Reserve as events are likely to have a short-term impact (e.g. days or weeks) while an interim solution is found, provided the capital is invested early on to investigate and rectify these issues.

1.14 Water Management

Adding to the uncertainty of the hydrogeology (highlighted in Item 1.10), the mine dewatering system is also highly constrained by the water treatment plant capacity. The water treatment plant has been operating at/near its maximum capacity throughout commissioning and operations and has been observed to be a constraint to dewatering and mining operations at times.

A higher than predicted groundwater inflow rate would impact the production rates assumed in the life of mine plan. A sudden inrush event would pose a safety risk, could materially impact the mining production rates assumed in the life of mine plan, and require significant remediation measures.

Surface run-off from disturbed areas of the mine site that does not come into contact with the ore stockpiles, waste dumps or paste backfill plant is considered ‘non-contact’ and is diverted and discharged from the site without treatment. Best-practice is to divert runoff from any disturbed ground associated with the mine to a suitably designed sediment pond. DPM has indicated that it intends considering all site water as contact water. However, this is yet to be developed and incorporated into an update water management plan

Both higher groundwater in-flows and sudden inrush would have a cost impact. The expansion of the water treatment plant and sediment management infrastructure at the mine site will require additional capital, and an estimate is included the current economic analysis.

The QP made recommendations in relation to water balance studies to assess future water supply requirements; water shortage and/or water surplus; hydrogeological characterisation including hydrogeological modelling to better define mine inflows, the risk of sudden inrush and the risk of drawdown impact on affected persons.

1.15 Environment, Permitting and Social Consideration

The environmental, social and governance (ESG) input was prepared based on a desktop review of available information and a site visit by an ESG specialist. The review identifies ESG factors that could be Modifying Factors when reporting Mineral Reserves and may influence the determination of economic extraction. Through this review, the QP received limited information regarding status of approvals and compliance, surface rights and legal matters, which resulted in the uncertainties presented in this Technical Report.

From a permitting perspective, the operation appears to have two active environmental permits issued by the Federal Ministry of Environment and Tourism: one for the VPP and one for the Rupice mining area. A renewal for VPP environmental permit is in progress but the outcome is unknown. The status of urban planning and water approvals is unconfirmed based on the information provided, though the QP understands construction permits are outstanding for the Veovaca TSF access road and pipeline, and the paste plant. To support the full LoM plan, permits are also outstanding for the final waste rock volume, including storage of PAG waste material, and Phase 2 of the Veovaca TSF.

Several environmental assessments were conducted for the asset to inform permitting processes and align management practices with good international industry practice. These include EIAs prepared by Bosnian consultancies for in-country permitting processes, and an ESIA prepared by Wardell Armstrong International (WAI) for project financing.

The operation implemented an integrated management system through an online platform (INX), which includes policies, legal and other obligations, risk registers, management plans, incidents, inspections and other documents. A suite of 18 environmental and social management plans were originally prepared as part of the 2022 ESIA. These plans are being updated to reflect the current stage of operation, and to satisfy requirements of regulatory permits, as well as measures included in the 2022 ESIA. The operation has an annual monitoring programme aligned with permits and management plan requirements. The QP did not receive sufficient monitoring information to confirm the status of compliance with conditions of approval or confirm effectiveness of management controls.

The operation has a recently updated stakeholder engagement plan, including stakeholder mapping, communication activities, key issues, monitoring and evaluation. Grievances are managed through a grievance mechanism that is reportedly aligned with UN Guiding Principles on Business and Human Rights. The previous operator (ADT) indicated it had broad support for the operation but recognised the need for continued efforts to improve relations, specifically with communities around the VPP and Veovaca TSF, along the haul road, and with stakeholders in the adjacent Kakanj municipality. The most common concerns raised by stakeholders relate to the potential for community health impacts, particularly dust from vehicle movements near VPP, environmental impacts specifically on water courses, air quality and biodiversity, and requests for local employment and procurement.

The identified potential modifying factors relate to permitting, environmental and social management, stakeholder engagement, and operational water and waste management, climate change and closure.

- Permitting: Delays in obtaining permits or compliance-related issues could disrupt operations, delay ramp-up schedules, or result in fines and reputational damage.
- Environmental and social management: Uncertainties around effectiveness of management controls present a risk that additional capital and operating expenditure may be required to upgrade infrastructure and / or address any actual impacts.
- Stakeholder engagement: Historic gaps in engagement with certain stakeholder groups and several on-going issues could give rise to a deterioration of relationships and social licence.

- Water management: Risks include potential impacts on downstream water quality, water supply sources, and insufficient baseline data for the Veovaca TSF. Additional costs may be required to upgrade water management infrastructure
- Waste management: In addition to outstanding permits for waste facilities, there is a risk of delays to the Life of Mine (LoM) plan and cost uncertainties from gaps in waste management planning for revised LoM plan.
- Climate change: Bosnia’s upcoming carbon tax in 2026 could directly or indirectly result in an increase to operating costs. The operation lacks a decarbonization strategy and future capital expenditures for carbon reduction projects remain undefined
- Closure: Additional costs may arise from waste rock and water management requirements. The closure plan also assumes minimal post-closure water management and a 5-year monitoring period, which may be insufficient given legal obligations for 30 years of aftercare.

These risks are considered qualitative and therefore no specific adjustments were made to the LoM plan or financial model. A series of recommendations were made to address the factors to reduce the risk to continuation of operations, control of costs and maintenance of the operations social licence to operate.

1.16 Capital and Operating Costs

The continued initial capital costs, amounting to USD 76 million, and sustaining capital costs, amounting to USD 143 million, were projected (excluding USD 24 million as a closure cost allowance).

The annual operating costs are between USD 90 and 100 million when the mine operates at full production. Mining accounts for 58% of costs, with processing and tailings disposal accounting for 25%. A contingency of 7.5% has been added to all capital and operating costs.

1.17 Economic Assessment

ADT secured off-take agreements for 100% of silver-lead concentrate and over 90% of zinc concentrate production for the first 2-3 years of operations. Concentrate deliveries have already commenced, with further sales agreements recently established.

The customers are well-known smelting and trading companies. Terms are representative of the general market for long-term concentrate sales with smelters and traders. The QP expects that the contracts can be extended at the same, or better, terms and conditions.

Commodity price forecasts are based on Bloomberg’s analyst consensus metal price forecast. The QP notes that the long-term price for gold is USD 2,200/oz, which is a step change increase that has taken place over the last six months. The QP notes that this aligns with an independent consensus market forecast source.

Net smelter revenue amounts to USD 250 and 400 million during full production years, varying in line with the various metal grades. In order of priority, revenue is generating by silver, zinc, lead, gold, and copper.

The economic analysis undertaken results in a positive NPV of USD 1,585 million at a discount rate of 5%. The key technical and economic inputs and resulting economic indicators are presented in Table 1-3.

Table 1-3: Key Inputs and Financial Indicators

Description	Unit	Value
Macroeconomic Parameters		
Long term metal prices		
Gold	(USD/oz)	2,212
Silver	(USD/oz)	27.69
Zinc	(USD/lb)	1.21
Lead	(USD/lb)	0.94
Copper	(USD/lb)	4.24
Discount rate	(%)	5
Production		
Mineral reserve	(Mt)	9.5
Annual throughput	(ktpa)	850
Average grade processed (LoM average) (1)	(g/t Au Eq)	9.15
Gold equivalent recovery (LoM average)	(%)	85.4
Gold equivalent payability (LoM average)	(%)	76.2
Gold equivalent payable production (LoM)	(Moz Au Eq.)	1.8
LoM Operating Costs	(USDm)	(USD/t ore)
Mining	570	60
Processing + TSF	246	26
G&A	142	15
Contingency	72	8
Royalties	21	2
Total cash cost (2)	**1,050**	**111**
Offsite Cost (3)	419	
LoM All-in Sustaining Cost (co-prod) (2)	(USD/oz Au Eq)	901
Capital Cost Estimate		
Initial Capital	(USDm)	76
Sustaining Capital (LOM)	(USDm)	143
Closure Costs	(USDm)	24
Project Economics		
Cash flow (post-tax)	(USDm)	2,071
NPV (after-tax, 5% discount)	(USDm)	1,585

Note:

(1) A Au equivalent grade is reported to align with DPM's standard reporting format. The QP notes the Au contributes to 14% to the net revenue, whereas other metals contribute in the amounts of, Ag 39%, Zn 28%, Pb 17%, and Cu 2%. The reported grade was calculated from the Mineral Reserve metal grades presented in Table 1-2. The QP further notes that the commodity prices are detailed in Table 19-1, the metal recoveries in Table 22-6, and the metal payabilities in Table 22-1.

(2) Cash cost and cash cost per tonne of ore processed; all-in sustaining costs and all-in sustaining cost per gold equivalent ounce on a co-product basis are non-GAAP financial measures or ratios and have no standardised meaning under IFRS Accounting Standards (IFRS) and may not be comparable to similar measures used by other issuers. Refer to the "Non-GAAP Financial Measures" in Item 2.8 of this Report for more information, including a detailed description of each of these measures.

(3) Offsite costs include concentrate sales costs, including freight, treatment and refining charges.

1.18 Conclusions and Recommendations

The Vareš Mine commenced production and derisked many areas of the project. A number of areas requiring attention were highlighted, symptomatic of a new operation. DPM is developing an Integration Plan as part of DPM taking over ownership and operation of the Vareš Mine. This is a short term plan which will be deployed until the point at which the Vareš Mine is projected to achieve full production, which is expected to be by December 2026.

The production of this Technical Report took place during the course of a transaction, resulting in the flow of information being restricted. Limited information and statistics on performance, costs, state of infrastructure and operations, environmental, social and governance, including permitting, are known. However, the QPs have reviewed sufficient data to reach an opinion and be satisfied that there is a sufficient level of confidence in the technical studies and work undertaken to support the declaration of the Mineral Resources and Mineral Reserve.

Various areas of risk have been identified and all of the QP expect the Integration Plan to address these. This will include DPM's planned change to the mining method, mine ventilation, revision to paste backfilling and reticulation, waste rock disposal, remediation of the temporary tailings storage facility, improvements to the power supply (notably to underground operations and the process plant), increase in water treatment capacity, and the condition of the haul road. The QPs have made a wide range of recommendations, as fully described in the main body of this Technical Report.

The areas of high risk that the QPs perceive may affect the delivery of the Mineral Asset include permitting of the paste backfill plant, the requirement for greater water treatment and storage, the maintenance and/or upgrade of the 25 km haul road, and the remediation of the temporary tailings storage facility. A number of medium risks were also identified in relation to further permitting requirements, underground conditions and underground water inflow, the mining method and mine design yet to be changed, the Veovaca tailings storage facility yet to be constructed, waste rock management and stakeholder relations. These risks are still a reflection of the early stage of the mine development and ore production and will require the appropriate attention. The associated capital and operating costs are included in the economic analysis.

ITEM 2. INTRODUCTION

SRK Consulting (UK) Limited compiled this Amended and Restated NI 43-101 Technical Report (the Technical Report) on the Vareš polymetallic mine (the Vareš Mine or Mineral Property), located in Bosnia and Herzegovina. For reference, the initially issued NI 43-101 Technical Report, has been updated to reflect the change of QP in respect of underground geotechnics from Michael di Giovinazzo to Neil Marshall, and the removal of revenue associated with a minor amount of Inferred Mineral Resource being present in a few mining blocks.

Dundee Precious Metals Inc (DPM) is contemplating the acquisition of Adriatic Metal Plc (ADT) (the Transaction).

The Vareš Mine has been under the ownership of ADT, who completed construction of the process plant and most mine infrastructure in 2023. Underground development to access the Rupice deposit commenced in 2023, with first ore mined in February 2024. First production of two concentrates for silver, zinc, gold, lead and copper (in order of revenue generation) took place in May 2024. See Item 6 – History for further information.

The Technical Report was prepared on behalf of DPM and reflects the mine plan and mining and operating methods DPM contemplates applying to the Vareš Mine.

2.1 Terms of Reference

This Technical Report is intended to support DPM and ADT disclosures in the news releases, management information circulars and other disclosure documents in connection with the Transaction.

The Rupice deposit, which is the focus of current operations, and the Veovaca deposit, which has been historically mined by open pit, are wholly contained within the Vareš licence area.

This Technical Report is produced in accordance with the Standards of Disclosure for Mineral Projects as contained in NI 43-101 and accompanying policies and documents. NI 43-101 utilises the definitions and categories of Mineral Resources and Mineral Reserves as set out in the Canadian Institute of Mining, Metallurgy and Petroleum (CIM) Definition Standards for Mineral Resources and Mineral Reserves (May 2014).

All measurement units used in this Technical Report are metric unless otherwise noted, and currency is expressed in United States dollars (USD).

A draft of this Technical Report was provided to DPM to check for factual accuracy, to the best of DPM's knowledge.

2.2 Qualified Persons

The Qualified Persons (QPs) responsible for the "Amended and Restated NI 43-101 Technical Report on the Vareš Mine, Bosnia and Herzegovina", issued on 9 June 2025, and their respective areas of responsibility are presented in Table 2-1.

Table 2-1: Qualified Persons

Category	Author	Responsible Items	SRK Practice
Mineral Reserve, Economic evaluation Permitting, Environmental, Social and Governance, Review lead	Sabine Anderson MEng, CEng, MIMMM	1.1 – 1.3, 1.9, 1.15 – 1.18 2 - 6 12- 24 25.1 25.8 – 25.14 26.4, 26.11, 26.12 27	UK
Geology and Mineral Resource estimation	Martin Pittuck MSc, CEng, FGS, MIMMM (QMR)	1.4 – 1.7, 1.9 7 - 11 14 25.2, 25.3 26.1	UK
Metallurgy and processing	Dr John Willis MAusIMM(CP)	1.8, 1.11 13 17 25.5 26.6	UK
Mining engineering	Peter Myers FAusIMM	1.10 16 other than: 16.1 16.2 16.8.6 16.12.2	UK

Category	Author	Responsible Items	SRK Practice
Geotechnical engineering	Neil Marshall MSc, CEng, MIMMM	16.1 26.2	UK
Hydrogeology, dewatering, water management	James Bellin MSc, CGeol, FGS	1.14 16.2, 16.12.2 18.5, 18.9.2 20.3.4 25.7 26.2, 26.9	UK
Infrastructure	Colin Chapman MSc, CEng, MIMMM	1.13 18 other than: 18.4 18.5 25.8 26.10	UK
Tailings management	Richard Martindale BSc, MSc, CEng, MIMMM	1.12 18.4 25.6 26.7, 26.8	UK

2.3 Personal Inspection of the Vareš Mine

The QPs that undertook personal inspections of the Vareš Mine from 25 to 26 March 2025 included:

- Mr Martin Pittuck, in relation to Rupice deposit and Mineral Resource estimate. He visited the drill core shed, the current underground workings;
- Mr Mikko Koivisto, mining engineer with SRK Consulting (UK) Ltd, provided input into the review of the underground mining operations, led by Mr Peter Myers. Mr Koivisto visited the relevant underground working areas;
- Mr Michael Di Giovinazzo, geotechnical engineer with SRK Consulting (UK) Ltd, provided input into the review of the underground working areas, led by Neil Marshall. Mr Di Giovinazzo visited the relevant underground working areas; and
- Mr Richard Martindale visited the temporary TSF, the Veovaca TSF, and the main site haul road (processing site to mine site).

Ms Anderson did not undertake a visit of the mine, however joined meetings with the QPs and the DPM technical team in Bosnia during the site visit.

Ms Emily Harris, who is not a QP, but is part of the SRK team, also undertook a personal inspection of the surface infrastructure at Rupice and VPP, and the Veovaca TSF, during these days.

The QPs, Michael Di Giovinazzo and Ms Harris held face to face discussions with key ADT personnel. The QPs are satisfied that the discussions, site visits and all inspection were conducted with the full support of ADT and without restriction in any respect. All of the QPs note that data flow post the site visit was restricted, as outlined inItem 12.

2.4 Levels of Study

The Vareš Mine reached feasibility level of confidence in 2021, with the issuance of "Vareš & Rupice Feasibility Study Report" prepared by Ausenco Engineering Canada Inc.("Ausenco") dated 23 September 2021 (the "DFS"). Authors included Ausenco, Adriatic Metals, CSA Global, Mining Plus, Paterson and Cooke, and Wardell Armstrong International. Mineral Resources and Ore Reserves were reported following the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves ("JORC Code").

Since then, ADT constructed and developed the mine and has undertaken various additional recent studies.

At the time of this Report, DPM is developing an Integration Plan as part of the Transaction. This is a short-term plan which will be deployed until the point at which the Vareš Mine is projected to achieve full production (Dec 2026). The QP expects the Integration Plan to address DPM's planned change to the mining method, mine ventilation, revision to paste backfilling and reticulation, waste rock disposal, remediation of the temporary tailings storage facility, improvements to the power supply (notably to underground operations and the process plant), increase in water treatment capacity, and the condition of the haul road.

The overall level of study is deemed to be at pre-feasibility, whereas some components are at feasibility level and some are now actuals and known. Whereas pre-feasibility is a lower confidence level of study than the DFS issued in 2021, DPM now has the benefit of construction and initial production having identified a number of unknowns which are being addressed. Therefore, despite the level of confidence being overall at pre-feasibility, in the life of mine plan and inputs to the economic evaluation is deemed to be higher than at the time of the DFS (with the exception of permitting which the QPs have not been able to review due to insufficient data provision).

2.5 Technical Study Authors

The QPs reviewed data provided by ADT and DPM in relation to the estimation of the Mineral Resources and Mineral Reserve. The QPs did not author any part of the technical studies resulting in the life of mine plan.

The authors of technical and related studies supporting the Mineral Resources and Mineral Reserve are listed in Table 2-2, alongside the perceived level of confidence achieved. The QPs reviewed all data made available to satisfy themselves that the technical and related studies were sufficiently advanced to meet minimum prefeasibility level of study and associated level of confidence, to enable the sign off of Mineral Resources and Mineral Reserve and do not disclaim any responsibility.

Table 2-2: Technical Study Authors

		Confidence Level
Mineral Resource estimation	ADT and appointed consultants	Suitable for FS
Geotechnical studies	ADT and appointed consultants. DPM has provided useful comments on geotechnical studies and current underground mine conditions	PFS
Hydrogeological studies	ADT and appointed consultants	PFS
Mine plan, including design, scheduling, equipment schedule for the life of mine	DPM and appointed consultants	PFS
Metallurgy and processing	ADT and appointed consultants Mostly constructed with some changes/ upgrade planned by DPM.	FS
Tailings management	ADT and appointed consultants DPM is developing a plan to remedy the Temporary TSF as part of its Integration Plan	PFS
Water management	ADT and appointed consultants	
Mine infrastructure	ADT and appointed consultants. Mostly constructed. Infrastructure construction to be completed includes DPM planned modifications and upgrades	PFS for incomplete items
Off-site logistics	ADT and appointed consultants, now constructed.	N/A (1)
ESG	ADT and appointed consultants, including Wardell Armstrong International	N/A (1)
Permitting	Due to the limited data provided, SRK was not able to assess the technical studies conducted	N/A (1)
Operating costs	DPM	PFS
Capital costs	DPM	PFS
Economic assessment	DPM, with inputs sourced from other authors listed in this table as relevant.	PFS

1. N/A: Not applicable

2.6 Effective Date

There are several dates pertinent to the Technical Report as follows:

- The Effective Date is 1 April 2025, being the cut-off date of availability of data and, therefore, the date of the Mineral Resource and Mineral Reserve estimates and the economic evaluation; and,
- The signature date of the Technical Report is 9 June 2025.

Any changes and/or data made available between the Effective Date and the date at which the Report is published by DPM was not considered by the QPs. The QPs do not take any responsibility for requesting updates from DPM or updating the Technical Report in relation to any material changes, except as otherwise required by applicable laws.

2.7 Information Sources

This Technical Report is based on various key study documents and ADT public releases. The full list of references is presented in Item 27.

As the Vareš Mine has commenced production, information and statistics on performance, costs, state of infrastructure and operations, environmental, social and governance, including permitting, are known. The QPs highlight that their review and the production of this Technical Report took place during the course of the Transaction, resulting in the flow of information being restricted. The QPs direct the reader to Item 12, which outlines the data that has not been provided during the period of the review, the perceived impact and risk.

2.8 Non-GAAP Financial Measures

Certain financial measures referred to in this Technical Report are not measures recognised under IFRS and are referred to as non-GAAP financial measures or ratios. These measures have no standardised meaning under IFRS and may not be comparable to similar measures presented by other companies. These measures are intended to provide additional information and should not be considered in isolation or as a substitute for measures prepared in accordance with IFRS.

The non-GAAP financial measures used in this Technical Report and common to the gold mining industry are defined below:

- Cash cost and cash cost per tonne of ore processed: Cash cost consists of all production related expenses including mining, processing, services, filtered tailings and paste fill, royalties and general and administrative. Cash cost per tonne of ore processed is calculated as cash cost divided by volumes of ore processed.
- All-in sustaining cost and all-in sustaining cost per gold equivalent ounce on a co-product basis: All-in sustaining cost consists of all cash costs, plus treatment charges, penalties, transportation and other selling costs, cash outlays for sustaining capital expenditures and leases, and rehabilitation-related accretion and amortisation expenses. All-in sustaining cost per gold equivalent ounce is calculated as all-in sustaining cost divided by payable gold equivalent ounces. The QPs use conversion ratios for calculating gold equivalent ounces for its silver, zinc, lead and copper sales, which are calculated by multiplying the volumes of metal sold by the respective assumed metal prices and dividing the resulting figure by assumed gold price.

These non-GAAP cost metrics capture the important components of the Company's production and related costs and are used by DPM and investors to monitor cost performance at the DPM operations.

As the Vareš Mine is not in commercial production, the QPs do not have historical non-GAAP financial measures nor historical comparable measures under IFRS, and therefore the foregoing prospective non-GAAP financial measures or ratios presented may not be reconciled to the nearest comparable measure under IFRS.

2.9 Forward-Looking Statements

This Technical Report contains “forward-looking information” or “forward-looking statements” that involve several risks and uncertainties. Forward-looking information and forward-looking statements include, but are not limited to, statements with respect to the future prices of metals, the estimation of Mineral Resources and Reserves, the realisation of mineral estimates, the timing and amount of estimated future production, costs of production, capital expenditures, costs and timing of the development of new mineral deposits, success of exploration activities, permitting time lines, economic analysis, LOM, rates of production, annual revenues, internal rate of return (IRR), net-present value (NPV), currency fluctuations, requirements for additional capital, and government regulation of mining operations.

Often, but not always, forward-looking statements can be identified by the use of words such as “plans”, “expects”, or “does not expect”, “is expected”, “budget”, “scheduled”, “estimates”, “forecasts”, “intends”, “anticipates”, or “does not anticipate”, or “believes”, or variations of such words and phrases or state that certain actions, events or results “may”, “could”, “would”, “might” or “will” be taken, occur or be achieved. Forward-looking statements are based on the opinions, estimates and assumptions of contributors to this report. Certain key assumptions are discussed in more detail herein.

Forward-looking statements involve known and unknown risks, uncertainties and other factors which may cause actual results, performance or achievements to be materially different from any other future results, performance or achievements expressed or implied by the forward-looking statements.

Such factors include, among others: fluctuations in metal prices, risks arising from an inflationary environment and the impact on operating costs and other financial metrics, including risks of recession; the commencement, continuation or escalation of geopolitical crises, and their direct and indirect effects on the operations of the Vareš Mine; changes in tax, tariff and royalty regimes, operations, or financial condition; operational risks inherent in the mining industry; the speculative nature of mineral exploration, development and production, including changes in mineral production performance, exploitation and exploration results; dependence on continually developing, replacing and expanding its Mineral Reserves; risks that quantities or grades of Mineral Reserves will be diminished, and that Mineral Resources may not be converted to Mineral Reserves; competition in the mining industry; risks related to the financial results of operations, changes in interest rates, and the ability to finance operations; risks related to managing environmental and social matters, including risks and obligations related to closure of the Vareš Mine; fluctuations in foreign exchange rates; possible inaccurate estimates relating to future production, operating costs and other costs for operations; as well as those risk factors discussed or referred to in this report and in DPM’s latest annual information form under the heading “Risk Factors” and other documents filed from time to time with the securities regulatory authorities in all provinces and territories of Canada and available at www.sedarplus.ca and ADT’s public disclosure documents.

There may be factors other than those identified that could cause actual actions, events, or results to differ materially from those described in forward-looking statements, there may be other factors that cause actions, events or results not to be anticipated, estimated or intended. There can be no assurance that forward-looking statements will prove to be accurate, as actual results and future events could differ materially from those anticipated in such statements. Accordingly, readers are cautioned not to place undue reliance on forward-looking statements. Unless required by securities laws, the authors undertake no obligation to update the forward-looking statements if circumstances or opinions should change.

ITEM 3. RELIANCE ON OTHER EXPERTS

3.1 Legal Title

The QP did not review a legal due diligence report nor information around surface rights for the property, as this was not available during the period of the review. In addition, the QPs were not provided with copies of environmental approvals, permit applications, compliance reports or an updated version of a permit register for the asset (version provided is dated 2023).

The QPs who prepared the Technical Report are therefore including a limited disclaimer of responsibility for Sections 4.3, 4.4, 4.5, 4.6. 5.3 and 20 as the QP has relied on incomplete information provided by ADT (as detailed in Section 20.1) to identify qualitative risks linked to legal and environmental potentially modifying factors.

The QP notes that they did not consider any legal matters associated with the Transaction. This includes the process by which DPM secures full ownership and rights for it to operate the Mineral Asset and deliver on the life of mine plan.

Legal title is required to enable operations to continue.

3.2 Environmental, Social and Governance

The QP taking responsibility for Items 4, 5 and 20 has relied upon Ms Harris (MSc, CEnv, MIEMA) to prepare the parts of Items 4, 5 and 20, that relate to legal and environmental matters. Ms Harris is a Chartered Environmental professional with 18 years experience in the mining industry.

3.3 Taxation

The QP relied on DPM for all matters relating to taxation and how it is applied in the economic analysis. Changes or inaccuracies in taxation will impact the post-tax cash flow, presented in Item 22.14. The impact may be material, however would not impact the Mineral Reserve declaration.

ITEM 4. PROPERTY DESCRIPTION AND LOCATION

4.1 Property Description and Ownership

The Vareš Mine is located in Federation of Bosnia and Herzegovina (“Bosnia”) and owned and operated by Adriatic Metals BH d.o.o., a wholly owned subsidiary of ADT. The Vareš Mine is located in a single concession comprising three separate licence areas; one at Rupice in the west and two at Veovaca in the east. The area of the original concession was 280.5 ha, with 83.1 ha of that at Rupice and 197.5 ha at Veovaca. Subsequent to the original concession being granted, it was extended increasing the overall project area to 869.3 ha with 535.2 ha at Rupice and 330.1 ha at Veovaca.

4.2 Location

The Vareš Mine is situated within the Bosnia autonomous entity, made up of 10 cantons (regions) that have their own cabinet, constitution, parliament and judicial powers. Cantons are further divided into municipalities. The Vareš Mine is situated wholly within the Zanica-Doboj Canton and Vareš Municipality. The western boundary of the mineral concession is adjacent to the municipality boundary with Kakanj Municipality.

The Project is located approximately 50 km from the capital city of Sarajevo. The closest town is Vareš, located between the Rupice Mine (8.5 km north-west) and Vareš Processing Plant (VPP) (3 km east) (Figure 4-1). Refer to Item 5.3 for more detail on communities surrounding the project. Table 4-1 provides an overview of the geographical data for the Vareš Mine.

Table 4-1: Geographical Data

Description	Detail	
Country	Bosnia and Herzegovina	
Region	Zenica-Doboj Canton, Vareš Municipality	
Area	Zvijezda Mountain and Vrući Potok Valley	
Design Altitude (AMSL)	1060 – 1250m	
General topography of site	Mountainous	
Survey coordinates system	MGI 1901 Balkans zone 6 Datum: MGI 1901	
Centre point coordinates	Latitude	Longitude
Rupice mine	6519110.763	4894600.403
VPP	6528391.339	4888466.984
Veovaca TSF	6529717.831	4889726.445

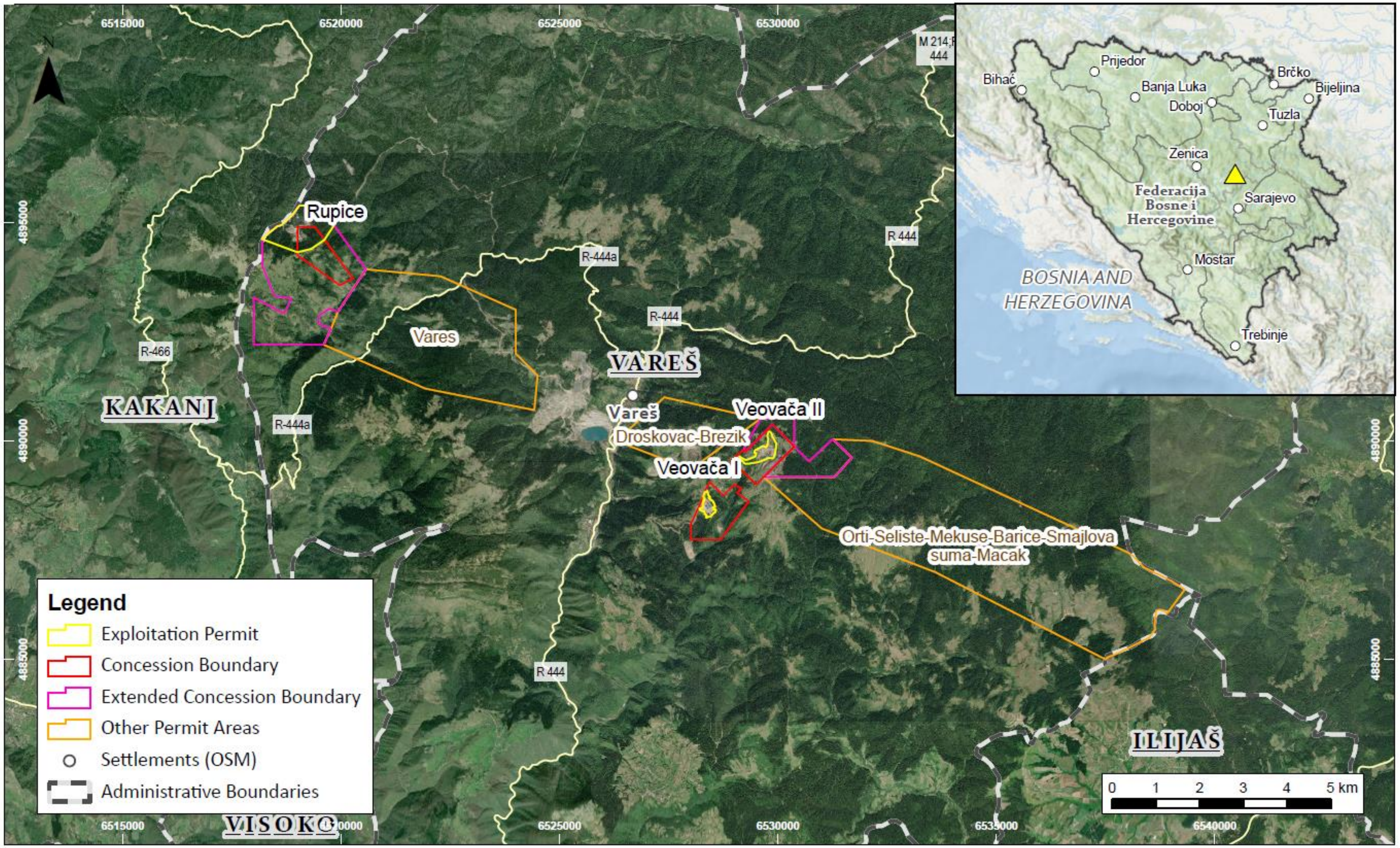


Figure 4-1: Mineral tenements (Source: SRK)

4.3 Surface Rights

No legal opinion was made available regarding the status of surface rights for the Vareš Mine.

4.4 Mining Rights and Approvals

4.4.1 Regulatory Framework

The Law on Concessions (No 40/02 and 61/06) regulates the process for awarding mineral rights. According to this law, the awarding of concessions for minerals shall be regulated at a Cantonal (regional) level, rather than Federal. A concession is awarded via a contract or agreement that has a definite term, not exceeding 30 years.

The ‘Law on the Mining Industry’ of the Federation of Bosnia and Herzegovina (Law 01-02-224/10) provides the legal framework for mining activities. Article 4 states the management of mineral raw materials is the responsibility of the Federation and the Cantons, ensuring their judicious utilisation in compliance with regulations on safety of mining facilities and employees, and on the protection of the environment and nature.

To authorise a mining operation, it is necessary to obtain the following permits from the Federal Ministry or the Cantonal Ministry responsible for the mining industry (Article 37):

- exploitation permit;
- permit for complete and permanent suspension of exploitation;
- permit for operations according to a mining design;
- permit for the use of mining facilities, plant, equipment and installations - use permit;
- provisional permit for operations; and
- final permit for operations.

4.4.2 Current Status

The QPs were provided with copies of the concession agreement and exploitation permits for the Vareš Mine. Independent legal opinions to confirm whether the concessions and licences are in good standing with the responsible authorities were not made available for the preparation of this Technical Report.

The concession agreement (No. 04-18-21389-1/13) was issued by the Ministry of Economy of the Zenica-Doboj Canton in March 2013 for a 25-year period, expiring in 2038. The agreement can be extended for an additional 12 years to 2050. The concession agreement includes basic conditions relating to environmental protection and a commitment to rehabilitate the site at closure.

Several amendments or annexes were issued after the original agreement to change the name of the concession holder to Eastern Mining d.o.o. (Annex 1 and 2), add rights to gold and silver (Annex 4) and to extend the area for activities (Annex 3, 5 and 6). The project-related mineral tenements are set out in Table 4-2 and in Figure 4-1.

Table 4-2: Mineral tenements

Document	Number	Area name	Granted	Expiry
Concession Agreement	No.:04-18-21389-1/13	Veovaca I, Veovaca II, Rupice-Jurasevac, Brestic	12-Mar-13	12-Mar-38
Annex 3 and 6	No.:04-18-21389-1/13	Rupice – Borovica and Veovaca - Orti - Seliste - Mekuse	14-Nov-18	12-Mar-33
Annex 5	No 2-14-14461/20	Orti-Selište-Mekuše- Barice-Smajlova and Droskovac-Brezik and Borovica – Semizova Ponikva	3-Dec-20	3-Dec-50

An exploitation permit (No. 06-14-1-334/21) was obtained for Rupice-Jurasevac-Brestic in July 2021 and remains valid during the term of the concession agreement. An exploitation permit (No 06-14-2-658/20) was also issued for Veovaca I and II in January 2021.

Conditions in the Rupice exploitation permit required a hydrological study and tests to establish possible connection between the underground excavations and water features in the Bukovica basin, and establish quantitative and qualitative monitoring of springs in the Bukovački potok basin. This work was completed but evidence of receipt and response by the authorities was not available to the QPs for review.

In December 2024, media sources[1] reported that the Cantonal Court of Mostar annulled the Rupice exploitation permit following a lawsuit filed by JP Vodokom (water company), citing the potential threat to the drinking water source suppling Kakanj Municipality. Media sources[2] also reported the permit was re-issued 15 days later in January 2025. The QP understands from discussions with ADT that authorities are satisfied with the information provided regarding the impact from the mine on the Bukovica basin. However, evidence of this and legal opinion on the lawsuit and risk of future claims was not made available for this review.

Regarding the approvals issued subsequent to the exploitation permit (identified in Section 4.4.1), the QP did not have sight of recent permit register, copies of approvals or findings of a legal due diligence to confirm the status. ADT reported in the 2024 Rupice Mineral Resource and Reserve Update (ADT, March 2025) that "*All major permits for operations have been granted by the various competent authorities within Bosnia and Herzegovina, however some more routine permits and permits that would not ordinarily be issued until after the commencement of production are outstanding and are expected to be issued in due course*."

4.4.3 Royalties and Other Rights

Please refer to Item 22.5 describing the mining royalites payable. No other parties are known to have rights with any economic terms.

[1] CANTONAL COURT IN MOSTAR DECIDED: Adriatic Metals loses exploitation permit for Vareš Mine | Žurnal | Jedina slobodna teritorija

[2] Adriatic Metals Fast-Tracks New Mining Permit - CIN

4.5 Environmental Approvals

4.5.1 Regulatory Framework

The primary environmental approval in the Federation of Bosnia and Herzegovina is an environmental permit. The Law on Environmental Protection (No 15/2021) requires an Environmental Impact Assessment (EIA) process to be conducted to obtain an environmental permit. EIAs are mandatory for projects that may significantly affect the environment, including mining. The EIA process must be undertaken by an authorised body in accordance with relevant regulations and must include the preparation of a Waste Management Plan, prepared in accordance with Article 19 and 20 of the Law on Waste Management (No 33/03, 72/09 and 97/17).

Once complete, an EIA report is submitted to the Ministry of Environment and Tourism for review and decision-making. Following submission, a 30-day period for public comment is conducted, including a public hearing, and comments received are considered in the decision to approve or decline the environmental permit. The environmental permit is issued for a period of 5 years, after which the operator is obliged to submit a request for re-issuance of the permit.

In addition to the environmental permit, several other permissions are required including the following:

- Water consents for use, collection, treatment and discharge of water, in accordance with Law on Water (No 70/06);
- Urban planning permit, in accordance with Law on Spatial Planning and Land Use (No 2/06,72/07, 32/08, 4/10, 13/10 and 45/10), followed by building permits for construction, and usage permits once development has been constructed and inspected.

An EIA and environmental permit are also required for rehabilitation and closure of industrial areas at the end of operations.

4.5.2 Current Status

Several environmental assessments have been conducted for the asset, as discussed in Section 20.2.1. These include EIAs prepared by Bosnian consultancies for in-country permitting processes, and an ESIA prepared by Wardell Armstrong International (WAI) for project financing. While the QP has a copy of the 2022 ESIA, it was not provided with copies of EIAs prepared for the permitting process, copies of permits or an up-to-date environmental permit register (version provided is dated 2023). It was therefore not possible to verify the status of environmental approvals for the mine and review associated conditions.

ADT reported in the 2024 Rupice Mineral Resource and Reserve Update (ADT, March 2025) that it is “currently compliant with all legal and regulatory requirements and there is no reason to assume any further government or local council permits, licences, or statutory approvals will not be granted, if required”. The QP was unable to verify this statement.

Based on the 2023 permit register, it appears that the mine has two active environmental permits issued for the Mine by the Federal Ministry of Environment and Tourism; one for the VPP (UPI 05/2-23-11-195/19), which is valid until May 2025, and one for the Rupice mining area (UPI 05/2-02-19-5-60/20 SC), which is valid until May 2026. At the end of March 2025, ADT reported that it was in the process of applying for a renewal of the VPP environmental permit. The public consultation process had been completed, and ADT was expecting issue of the new permit in the following weeks.

The mine also had a third environmental permit (UPI 05/2-23-11-145/19) for rehabilitation and closure works of the old Tiscovi processing plant, which has since been completed.

The current status of urban planning and water approvals is unconfirmed based on the information provided.

A Constitutional Court ruling in July 2024 repealed the Federal law permitting the removal of state forest for temporary use. This resulted in ADT losing previously issued permissions for construction of planned infrastructure due to proposed footprints overlapping with State Forest boundaries. Affected infrastructure included part of waste rock storage facility at Rupice, the tailings facility south of VPP and the paste backfill plant. Discussions with the Ministry of Environment and Tourism remain on-going to resolve land access issues (Annual Report, ADT 2025).

In communication with regulatory authorities, waste disposal at Rupice WRD re-started. However, additional permits are required to store a surplus of waste rock that cannot be accommodated in the current location. A proportion of this waste rock will be potentially acid generating (PAG). PAG waste is currently stored on the ore stockpile until a permanent location is identified and permitted.

For tailings, a temporary TSF was constructed immediately adjacent to the northern access to VPP, within the limits of the exploitation permit boundary. This facility has been in use since the start of production. However, the status of permitting for this facility is unclear. In October 2024, the VPP environmental permit (UPI 05/2-23-11-195/19) was amended to include Phase 1 of the Veovaca TSF. At the end of March 2025, the QP was verbally informed by ADT that construction permits were still pending for part of the dedicated access road to the facility and the pipeline for return water to VPP. A permit for Phase 2 of the facility will be required in future to support the LoM plan.

The current permitting status of the paste plant is unclear from the information provided.

As disclosed in the ADT 2024 Annual Report, a complaint against Bosnia and Herzegovina regarding environmental impacts from the Vareš Mine was made to the Secretariat of the Bern Convention (Convention on the Conservation of European Wildlife and Natural Habitats) at the Council of Europe. The complaint was lodged in 2022 and remains under review, with active discussions with relevant stakeholders. Legal opinion is required to confirm the implications of potential outcomes from this case.

4.6 Environmental Liabilities

The QP identified potential environmental liabilities based on information reviewed for this Technical Report, but further legal due diligence is required for a comprehensive view on liabilities associated with the mine.

The Vareš District has a significant mining history, resulting in several historic operations such as the now-abandoned Smreka iron mine to the west of Vareš and local steel making activities. The Vareš Mine concession area specifically extends over historic mining infrastructure, including the Veovaca open pit, the Tisovci mineral processing facility (which was mostly demolished except for office buildings being re-used by the mine), and a TSF associated with the Tisovci processing facility.

Both the Veovaca open pit and site of the Tiscovi mineral processing facility are actively used for Vareš Mine infrastructure. By interacting with these sites, the QP expects historic liabilities have been accepted and DPM will be responsible for rehabilitation of the sites at the end of operations, upon completion of the Transaction.

The historic TSF is located immediately downstream of the new Veovaca TSF. It is located within the concession area but outside of the Veovaca exploitation licence area. According to the 2022 ESIA (WAI, 2022), "*the starter embankment of the cross valley TSF and upstream raises are over-steepened and localised instability and seepage has occurred. In addition, the water level within the facility is very high…The water quality at depth is unknown*". No legal opinion was made available regarding the ownership of this facility or the liabilities associated with it. The QP understands ADT does not have ownership, responsibility or control over the historic TSF despite it being located within the concession area.

4.7 Significant Factors and Risks

Significant factors and risks related to mineral rights, environmental approvals and other legal considerations, are reported in Section 20.

ITEM 5. ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE AND PHYSIOGRAPHY

5.1 Project Description

The Vareš Mine is comprised of the polymetallic underground Rupice Mine, the Vareš Processing Plant (VPP), Veovaca TSF and associated infrastructure, as well as a 24.5 km haul road which connects the Rupice Mine to the VPP.

5.1.1 Rupice Mine

The Rupice Mine (Figure 5-1) is an operating underground mine constructed on a greenfield site. The mine consists of several terraces that accommodate the three underground mine access portals, two production declines and one ventilation return airway decline. Stockpiles are required for management of run-of-mine (RoM) and waste rock. Using front-end loaders, the RoM is deposited from the stockpiles to the ore bins for crushing. A three-stage crushing process is in place above ground at the Rupice Mine. The crushing circuit will also be used to crush waste rock for the use of backfilling, when needed. The crushed ore is then transported to the VPP via the 24.5km haul road. A proportion of the tailings produced at VPP will be transported from the VPP to Rupice Mine for use in backfill operations. Waste rock generated as part of the mining activities at Rupice is stored in a waste rock dump on surface, or crushed and used as backfill underground.

A program of ARD/ML test work was undertaken on 34 samples of Rupice deposit lithologies as part of the 2022 ESIA (WAI, 2022). Results of the geochemical testwork and field trials indicates that the sulphidic ore material is likely to produce acid rock drainage, low pH and metal leaching, while the partially mineralized hangingwall and footwall sediments (HWMISED and FWMISED), which comprise an envelope around the orebody are expected to be mildly reactive lithological units and potentially acid generating (PAG). The remaining hostrock units are unlikely to generate acid given the high carbonate content and neutralizing capacity. These materials naturally buffer potential localised acid production but even in alkaline conditions can still show metal leaching at reduced levels. Operationally, waste is classified as non-acid-generating (NAG) or potentially acid generating (PAG) as it is brought to surface and stored appropriately. PAG waste is being temporarily stored on the ore stockpile until a permanent facility has been constructed.

5.1.2 Vareš Processing Plant

The VPP (Figure 5-2) is situated in the village of Tisovci and is a brownfields site. The VPP has been constructed within the footprint of a historic processing facility that serviced the Veovaca open pit mine, which operated until the late 1980s. The previous buildings and concrete structures were demolished and repurposed to accommodate the VPP. Ancillary infrastructure at VVP includes a laboratory, reagent storage, administration buildings, concentrate storage, security, warehouse, laydown areas and the rail loadout facility. The old tailings facility associated with the historic processing facility remains within the concession area.

A conventional process plant has been constructed for the production of the Pb and Zn concentrates, namely a three-stage crushing and ball-milling followed by Pb flotation and Zn flotation (AMC Consultants Pty Ltd, 2023).

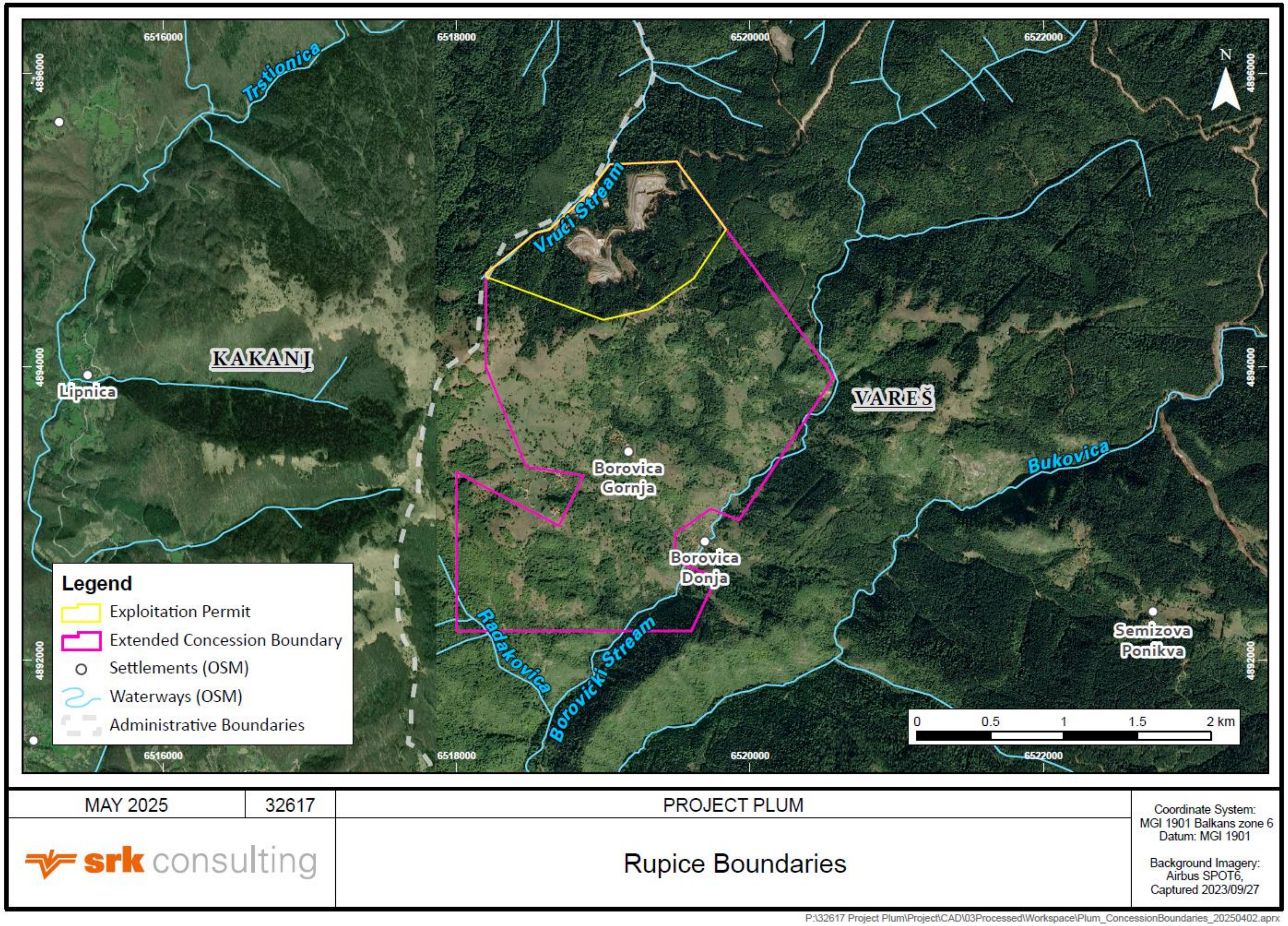


Figure 5-1: Setting of Rupice Mine

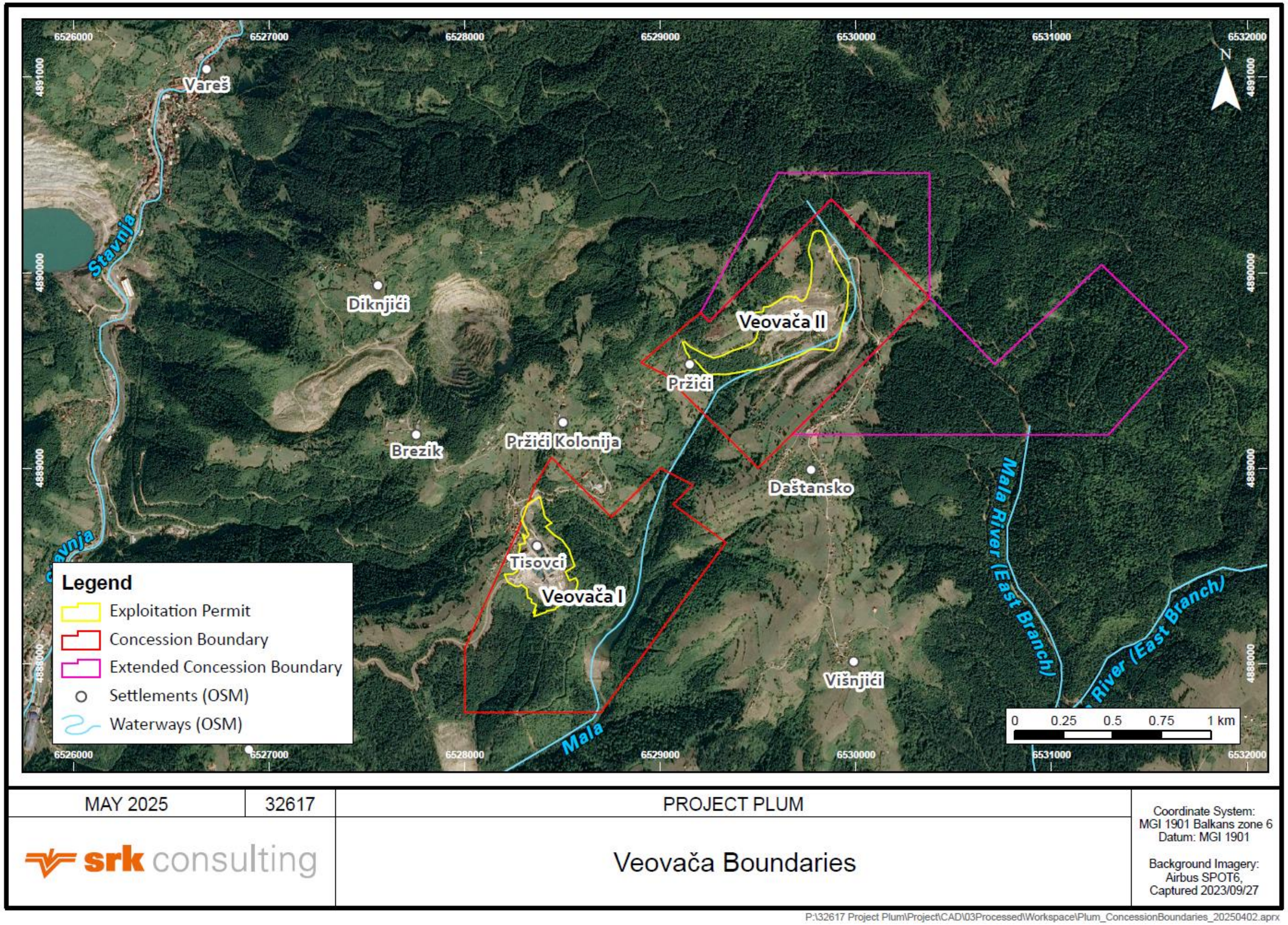


Figure 5-2: Setting of VPP

5.1.3 Veovaca TSF

The tailings that are produced as part of the ore processing and are not required for backfilling will be stored on surface at the Veovaca TSF. The Veovaca TSF is currently being constructed within the historic Veovaca open pit and has been designed as a filtered stack. The tailings have been classified as potentially acid-forming, with the potential to leach metals and sulphides if exposed to atmospheric conditions. The TSF is lined to prevent leaching that may lead to groundwater contamination. Contact water from the Veovaca TSF will be collected in a catchment pond at the toe of the TSF embankment and fed back to the VPP for reuse. The facility will be progressively closed and capped with an impermeable clay layer overlain by waste rock before being covered with topsoil to encourage natural vegetation growth.

As the mine commenced operating and processing ore prior to construction of the Veovaca TSF (refer to Section 4.4), a temporary TSF was developed immediately north of the VPP. The Temporary TSF is lined and the tailings material will be relocated to Veovaca once the new TSF is completed (WAI, 2022).

5.1.4 Haul Road

A 24.5km haul road has been developed to connect the Rupice Mine to the VPP and VPP to the rail loadout. Haul trucks use the route to transport crushed ore from the Rupice Mine to the VPP, as well as transport tailings from the VPP back to the Rupice Mine, which will form part of the paste backfilling.

The haul road utilises 9km of existing roads and forest tracks. In addition to this 15.5km of new roads have been constructed for the sole purpose of connecting the Rupice Mine to the VPP. The haul road has been constructed and owned by the Municipality of Vareš. This road will be multipurpose and will be utilised by the Vareš Mine, the forestry industry, as well as the general public.

5.1.5 Local Resources and Infrastructure

Power Supply

Electricity is supplied to the project via the national grid, which is owned and maintained by a state-owned company, JP Elektroprivreda BiH. An existing and historic 35kV line from the town of Vareš, will feed into the 35kV/6kV substation at VPP. This existing line also provides power to nearby villages, as well as the Veovaca open pit. JP Elektroprivreda provides power via a buried cable along the haul road to the Rupice Mine. Solar panels have been installed on the roof of the administration building.

Water supply and management

The following water sources are available for the Rupice Mine and VPP (Water Management Plan, 2024):

- Rupice Mine: Mrestilište Bukovica (potable quality water), Borovički Potok catchment (process water supply – non-potable) and JKP Vrući Potak (K Series) (process water supply – non-potable).
- VPP: JKP Municipal Water Supply (potable water quality) and recycled contact water

Runoff from the waste rock dump, stockpiles and paste plant is diverted into a lagoon that is fed through the water treatment plant and then discharged off-site as low grade water. Runoff from other area of the site is diverted to drainage channels around the periphery of the site and TSF, and released downstream into the Mala River Catchment (VPP) and Vrući Potak catchment (Rupice Mine).

Waste Disposal

Hazardous waste is stored on site in a hazardous waste warehouse and is disposed of by a licensed disposal company. Non-hazardous waste is separated and stored based on the type of waste, and is also disposed of by a licensed operator (WAI, 2022).

5.2 Accessibility

The project is located 50 km north of the capital city, Sarajevo. International flights to BiH operate regularly through the Sarajevo International Airport. The VPP can been accessed via the Sarajevo – Tulza freeway (R444) and secondary sealed road that passes the Tisovci village, to the VPP. The nearest small village to the Rupice Mine is the village of Borovica Gornja. This can be accessed via the R444 and turning west on to the secondary sealed road (R444a) towards the village of Borovica Gornja.

Construction material, equipment and consumables are transported via rail or heavy trucks, either from the point of origin in Europe or via Port of Ploče, located in the Republic of Croatia. A rail line was constructed as part of historic mining activities from the Vareš Mine to the capital of Sarajevo. The final concentrate is transported via the existing railway facility to Port of Ploče in Croatia. Plans are being developed by the government of Bosnia to extend the railway network north of Vareš to connect the line to the main Balkan network (WAI, 2022).

5.3 Environmental and Social Setting

Topography and land use

The Vareš region is located within the central area of BiH, which consists of a succession of ridges and peaks, high plateaux and deep valleys. The Rupice Mine is located within a forest environment on the Zvijezda Mountain, at an altitude of approximately 900 – 1,280m above sea level (asl). The area is dominated by coniferous forest habitat (spruce and fir) growing on siliceous soils derived from the parent and rocks. Some areas of rocky slopes and grassland are also present, with several watercourses.

The VPP is located at an altitude of approximately 1,060m asl to the east of Vareš. The surrounding area is dominated by rural residential communities and small parcels of land utilised for subsistence farming.

Communities

The closest urban centre to the Project is the town of Vareš, with all other surrounding villages classed as rural communities. There are many community centres (villages) surrounding the Rupice Mine, the VPP and the Veovaca TSF (Figure 5-3). Each community centre has an elected leader who liaises with the municipal government on local issues.

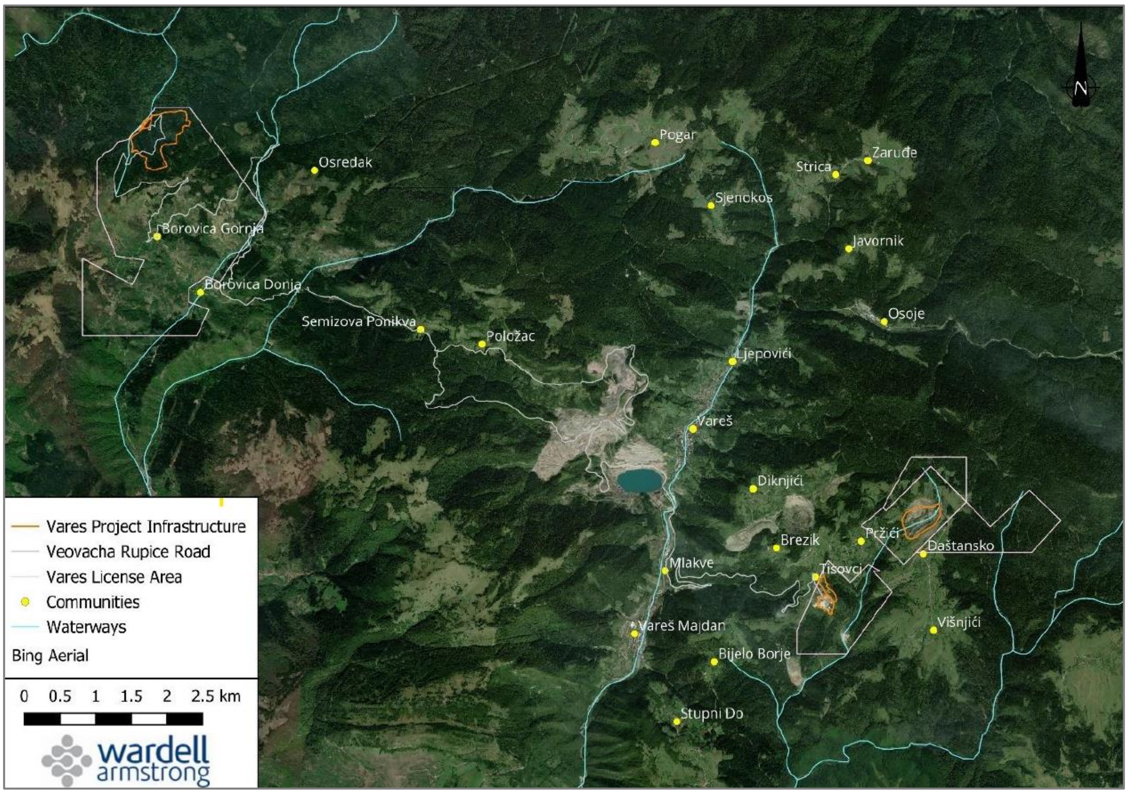


Figure 5-3: Communities surrounding the project

The population within BiH and the Vareš Municipality has seen a steady decline since the Bosnian War (1992-1995). Based on the last census undertaken in 2013, the population decreased from 22,203 in 1992 to 8,892 in 2013. It is understood many of the younger population have moved from the rural villages to Vareš in search of work and social activities, as well as better accessibility to Sarajevo.

Prior to the development of the Vareš Mine, the road infrastructure surrounding the project was in a poor condition with many of the asphalt roads severely weathered and many areas unsurfaced. There is a lack of public transport within the area with many relying on lift shares, taxis and one daily bus service to Vareš.

Climate

The Vareš Mine area is characterized by a humid continental climate. Average monthly temperatures range from approximately 18°C in July to -3°C in January, with extremes of up to 30°C during the summer months (July to August) and as low as -20°C in January. Annual precipitation totals approximately 1,000 mm, with monthly values ranging from 127 mm in June (the wettest month) to 61 mm in February (the driest month). Snowfall occurs on average 48 days per year in the region. At the time of writing DPM had not confirmed the length of the planned operating season.

Climate change is expected to produce increases in monthly maximum temperatures by 1-2°C before 2039, and increase the number of hot days, thus increasing the expected incidence rate of drought and heat waves. Over the LoM, the change in rainfall patterns is expected to be minor. However, in the longer term (2040-2059), precipitation is expected to decrease by 4.2 mm under the RCP 8.5 scenario, though intense rainfall is more likely (WAI, 2022) – this has implications for closure planning.

Hydrology

The project components, including the mining concessions, haul road, processing plant and TSFs, are situated within the Bosna River catchment. The Bosna River is one of the three most significant rivers in Bosnia and Herzegovina, flowing north into the Sava River on the border with Serbia.

Runoff from the Rupice mining area drains to the Vrući Potok, a small mountain stream, which flows in a north north-easterly direction for about 2 km where it joins the Trstionica River (Figure 5-1). The Trstionica River catchment is approximately 161 km² and flows in an approximately south and westerly direction to the Bosna River at the town of Kakanj.

The southeastern boundary of the mining concession sits on the catchment divide between the Trstionica River catchment to the north and west and the Bukovica River catchment immediately to the south and east. The Borovički Stream drains the slopes immediately south-east of the mining concession boundary, flowing south into the Bukovica River, approximately 3 km downstream of the town of Borovica Donja. The Bukovica River flows in an approximately south and westerly direction, joining the Trstionica River at Kraljeva Sutjeska, around 8km upstream of its confluence with the Bosna River at Kakanj.

The processing plant and Veovača TSF are located within the Mala River catchment (Figure 5-2) that flows south to the Stavnja River and onto the Bosna River, joining approximately 30 kilometres upstream of the confluence with the Trstionica.

The haul road crosses the Bukovica River catchments at the Rupice Mine site, the Mala catchment, and a number of other minor watercourses including the Zargarski Stream. The Zargarski Stream flows west from the VPP area towards Vareš Town where it joins the Stavnja.

Surface water flow and quality are monitored in the Borovički and Vrući streams at the Rupice Mine site, as well as at seven locations along the Mala and Trstionica rivers at the process plant and Veovaca TSF. Both the mine site and the processing plant catchments have been significantly impacted by historical mining, as well as some ongoing non-mining activities such as forestry.

Hydrogeology

Two key hydrogeological units have been described at the Rupice mine site; a Jurassic, sandstone aquifer overlying a Triassic dolomitic limestone unit, both dipping approximately to the north. Hydrogeological studies to date suggest groundwater flow in the dolomitic limestone is compartmentalised by cross-cutting faults that can act as a boundary due to low permeability infill and/or displacement of aquifer units, but also as a flow conduit along the brecciated fault margins. Mineralisation is hosted in the Triassic dolomite, which is separated from the overlying Jurassic aquifer by a clay-rich thrust boundary.

Groundwater inflows to the current mine developments are reported to be relatively small other than in areas of major late-stage sub-vertical faulting, which transects the stratigraphic sequence, and from which inflows are reported to be relatively short-lived.

The static groundwater level is approximately 30 to 35 m below ground level at the mine site. Groundwater flow is primarily northward. Groundwater hydrographs show an immediate response to rainfall events, typical of rapid groundwater recharge. At the process plant site, groundwater was encountered near surface in the valley bottoms up to a depth of 21.7 m below ground level on the valley sides, with groundwater flow to south-southeast, following topography.

Baseline groundwater quality at Rupice Mine is characterized by neutral to slightly alkaline pH and a calcium bicarbonate water type, distinct from the more magnesium and sulphate-rich groundwater observed at the process plant site. Monitoring data indicate consistent exceedances of various metals with respect to Bosnian MPC Class I-II guidelines, predominantly due to the historic mining activities in the Mala catchment and the mineralised ore body at Rupice (WAI, 2022).

Biodiversity

The closest protected area to the VPP is the proposed buffer zone of the Zvijezda Mountain, situated 1.1km north of the VPP. The closest protected area to Rupice Mine is the Tajan Natural Monument (IUCN Category 3), which is approximately 6km north of the Rupice concession boundary.

While the project reportedly has no significant impact on protected sites, the VPP, Rupice Mine and haul road are anticipated to have varying levels of impact on habitats listed under the EU Habitat Directive. These habitats have priority biodiversity features (PBF), which are subsets of biodiversity that are particularly irreplaceable or vulnerable, but at a lower priority level than critical habitats, as defined by the EU Habitat Directive. The EU Annex IV yellow bellied toad, Greek frog, green toad and agile frog were found in several watercourses in the region. Aquatic species of conservation concern identified in the project area include stonefly (nationally vulnerable), stone crayfish (nationally vulnerable). White-claw crayfish (EU Annex II, IUCN and nationally endangered) were identified in the Mala River catchment downstream from VPP and Veovaca TSF. Horseshoe bats (nationally endangered) were also identified (WAI, 2022).

A new proposed protective area was identified to establish suitable areas and programmes for ensuring the biodiversity offset is met for Project related impacts. The chosen area is to the north and east of the Rupice Mine site and spans 110 ha. The status of this area and formal approval by regulatory authorities is not specified in the documents reviewed.

Cultural heritage

Mining has been undertaken in the Vareš area since the Bronze Age (9th- 8th century BC), with known activity also during the Roman era (AD 9-10 – 395). Modern mining was initiated in 1878 with evidence of this scattered across the landscape in the form of abandoned open pits, waste dumps and mine shafts.

Due to the location of the Vareš Municipality, there are strong ties to the Bosnian War (April 1992 – December 1995), as there were three forces located nearby. Due to the war, many settlements have been left uninhabited. War memorials and cemeteries linked to the war are found throughout the region.

There are no World Heritage Sites or receptors of high sensitivity located close to the project. Eight designated cultural heritage assets are located within Vareš Municipality but none in close proximity to the Project. The fortified medieval castle of Bobovac is located 6.5 km south east of the Rupice Mine and 5 km from the haul road, and is unaffected by the project.

ITEM 6. HISTORY

6.1 Ownership

Modern exploration was commenced in the late 1940s by Energoinvest, a parastatal exploration and mining company, some mining was conducted which was discontinued in the late 1980s.

In March 2013, Energoinvest's Concession at Vareš was auctioned and acquired by MM Project d.o.o which subsequently changed its name to Eastern Mining d.o.o. which was acquired by ADT in September 2017.

On 12 March 2013, a Concession Agreement for exploration and exploitation of metallic resources lead, zinc and barite No. 04-18-21389-1/13 (later amended to include silver and gold) was issued the Ministry of the Economy which was a prerequisite for approval of 3 exploration licenses:

- Rupice-Juraševac-Brestic (RJB);
- Veovača I; and
- Veovača II.

These licenses are defined as an exploration area and have an overlying exploration permit granted by the Ministry of Energy, Mining and Industry.

Additional information is provided in Item 4.4.

6.2 Exploration History and Status

Early reports dated 1870-1886 from the Austrian- Hungarian occupation refer to the lead-zinc deposits. General descriptions of the geological structure and mineralization are variously reported in publications dated between 1900 and 1929. Mining is generally understood to have taken place in the area historically.

Significant exploration commenced after 1945; and modern systematic exploration started in the early 1960s through Energoinvest.

Detailed exploration at Rupice itself commenced in the 1960s through development of exploration adits and drives followed by a substantial program of trenching and diamond core drilling in the 1980s. Trenches have not been used in the MRE.

Drilling in the Rupice area can be summarised as follows:

- 1980-1990: 49 Energoinvest diamond drillholes were used to inform an early MRE; these were drilled to less than 200m below surface
- 2012: an additional 7 historical drillholes were captured in a digitisation exercise
- June 2017 to December 2018: ADT undertook infill and extension diamond drilling some twins of historical drillholes
- 2019: ADT completed 49 extension diamond drillholes which informed ADT's 2020 Mineral Resource estimate for Rupice Main zone
- 2021: ADT completed 31 infill diamond drillholes
- 2022: ADT completed 66 drillholes some of which were in Rupice North West zone

– 2023: ADT reported 44 diamond drillholes to infill, extend and regularise coverage in the North West zone

6.3 Previous Mineral Resource Estimates

6.3.1 Rupice

The most recent historical Mineral Resource statement for Rupice was issued jointly by AMC and ADT on 14 March 2025 and presents an MRE statement that is depleted to 31 December 2024. This estimate was superseded by the QP's estimate and is therefore no longer deemed relevant by the QP. The QP's Mineral Resource estimate is presented in Item 14.

Table 6-1: 31 December 2024 AMC & ADT Historic Mineral Resource Statement for Rupice

Mineral Resource	Tonnage (Mt)	Ag (g/t)	Zn (%)	Pb (%)	Au (g/t)	Cu (%)	Sb (%)	BaSO4 (%)
Indicated	18.4	164	4.7	3	1.2	0.4	0.2	30
Inferred	2.5	67	1.7	1.3	0.4	0.2	0.1	13
Total	20.9	153	4.3	2.8	1.1	0.4	0.2	28

The historical statement was reported using the JORC Code and was authored jointly by two Competent Persons: Sergei Smolonogov from ADT and Dmitry Pertel from AMC. The historical statement includes barite which was considered as a potential source of revenue in the DFS. This has not been realised to date.

The historical statement uses a 50 g/t silver equivalent cut-off grade based on parameters stemming from work completed in 2020. This cut-off grade has been superseded, presented in Item 14.11.1.

The QP removed barite and used a net smelter return cut-off value (based on current metal prices and technical-economic forecasts) to report the current Mineral Resource statement given in this document. Refer to Item 10.3.4 for details as it relates to datasets included within this estimate.

6.3.2 Veovaca

Historically, ADT stated a 7.4 Mt polymetallic Mineral Resource for the Veovaca project. The QP has not done sufficient work to classify the historical estimate as current mineral resources or mineral reserves, and DPM is not treating the historical estimate as current mineral resources or mineral reserves.

The deposit is in the same mineralised belt some 12 km southeast of Rupice near the Vareš processing facility. The deposit was mined historically in a small open pit. However, the historical pit and immediate surrounds, at the time of writing, are destined to be used for tailings storage which in the QP's opinion sterilises the deposit as a potential open pit project. No studies have been undertaken to assess its economic potential as an underground project. It is therefore no longer reasonable to assume this can be mined economically and Veovaca has therefore been removed from the QP's current Mineral Resource statement given in this document.

6.3.3 Droskovac - Brezik West

A historical, locally reported resource of 887,000 t @ 3.9% Pb+Zn is quoted by ADT. The QP has not done sufficient work to classify the historical estimate as current mineral resources or mineral reserves, and DPM is not treating the historical estimate as current mineral resources or mineral reserves. This area is due to be drilled according to ADT's exploration budget as covered in Item 9.2.1.

6.4 Previous Mineral Reserve Estimates

The 2025 Vareš Mine estimate of Mineral Reserves was prepared following previous published estimates in 2021 (Ausenco), 2023 (AMC) and 2024 (AMC).

Table 6-2: July 2021, Ausenco DFS Mineral Reserve estimate

Ore Reserve	Tonnage (Mt)	Zn (%)	Pb (%)	Cu (%)	BaSO4 (%)	Au (g/t)	Ag (g/t)	Sb (%)
Proved	-	-	-	-	-	-	-	-
Probable	7.29	5.72	3.59	0.61	32.36	1.88	202.03	0.23
Total Ore Reserve	7.29	5.72	3.59	0.61	32.36	1.88	202.03	0.23

Table 6-3: 10 October 2023, AMC Rupice Ore Reserves

Ore Reserve	Tonnage (Mt)	Ag (g/t)	Zn (%)	Pb (%)	Au (g/t)	Cu (%)	Sb (%)
Proved	-	-	-	-	-	-	-
Probable	13.8	187	5.2	3.3	1.4	0.5	0.2
Total Ore Reserve	13.8	187	5.2	3.3	1.4	0.5	0.2

Table 6-4: 31 December 2024, Adriatic 2024 Rupice Mineral Reserves Update

Mineral Reserve	Tonnage (Mt)	Ag (g/t)	Zn (%)	Pb (%)	Au (g/t)	Cu (%)	Sb (%)
Proved	-	-	-	-	-	-	-
Probable	12.3	192	5.7	3.6	1.5	0.5	0.2
Total Ore Reserve	12.3	192	5.7	3.6	1.5	0.5	0.2

The QP highlights notable changes between successive Mineral Reserves estimates as follows:

- 2021 to 2023 – inclusion of Rupice North West Mineral Reserves;
- 2021 to 2023 – exclusion of barite ($BaSO_4$) from the suite of revenue generating minerals;
- 2023 to 2024 – depletion of 2024 ore mined; and
- 2023 to 2024 – increase of NSR cut-off grade from USD 68/t to USD 130/t.

The QP did not do sufficient work to classify the 2021 and 2023 estimates as current Mineral Resources or Mineral Reserves, and DPM is not treating these historical estimates as current Mineral Resources or Mineral Reserves. The QP re-estimated the Mineral Reserve, which is presented in Item 15.2.

6.5 Historical Production

The Vareš Mine was officially opened on 5 March 2024. Underground development commenced in 2023 with some 1.5 km developed and 3 km developed in 2024, to provide access to the deposit. The first stope was opened in August 2024.

The first sale of on-specification grade concentrates was in May 2024, via the port of Ploče. Concentrates have been sold and shipped to European smelters and beyond. ADT's 2025 (Corporate Presentation, 17 February 2025 https://www.adriaticmetals.com/wp-content/uploads/2025/05/Adriatic-Metals_Corporate-Presentation_17.02.25.pdf) guidance was 625 kt to 675 kt milled producing 12,000 koz to 13,000 koz AgEq. Full production mining rate as per the latest feasibility study is 850kt run of mine per annum. Concentrate and metal production will vary as the run of mine grade varies. The QP notes that DPM production ramp up to full production is delayed due to its change in mining method and Integration Plan, which addresses risks and recommendations highlighted in this Technical Report.

The historical production figures are presented in Table 6-5. The 2024 production figures have been sourced from ADT's March 2025 presentation. The 2025 production figures have been sourced from ADT's Operations Update dated 31 March 2025. These are public reports.

Table 6-5: Historical Production

		Q2 2024	Q3 2024	Q4 2024	FY 2024	Q1 2025
Mining						
Ore mined	(kt)	8	63	73	146	67
Processing						
Ore milled	(kt)	9	19	47	76	66
Head grade						
Ag	(g/t)	96	239	234	217	n/a
Au	(g/t)	0.6	2.6	2.6	2.3	n/a
Zn	(%)	2.2	8.6	7.5	7.1	n/a
Pb	(%)	1.6	5.6	4.8	4.6	n/a
Recoveries						
Ag	(%)	76	85	94	90	n/a
Au	(%)	45	65	74	71	n/a
Zn	(%)	29	56	63	60	n/a
Pb	(%)	59	55	68	64	n/a
Concentrate Production						
Ag/Pb concentrate	(kt)	0.3	1.4	3.8	5.5	n/a
Ag	(g/t)	2,322	2,131	2,185	2,177	n/a
Au	(g/t)	7.2	13.6	14.1	13.7	n/a
Pb	(%)	32.9	41.3	41.1	40.8	n/a
Zn concentrate	(kt)	0.1	2.1	4.8	7.1	n/a
Ag	(g/t)	602	411	427	425	n/a
Au	(g/t)	5.1	5.8	7.3	6.8	n/a
Zn	(%)	44.9	44.4	46.2	45.7	n/a
Metals Contained						
Ag	(oz)	21,722	126,376	333,148	481,245	n/a
Au	(oz)	81	1,021	2,859	3,961	n/a
Zn	(t)	58	931	2,238	3,226	n/a
Pb	(t)	85	594	1,561	2,240	n/a
AgEq	(Moz)				0.9	1.3

6.6 Change from Historical Production Plan

DPM has created a new mine plan that forms the basis of the Mineral Reserves presented in this Technical Report. After the Transaction is completed, DPM plans to maintain the DFS target production rate of 850 kt and will action an Integration Plan which transitions from the ADT life of mine plan to DPM's life of mine plan.

ITEM 7. GEOLOGICAL SETTING AND MINERALISATION

7.1 Regional Geology

The Vareš Mine is situated centrally within the Dinarides deformation belt which runs southeasterly over several hundred kilometres east of and parallel to the Adriatic coastline from Slovenia to Albania.

Generally, the geology comprises Jurassic and Cretaceous carbonate and flysch sediments and Paleozoic volcanogenic-sedimentary formations. These are deformed into southwest-verging nappe folds and stacked by northeast-dipping thrust faults.

Figure 7-1 illustrates the scale of the belt, the general geological arrangement and the location of the project.

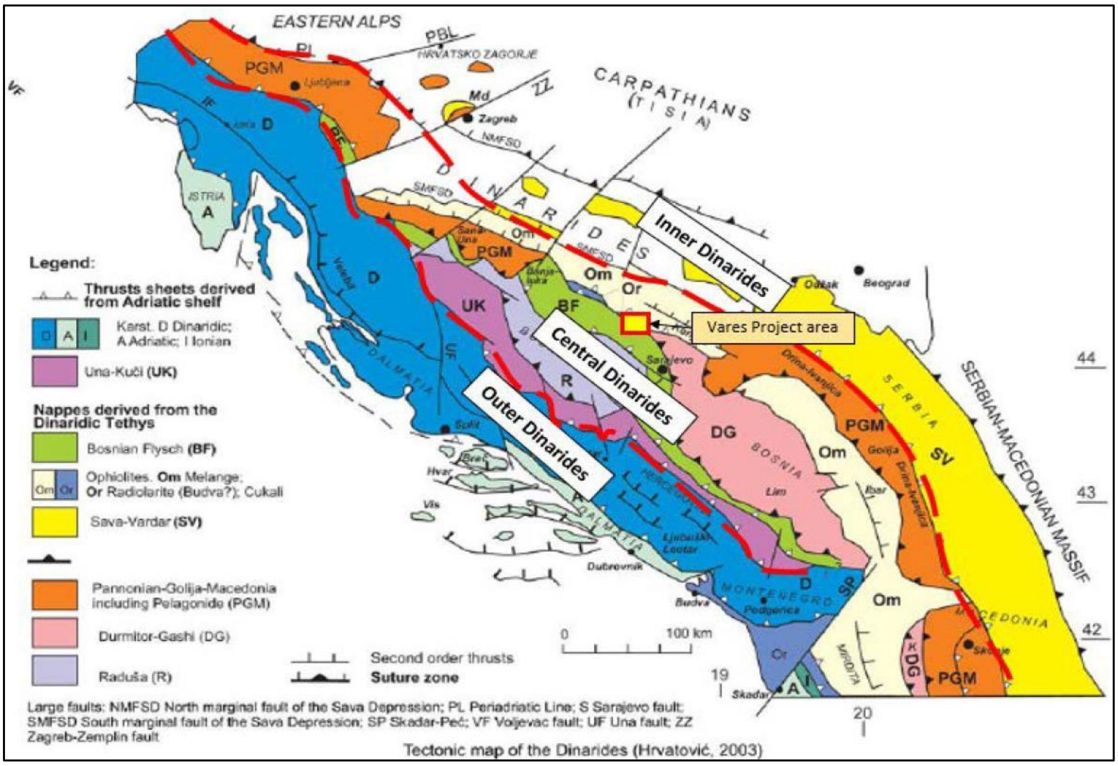


Figure 7-1: Regional Geology (after Hrvatović, 2003)

7.2 Project Geology

7.2.1 Stratigraphy and Lithology

The stratigraphy and structure at Rupice were summarised by Marjoribanks, 2018; his work and subsequent additions by ADT and their consultants are summarised below.

The stratigraphy in the Rupice mine comprises:

- Upper sequence of Jurassic dolomites and marls (project codes SLS and SMR) with a thrust fault defining the lower contact
- Upper Triassic dolomite flysch-melange with silicic and iron-rich alteration developed at its base (Massive Red Rock - MRR)

– Middle Triassic interbedded dolomite, tuff and shale (project codes SCH, FAC, GYD and SLD) including Ladinian chert and Anisian limestones-dolomites
  - strong bedding-parallel tectonic foliation in the pelitic rocks and clay filled styolites are present in the carbonate rocks
  - stratabound massive barite and sulphide lens with associated veining occur towards the base of the unit
  - laminated iron-rich altered dolomite occurs below the massive sulphide
– Lower Triassic siliciclastic turbidite comprising, chert, tuff, siltstone and sandstone (project code SST)

The geological context of the mineralisation is illustrated in Figure 7-2 in which Marjoribanks shows

– the general dip of the mineralisation which is moderate towards the northeast
– the surrounding stratigraphy dominated by carbonates
– the prevalence of strata-parallel thrusts and associated steeper linking thrusts
– the original lens geometry subsequently affected by deformation

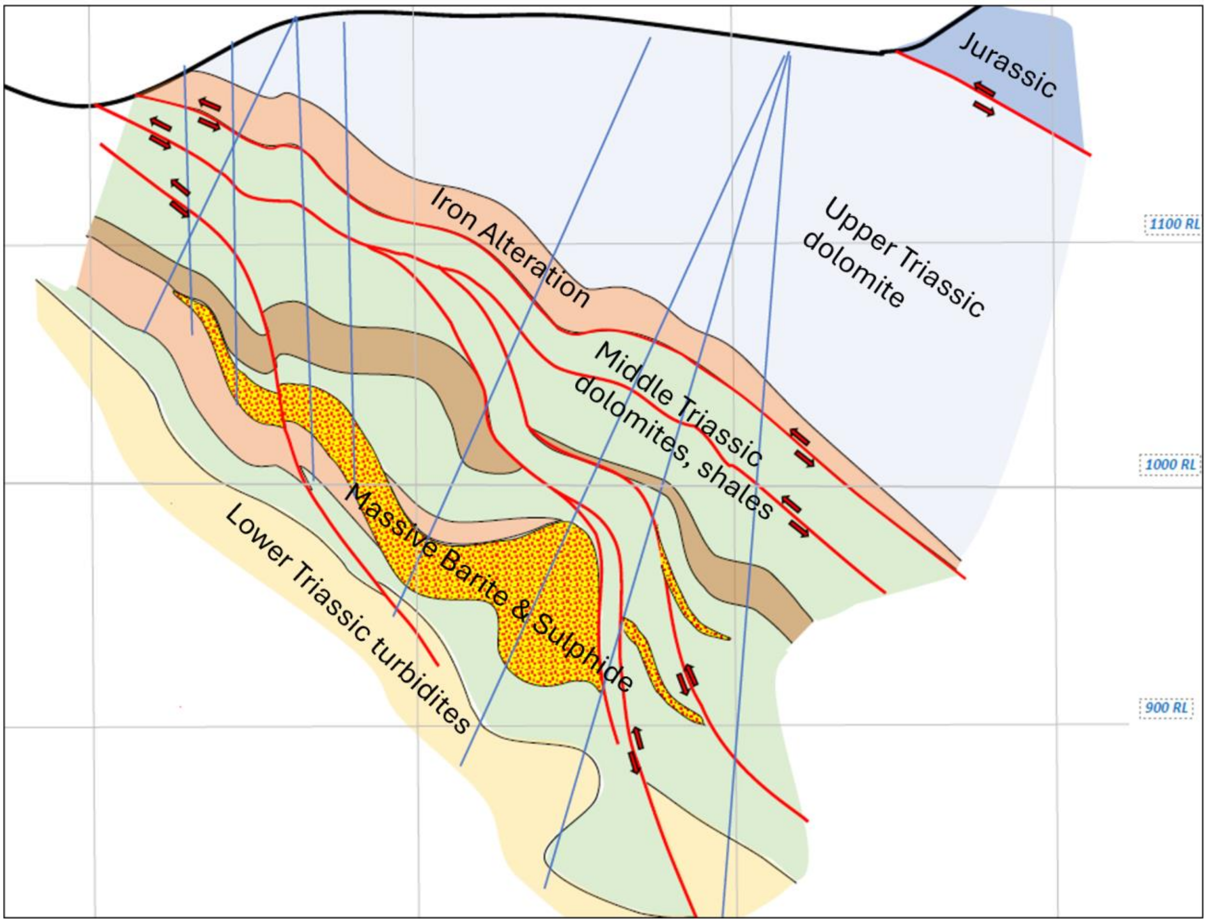


Figure 7-2: Cross Section Looking Northwest (modified from Majoribanks, 2018)

7.2.2 Mineralisation Style

Barite and base metal massive sulphides were originally deposited in a single layer of lenses which were conformable with the enclosing bedding.

Barite is thought by the ADT geology team to have originally formed a cap over the other base metal sulphide layers. The QP agrees this would be in keeping with observations at other similar deposits; also it is clear that barite grades tend to be highest in the stratigraphically higher part of the Rupice deposit.

Copper, lead, zinc and gold grades tend to be highest in the middle part of the mineralised package corresponding with the highest sulphur grade and density values. Iron grades tend to be more elevated towards the base of the package. Silver grades tend to be elevated both at the top and bottom parts of the package with lower grades sometimes distinctly evident in the central part.

The QP has prepared an illustration of the metal distributions using Section 5075 N in Figure 7-3 (each frame is 200m high by 3400m wide).

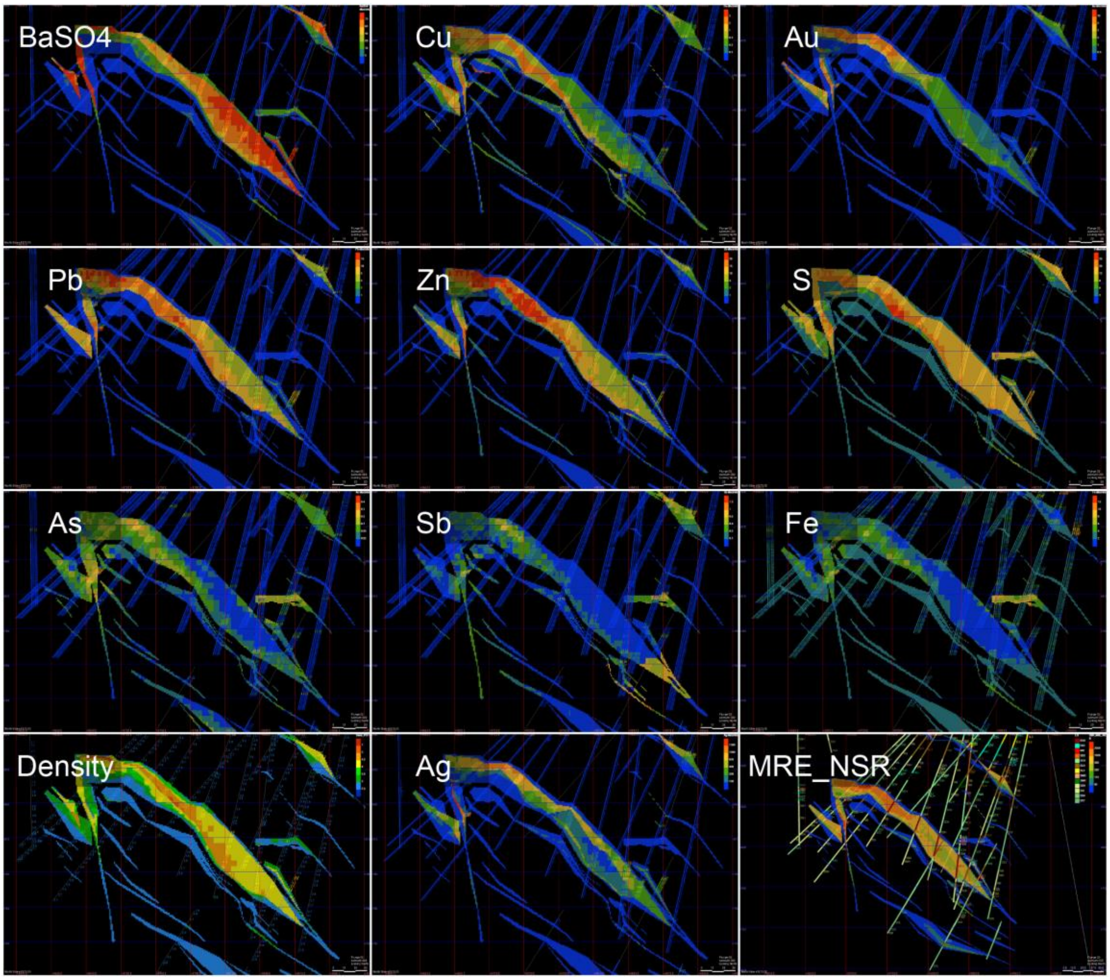


Figure 7-3: Metal Distribution

The mineralisation geometry was subsequently modified by thrust displacement and associated folding pinching and swelling resulting in shapes such as depicted in Figure 7-2 which were observed at a smaller scale by the QP in the exposed parts of the mineralisation in stopes and in drill core. This later event caused alteration, recrystallisation of barite and sulphides and it seems likely that there was some remobilisation causing sulphides to migrate towards fold hinges.

Steep faults formed imbricate ramps that wrapped around the silicified ore mass which resulted in deterioration of rock mass quality and increased clay alteration of shales and tuffs in the surrounding host rock.

7.2.3 Mineralogy

The mineralisation is characterised by abundant barite (BaSO4) with base metal sulphides, mainly comprising

- sphalerite ((Zn,Fe)S)
- galena (PbS)
- minor bournonite ($PbCuSbS_3$)
- chalcopyrite ($CuFeS_2$)
- pyrite (FeS_2),
- minor tetrahedrite ($(Cu,Fe)_{12}Sb_4S_{13}$),
- rare stibnite (Sb_2S_3) and
- rare cinnabar (HgS)

The gangue is dominated by calcite, dolomite and siderite with some tuffs and sediments which have sometimes altered to clays.

ITEM 8. DEPOSIT TYPES

8.1 Geological Setting

The geological setting is a very large-scale deformation belt within which Jurrasic, Triassic packages dominated by carbonates and volcano-sedimentary shelf sediment have been thrusted and folded. At Rupice, the Triassic sequence contains layers of iron alteration and one layer in which massive sulphide mineralisation was deposited.

8.2 Style of Mineralisation

Genetically, the deposit is associated with a shelf zone where volcanic activity generated hydrothermal processes that allowed the scavenging of metals from surrounding crustal material and delivery of this into the submarine environment resulting in formation of a Volcanogenic Massive Sulphide (VMS) deposit with associated breccia-hosted mineralisation. Globally, VMS deposits typically include base metals such as copper, zinc, lead and sometimes gold and silver.

The Kuroko sub-type VMS deposits are associated with gypsum (CaSO4) overlying massive sulphides, potentially equivalent to the barite (BaSO4) which is abundant at Rupice and arsenic-antimony bearing sulphosalts such as bournonite-tetrahedrite-stibnite observed in Rupice.

ITEM 9. EXPLORATION

9.1 Summary of Work Undertaken

The topographic surface in and around the mine site was based on a LiDAR survey undertaken by Hansa Luftbild of Germany to a better than 5 cm accuracy. The survey was undertaken in mid-September 2018.

Given that DPM does not yet hold the property, DPM has not conducted any relevant exploration. The exploration described in this section is work conduct by or on behalf of ADT. The QP has not reviewed reports and data pertaining to the historical exploration work referenced in this section.

9.2 Ongoing Exploration in the Belt

In addition to the mine geology team, ADT has a team dedicated to exploration in their concessions along the same geological belt that hosts Rupice and Veovaca. Figure 9-1 shows Rupice, the current operating mine, towards the western end of ADT’s ground.

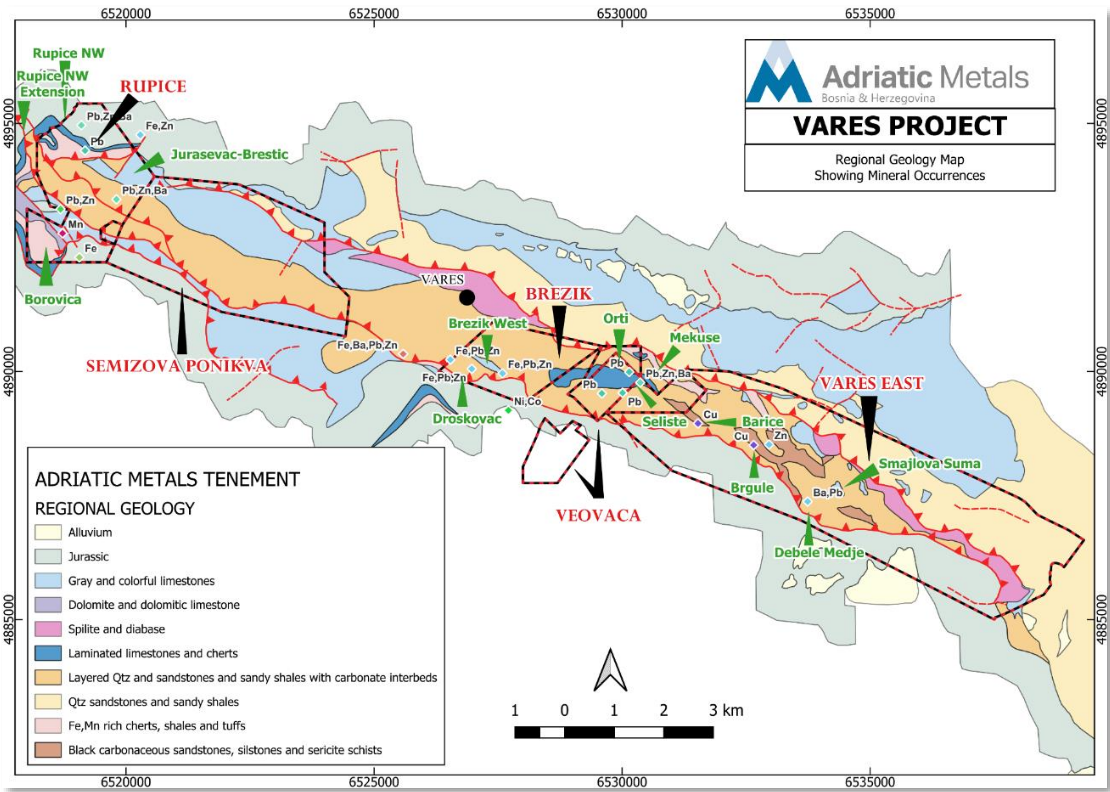


Figure 9-1: ADT Exploration Concession Map

Vareš and Veovaca which are near ADT’s mineral processing facility are in the centre of the concession area. A 10km stretch of concession follows the shear zone towards the eastsoutheast; overall ADT has exploration concessions covering most of a 25km length of the geological belt that hosts Rupice.

There are many locations along this belt where base metal and precious metal mineralisation have been identified in the same or similar stratigraphy as the Rupice deposit.

The map shows a number of exploration project areas for which a USD 5 million budget is in place, most notably:

9.2.1 Copper Rift (USD 2.3 million)

Five targets have been defined along a 4km mineralised corridor in the Vareš East concession (Figure 9-2) where some trenching and 6,800m of scout drilling in 34 drillholes is planned in 2025. This is based on a mid-1980s induced polarisation ("IP") geophysics survey and a more recent coincident geochemistry anomaly resulting from a 50m x 50m soil sampling survey. In the Grubanovici and Barice areas, mapping and sampling along traverses discovered barite and sulphide mineralisation in some areas from which grab samples were taken and assayed returning grades ranging from anomalous to ore grade.

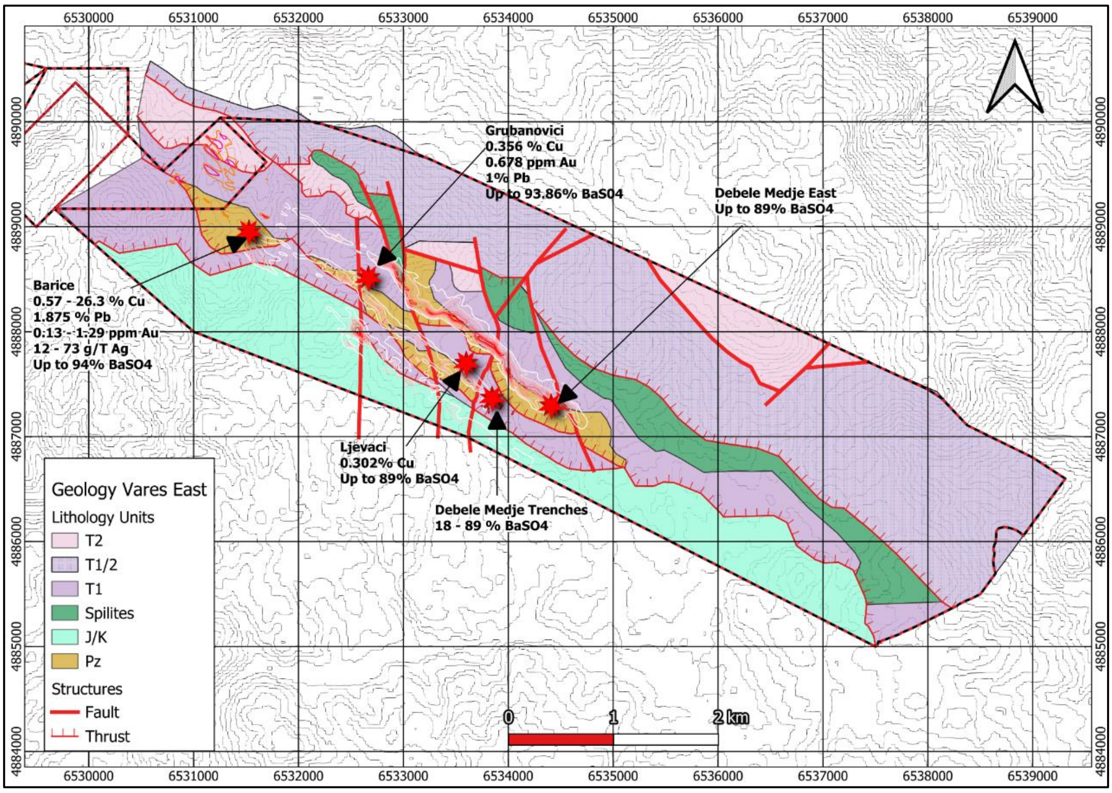


Figure 9-2: Vareš East 4 km Exploration Target Area

9.2.2 Droskovac and Brezic West (USD 1.9 million)

There is a historically reported mineral occurrence (historically mined underground for iron ore at Droskovac and by open pit at Brezic) in the west part of the Brezik concession. Some 3,500 m of drilling is ongoing and planned in 2025 to follow up on base metal in soil anomaly WNW of the Brezic open pit (Figure 9-3) with the objective of advancing towards a modern maiden Mineral Resource estimate at Droskovac and Brezic West.

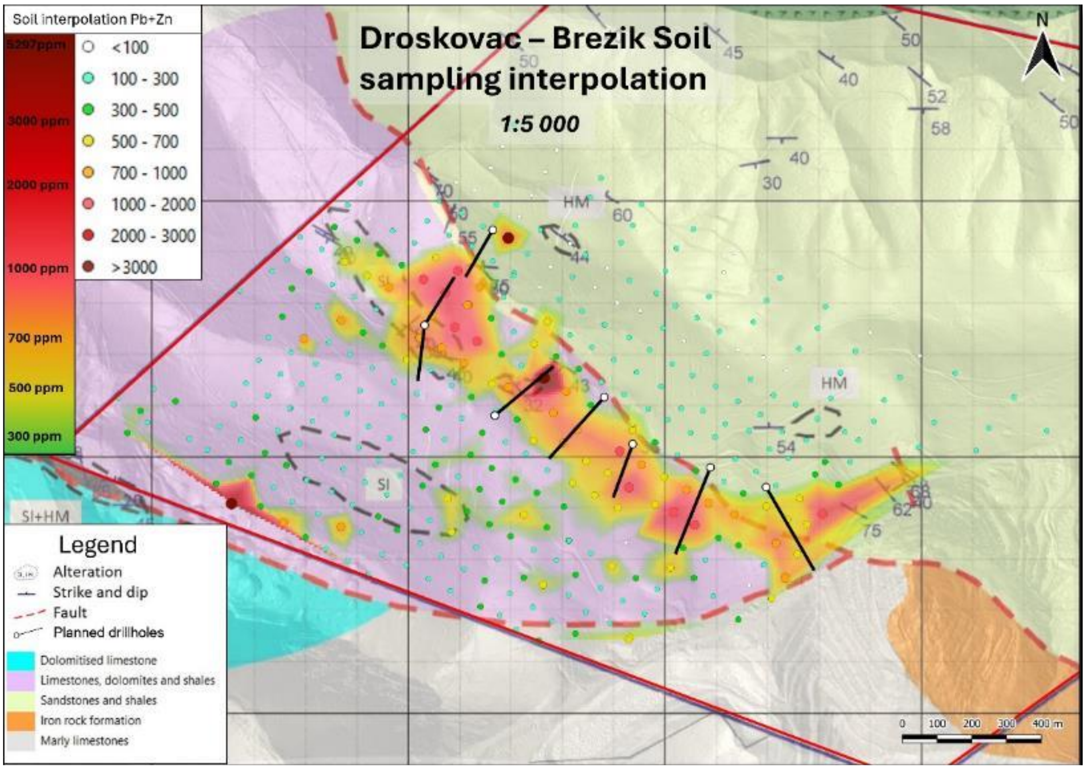


Figure 9-3: Droskovac - Brezic West Exploration Area

Historically, drilling samples were assayed for iron and base metals but precious metals were not assayed. A historical resource is reported by ADT which the QP did not review, however, the area does seem to present an encouraging drill target where base metals associated with iron may be suggestive of the mineralisation style at Rupice. Historical mining voids and land access could present challenges according to ADT.

9.2.3 Selište and Mekuse (USD 0.95 million)

Also in the Vareš East concession, drilling in 1970 reportedly intersected up to 50m-wide zone averaging 2-4% Pb and Zn grades at Selište. Some 3,000m of scout drilling is proposed for 2025 to test the 400m-long IP anomaly from work conducted in the 1980s and ADT's 2024 channel SECH-001 which confirmed economic grades at surface some 210m east of Veovaca open pit.

Whilst this presents another attractive drilling target, it is reportedly close to Daštansko village and also it is unclear how the proposed deposition of tailings in the old Veovaca Pit might affect exploration access or future mining.

The area to the north of Makuse is likely prospective based on northwestward extension of the IP survey anomalies which link down to Barice in the southeast; and based on lead-in-soil anomalies shown in ADT literature. The QP understands that ADT has applied for an extension to the concession area to capture this area.

9.2.4 Rupice West

Following up on a gravity anomaly and coincident soil anomaly some 800m southwest of the Rupice mine; ADT plans to continue ongoing target delineation work infilling soil samples to a 50m grid, mapping and sampling in the area.

Earlier drilling is thought to have missed the source of the gravity anomaly ADT hopes to improve geological understanding and targeting during 2025 ready for additional drill testing in 2026.

9.2.5 General Opportunities

In addition to these scheduled work programmes there is a general ongoing prospecting effort in all concession areas. The ADT geology team has sampled and mapped mineralised outcrops throughout their concessions, particularly in Vareš East. However some areas are currently inaccessible until the planned surveying and clearing of unexploded ordnance and landmines is completed, which is expected to be in 2026.

There is an attractive opportunity if a new concession area can be secured to the northwest of the existing concession areas where the Rupice deposit model terminates at the concession boundary and remains open at depth beyond the boundary. However the ground to the northwest is in a different municipality and it is uncertain if or when it will be possible to undertake exploration work there. Community engagement is ongoing as described in Section 20.2.4.

ITEM 10. DRILLING

10.1 Introduction

Drilling at Rupice commenced in the 1980s when Energoinvest held the concession; after a long paused in activities, ADT took control of the asset in 2017 since when the majority of drilling data available today was generated. The majority of drilling used large diameter core triple-tube core barrels and drilling muds to maximise core recovery and quality.

In summary, the current MRE model is based on 469 diamond drillholes comprising:

- 49 Historical drillholes for 5,691 m
- 420 ADT surface drillholes for 101,162 m

The QP is satisfied that these have:

- appropriate downhole survey records (for longer inclined drillholes)
- appropriate geological logging
- 18,693 density determinations
- mostly continuous sampling for multi-element assaying through the mineralised zone and surrounding host rock, including assays for the following key metals:

Element	Zn	Pb	Cu	Au	Ag	Sb	S
Number of Assays	42,149	42,130	41,360	41,334	41,395	41,288	41,231

10.2 Historical Drilling

Historical drillholes comprise less than 17% of the total number of drillholes used in the MRE.

All historical drillholes were diamond cored from surface using a variety of rigs which included various models manufactured locally to the design of a Longyear diamond core rig. Models include GR-300, GR-500, GR-600, and Janex-600.

All but one of the historical drill pads were located and surveyed by the ADT team.

The holes were drilled vertically, however there were no downhole surveys which is not considered to present a material issue to the MRE model.

All drillholes started with a core diameter of greater than 112 mm and sometimes reduced core size at varying down hole depths to 76 mm.

The core recovery reportedly averaged 83% in mineralisation and 77% in waste.

10.3 ADT Diamond Drilling

10.3.1 2017-2018

Drilling in 2017 was undertaken by S&V Drilling from Bor, Republic of Serbia using a crawler mounted Atlas Copco diamond core rig capable of drilling to depths of 800 m (HQ). Core diameter for the first three drillholes was initially PQ3 reducing to HQ3 to end of drillhole, with the remainder of the drillholes open-holed to average depths of 57 m in 2017 and 98 m in 2018 before being drilled with HQ3 to end of the drillhole.

10.3.2 2019-2021

From mid-2019 and into 2021, drilling was undertaken by GeoAvas (Bosnia) S&V Drilling, and by GIM Geotehnika, then in mid-2021 the drilling contractor was changed to GEOPS-Bolkan Drilling Services Ltd who drilled PQ to 150 m maximum, subsequently stepping down to HQ3 and then NQ for the deepest drillholes.

10.3.3 2022-2023

Drilling in 2022 was undertaken using three diamond drill rigs and crews provided by Drillex International (Drillex d.o.o. as of 1 November 2022). Drillholes were typically large diameter PQ size to a depth of 100 m through barren Jurassic sediments and then reduced to HQ through Triassic sediments and mineralization to end-of-hole. Drillholes varied in depth from 250 m to 350 m. A fourth rig was added in 2023.

10.3.4 Current MRE Estimate

The current estimate includes underground grade control diamond drilling and surface infill, step-out and twin verification diamond drillholes up to September 2024 (excluding 8 drillholes completed in November 2024 for which assay results were pending at the time of populating the block model).

The QP agrees with ADT that the results of the November batch of surface drillholes and the underground grade control drilling completed since that time broadly agree with the current block model and their incorporation would not produce a material change.

10.4 Spacing

ADT strived to achieve diamond drillhole on section lines spaced 40 m apart drilled in fans to achieve a 25 m to 30 m separation between mineralization intersections on the drill sections. Where there is apparent structural influence on mineralization, drillhole intersection spacings were decreased to 20 m on sections locally to allow for better definition of mineralisation.

10.5 Survey

All drillhole collars were located by Total Station (theodolite) with coordinates recorded in MGI 1901 / Balkans Zone 6 - Bosnia Herzegovina projection, to better than 1 cm accuracy. All drillholes were downhole-surveyed using a digital multi shot camera at or around every 30 m downhole. It is noted that the drillholes rarely deviated significantly from their set-up orientation.

10.6 Logging

The ADT team has implemented a consistent and meaningful logging code system which has been applied to historical drillhole logs to ensure all data is compatible.

ADT's lithological logging is conducted at the core farm and the data entered directly into Microsoft Excel via laptops using a geological template to ensure consistency. Geological logging was undertaken to a precision of 0.5 m.

Observations recorded include: oxidation, weathering, grain size, colour, alteration and alteration minerals, oxidation minerals, mineralization, texture, lithology, type of veins, type of breccia, and the log description.

All logging data currently collected on site is directly entered into specific logging laptops and reference logging information is used to ensure consistency, an example of which is shown in Figure 10-1.

The QP has reviewed the simple geological logging codes which provide consistent and comprehensive data which would allow the stratigraphy and host rock types to be modelled in reasonable detail if required.

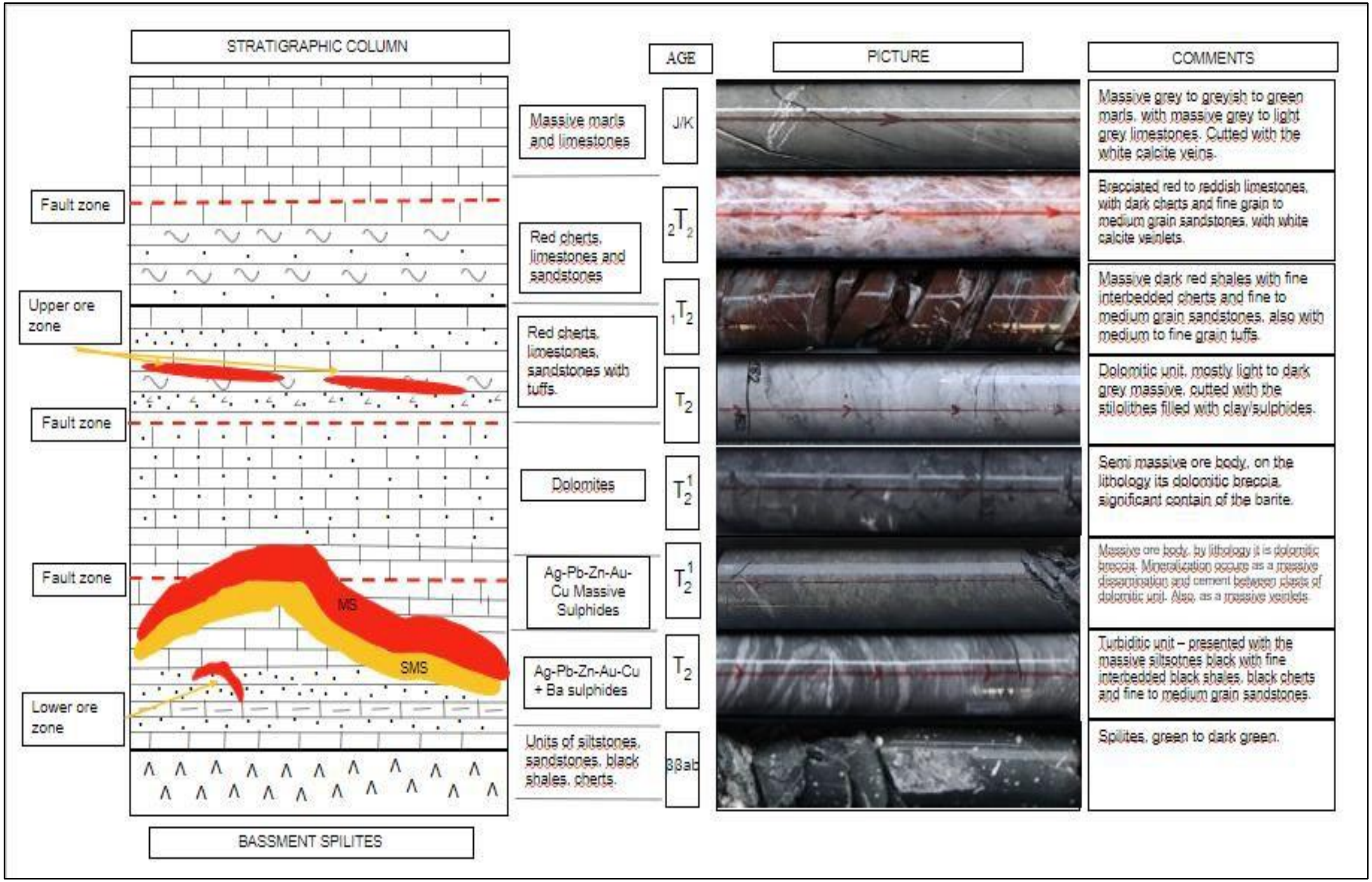


Figure 10-1: Example of logging code reference material

10.7 Recovery

Core recovery and RQD have been recorded consistently. The QP assessed all drillhole intervals withing broad intervals exceeding 100 g/t Ag and found the average core recovery affecting the MRE to be close to 97%.

10.8 Sample Storage

All core was collected in heavy-duty plastic core trays and marked with Hole ID, box number, and “from” and “to”. A plastic marker placed in the core tray marks the driller’s depth determination.

Core is securely stored in ADT’s warehouse located at the Ljepovici core farm.

ITEM 11. SAMPLE PREPARATION, ANALYSES AND SECURITY

11.1 Overview

Different laboratories have been used over the years. Information here has been compiled by ADT and its consultants. The QP has summarised findings previously reported by ADT's QPs and presents a summary of their report details here. The QP has not visited any of the laboratory facilities but is satisfied that these are reputable and internationally recognised companies who maintain ISO certification, overall presenting little risk to the grade estimation in the QP's opinion.

11.1.1 Prior to 2022

ADT's exploration drilling samples were sent to independent laboratories:

- Sample Preparation : ALS Bor in Serbia;
- Primary Laboratories : ALS Romania and ALS Ireland for assay; and
- Umpire laboratory : SGS Laboratory in Ankara, Türkiye.

The QP notes that ALS and SGS are global reputable accredited companies providing laboratory testing services. The QP did not verify the certification of the laboratories used.

11.1.2 Since October 2022

All analyses reported are certified by ISO laboratories and each laboratory was visited by ADT's QP who reported that there were no material issues.

Exploration drilling samples were sent to:

- Primary laboratory : SGS Ankara, Türkiye
- Umpire laboratory : ACME (Bureau Veritas) Laboratory in Ankara, Türkiye

Underground Grade Control drilling (which started in May 2024) samples were sent to

- Primary laboratory SGS Laboratory in Burgas, Bulgaria

11.2 Sampling Method

From 2017 to 2019 drill core was logged and processed in ADT's Ljepovici, core farm near Vareš village. All mineralized core was cut in half using a diamond saw, and sampled at two metre intervals regardless of the lithological boundaries, the remaining half core was retained in the core boxes.

Half core samples are packed in new (unused) calico bags, the sample label is placed inside, and the bag is marked with the sample number.

11.3 Chain of Custody

The samples are transported on pallets where all samples are ordered according to the work order. This practice has been in place since April 2023, prior to which sample loading was carried out manually according to the work order under the supervision of a responsible member of engineering staff.

The chain of custody since 2022 from ADT's core farm to the laboratory is rigorous with the samples accompanied from the warehouse to the customs facility at Visoko, where custom officers inspected the cargo before sealing the shipment. The shipment is then inspected for compliance (seal intact) at the BiH–Republic of Serbia border before travelling to the Bor customs facility where the seal was again inspected for compliance and the cargo inspected before its release to the laboratory. Crush and pulp reject material from the laboratory are returned to ADT, being transported in a similar manner. The samples remained sealed between the customs facility at Bor and its counterpart in BiH at Visoko.

Transport from Vareš to Ankara (SGS) has the same procedure as from Vareš to Bor (ALS). It is necessary to prepare proforma invoice and declaration of non-hazardous material, which are needed for import customs clearance in Visoko, in Republic of Serbia, Republic of Bulgaria and finally customs in Ankara.

11.4 Sample Preparation

From 2017 to the first half of 2022 sample material from all of the drillholes was dispatched to the ALS laboratory at Bor where it underwent sample preparation prior to pulp dispatch to ALS laboratories in Romania or Ireland. Sample preparation used ALS Prep-31 method:

- Sample is dried.
- Crushing with 70% less than 2 mm passing (10 mesh).
- Riffle splitting, for a 250 g sub sample.
- Pulverizing to better than 85% passing 75 microns (0.0074 mm / 200 mesh).

From mid-2022 onwards sample preparation is being undertaken at SGS Ankara by method PRP89:

- Sample is dried at 105°C.
- SGS crushing with 75% less than 2 mm passing (10 mesh).
- Splitting out a 250 g sub-sample in rotary splitter.
- Pulverizing to better than 85% passing 75 microns (0.0074 mm / 200 mesh), for a 250 g split for use in analytical submission.

11.5 Assay Method

11.5.1 Multielement

From mid-2022 the main package of elements were digested with four-acid digest (HNO_3, HF, $HClO_4$ and HCl) and analysed with ICP-AES, method ICP40B.

11.5.2 Base Metals and Silver

Prior to 2020, Lead, zinc, copper and silver were determined by an oxidizing acid digestion using HNO_3, $KClO_3$ and HBr with the final solution in dilute aqua regia finished with Inductively Coupled Plasma - Atomic Emission Spectroscopy (ICP-AES) on a nominal 5 g sample weight, analytical method ME-ICPORE.

After 2020, silver, zinc, lead, copper, and mercury were determined by four-acid digest and finished with ICP-AES, on a nominal 5 g sample weight by method ME-ICP61m, any over detection limit range results from the ICP61m were re-analysed using OG62 for silver, lead and copper. This is a four-acid digest with an ICP-AES finish.

Since 2022 samples with silver, zinc, lead and copper over the multielement assay detection limit were reassayed by four-acid digest with ICP-AAS finish for method GO_AAS43B.

11.5.3 Gold

From 2017 to 2019, samples were routinely analysed for gold by fire assay analytical method Au-AA25 with an Atomic Absorption Spectroscopy (AAS) finish on a nominal sample weight of 30 g. From 2020, the sample size was increased to 50 g and the detection limit lowered using method Au-AA24. From 2022 samples were routinely analysed for gold at SGS by fire assay with an Atomic Absorption Spectroscopy (AAS) finish on a nominal sample weight of 30 g (FAA303)

11.5.4 Barium

Barium oxide was determined by a lithium borate fusion prior to acid dissolution and ICP-AES on a nominal 5 g sample weight. Analytical method ME-ICP06.

From October 2022 onwards, over detection limit barium (>10%) results were analysed using portable pXRF under laboratory conditions with the results above detection limit (>50%) sent to SGS Lakefield, Canada by air freight for whole rock borate fusion XRF analysis.

11.5.5 Sulphur

All sampled intervals drilled by Eastern Mining in 2020, and selected samples from previous campaigns had total sulphur analysis by a LECO a combustion furnace with infrared detection method S-IR08. Subsequently, total sulphur was determined using S-IR08 method.

Since 2022 total sulphur determination has been done by LECO using a combustion furnace with infrared detection by method GE CSA06V

11.5.6 Mercury

Mercury was analysed by two acid digests with an Inductively Coupled Plasma Mass Spectrometry (ICP-MS) finish in method ICM14B. Over detection limit values for mercury were determined with aqua regia digestion with a ratio of HCl and HNO_3 of 3:1 and finished with ICP-AES (method ICP14B_Hg).

11.5.7 Antimony

Over grade antimony was determined by dissolution of sample in a molten flux, sodium peroxide fusion, finished with ICP-AES for method ICP90A

11.6 QAQC

11.6.1 Prior to 2017

No historical drillcore exists; past practice was for whole core to be assayed for mineralized intervals, whilst the remaining core represented by waste rock was discarded after being logged.

Historical exploration activities were often reported as six-monthly or annual reports. These contain comprehensive details of the drilling conducted, sampling method, and certified assay data. Many of these reports have been translated in full or in part by ADT.

11.6.2 2017 to September 2022

ADT routinely determined core recovery and certified reference materials, blanks and duplicates were routinely submitted to the laboratory at an overall insertion rate of 1/15, and field duplicates were submitted for 1/30 samples. From 2021, umpire laboratory pulp duplicates for "round robin" checks were dispatched for 1/15 samples which were analysed at SGS Bor.

This provided a reasonable amount of QAQC data for lead, zinc, silver, copper, gold and barite.

The SGS Bor umpire results were generally slightly lower than the primary laboratory results, by some 5.7% (gold) and some 4.5% (barium and copper) whilst silver and zinc were lower by less than 3%.

11.6.3 September 2022 to November 2024

In addition to enhanced core recovery and quality logging, the QAQC sample submissions were:

- Blanks 4%
- Standards 4%
- Field Duplicates 2%
- Crush Duplicates 5%
- Pulp Duplicates 10%

11.6.4 Current QAQC practice

The ADT geology team routinely submits QAQC samples although the submission frequency is different for surface drilling and underground grade control drilling, as follows:

- Blanks 5% (5% for UGGC)
- Standards 6% (8% for UGGC)
- Field Duplicates 2% (none – whole core sampling for UGGC)
- Crush Duplicates 2% (undergoing implementation for UGGC)
- Pulp Duplicates 18% (3% for UGGC)

Since 2021, some 4.3% of samples have had pulp duplicates submitted to an umpire laboratory. SGS Ankara was used as the umpire from 2017 to mid-2022 prior to it becoming it primary laboratory. Since October 2022 ADT has used ACME (Bureau Veritas) as their umpire laboratory.

BaO and other non-economic elements have been excluded from the umpire laboratory submission.

The detailed outcomes of the QAQC sample results are discussed by ADT in their MRE report. There has been considerable attention given to assay quality, notably the decision to change laboratory in late 2022 was made in an attempt to improve QAQC results.

ADT highlights some occasional results which seem to be incongruous and explains that some are due to sample mislabelling whilst others show occasional lapses in laboratory precision.

ADT has used some 13 different certified reference materials (“CRMs”) during its drilling programmes. Given the many different metals that are important for project revenue at Rupice, it is challenging to find one CRM that adequately represents all of the metal grades with values that are all close to those found in the deposit. ADT assessed that, of the total CRM submissions:

- 7% represent silver in the range of 200-500 g/t
- 10% represent zinc in the range of 3-10%
- 16% represent lead in the range of 1.5-8%
- 13% represent gold above 1.3 g/t; and
- 18% represent copper in the range of 0.15-1.3%

The overall conclusion reached by ADT and also their independent consultants is that there is no material concern of laboratory precision or accuracy, nor is there concern over sample preparation methodology or equipment cleanliness.

QP Comments

Some of the earlier CRM results prior to late 2022 show poorer results for some of the metals, for example copper and lead were slightly more erratic and marginally biased low. The precious metals were also occasionally slightly biased high in this period, generally by less than 10% relative. Since late 2022 the results are noticeably improved.

Field duplicates have reasonable repeatability with 90% of pairs differing by less than +/- 50% relative (60% for barium). Pulp and crush sample duplicates differ less than field duplicates since they are less affected by geological variability; these show good repeatability with 90% better than +/- 5% (10% for gold). Barium is not as well controlled, there was no CRM monitoring and some of the pulp duplicate plots are quite concerning although this is less the case for the crush duplicate plots.

The QP considers that overall, the QAQC results are presented comprehensively by ADT, they show no overall cause for concern. The CRMs demonstrated that the various laboratories and methods used in the generation of the majority of data used for the MRE have been monitored with sufficient rigour to support the classification of an Indicated Mineral Resource.

11.7 Density Determination

Samples each with a length of approximately 20cm, were collected every 20 m or after any change in lithotype, this has provided a comprehensive dataset for the project. Measurements were determined using an industry-standard Archimedes method using purpose-made equipment on site. The procedure was as follows:

- Sample was weighed in air using a cradle balance accurate to 0.1 g,
- Core was removed and the cradle immersed in water and “zero tared”,
- Core was placed in the cradle and completely submerged in water then weighed, and
- The bulk density (dry) value was calculated using the formula:

$$Bulk\ Density = Weight\ in\ Air\ /\ (Weight\ in\ Air - Weight\ in\ Water)$$

The mean density values are summarised by lithology in Table 11-1

Table 11-1: Summary of Densities by Lithology

Lithology type	Density (g/cm^3)
Tuffs	2.5
Tuffaceous sandstones and shales	2.5
Spilites	2.5
Sedimentary breccia	2.55
Marl	2.6
Chert	2.6
Limestone	2.65
Shales	2.75
Turbidites	2.75
Clear dolomites with stylolites	2.8
Pyritic shales	2.9
Semi-massive sulphides	3.5
Semi-massive barite	3.7
Massive barite	4.2
Massive sulphide	4.5

QP Comment

The density data is comprehensive and there is a strong relationship between density and metal grade which is typical for massive sulphide deposits. The method by which density has been estimated in the block model using multiple regressions with certain metals is not clear and the QP recommends further review of this; however, the QP has checked and agrees that densities in the block model are reasonable. Figure 11-1 illustrates the grade-density relationship.

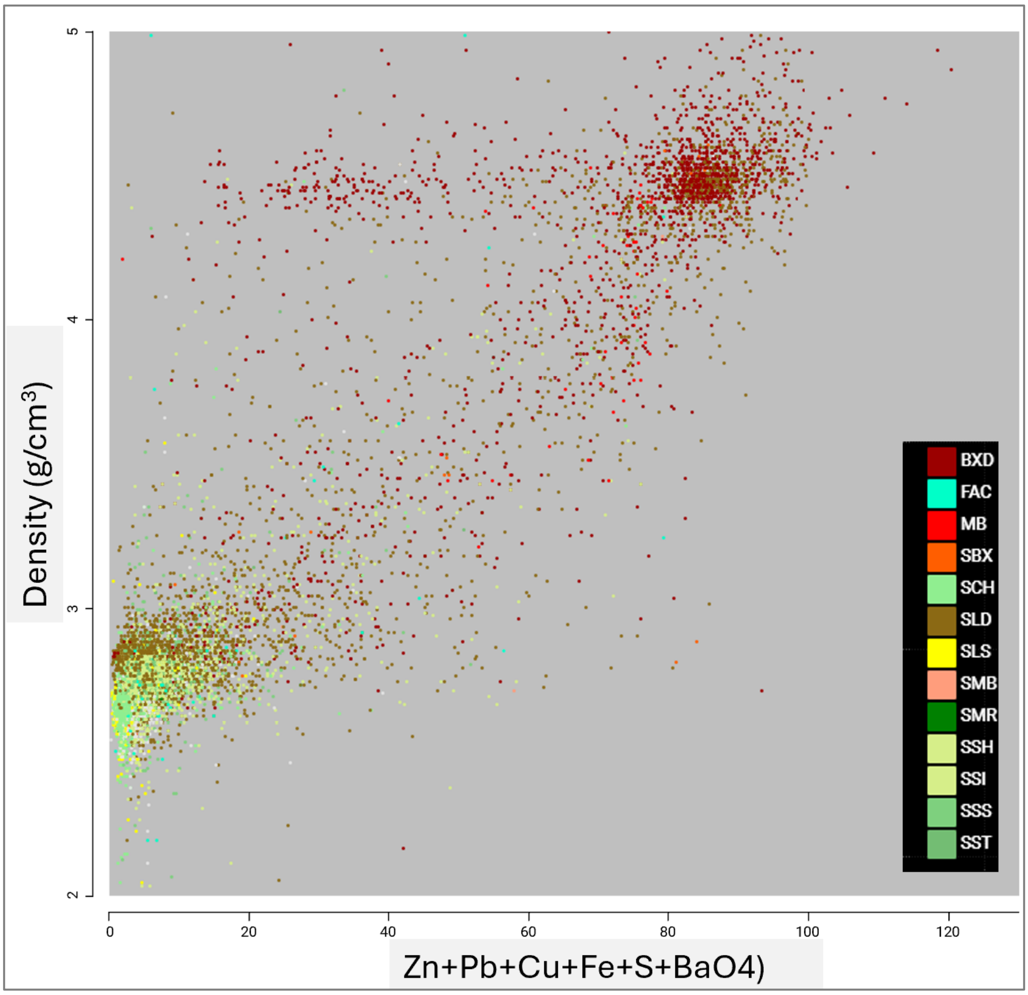


Figure 11-1: Density vs Grade coloured by Lithology

ITEM 12. DATA VERIFICATION

The Vareš Mine has commenced production, and as such information and statistics on performance, costs, state of infrastructure and operations, environmental, social and governance, including permitting, are known. The QPs highlight that its review and the production of this Technical Report took place during the course of a transaction, resulting in the flow of information being restricted.

The QPs have gained sufficient levels of confidence in the technical studies and work undertaken to support the declaration of the Mineral Resource and Mineral Reserve.

The QPs provide a summary of the data not provided by ADT by the Effective Date of this Technical Report in Table 12-1.

Table 12-1: Data Not Provided

	Data Not Provided	Qualification/ Potential Impact
Geotechnics	Geotechnical mapping data Ground support installation records	Actual conditions mapped as it compares to the study level rock quality characterisation from drill core. Partially supplemented by the QPs observations Actuals of ground support used versus design. Location of required rehabilitation. Suitable observational coverage of existing development ground support viewed by the QP
Hydrogeology	Numerical groundwater modelling.	Assumption that predicted inflows from numerical modelling are similar to those predicted in the DFS using analytical techniques.
Mining	Waste rock dump (WRD) design	Whereas a location is being permitting, no information on the design of the 600 kt WRD has been provided.
Processing	Limited historical operating data	Monthly production data includes tonnes processed, but no further data, preventing the QP from assessing plant performance. Though the plant is not yet operating at steady production this would have been beneficial to the QP's review.
Water management	As-built surface water management designs.	Assume that surface water management infrastructure was built as per the DFS.
Environmental and social	Project financing commitments	Environmental and Social Action Plan (ESAP) and monitoring reports from Independent Environmental and Social Consultant (IESC)
	Environmental monitoring	Environmental monitoring programme, monitoring data and reports.
	Assessments for Veovaca TSF	Environmental impact assessment for Veovaca TSF, including hydrological and hydrogeological water impact assessments
Legal	Legal due diligence	Status of surface rights, legal liabilities and on-going legal proceedings or claims that could pose a threat to the maintenance of mineral rights, surface rights, permits and approvals for the operation, or result in material fines and penalties.

	Data Not Provided	Qualification/ Potential Impact
Permitting	Evidence of environmental approvals	Copies of permits and up to date permit register (version provided dated 2023)
Permitting	Permit applications	EIA reports and waste management plans submitted to obtain key approvals
Permitting	Evidence of compliance with permit conditions	Regulatory compliance reports
Permitting	Permitting strategy	Roadmap with timelines for obtaining outstanding approvals
Mine closure	Detailed breakdown of closure cost estimates	Summary estimates provided but no detail
Access and Haul Road		The only documents providing information are the DFS report and monthly reports along with feedback from the site visit. The QP has not been provided with the designs or execution plan or specific details of the current interim remediation designs. This is noted as a gap in the QP's knowledge.
Logistics		Documents provided in the dataroom reference a suite of logistics related studies and documents, which haven't been made available. This is noted as a gap in the QP's knowledge.
Rail	Status of operation	The QP is unaware of the current condition of the railway line or risk of future disruptions due to failure of the infrastructure. This is not considered critical to the Vareš Mine, as alternative road transport is available for the sale of concentrates and supply of materials, where the cost impact is not expected to be prohibitive. However, it is raised as a gap in the QP's knowledge.
Actual capital costs	Little detail provided	Construction has been mostly completed. The remaining capital items outlined in the DFS and updates based on requirements identified by DPM and the QP form the basis of the projected capital costs. The QPs deem capital costs to meet minimum PFS level.
Operating costs	Detailed historical operating costs for 2024 and Q1 2025	Detailed actual operating costs are not critical to the QPs' review, due to the operations still ramping up, and costs not reflecting steady state. – The mining and processing unit costs have been estimated by DPM based on its operating experience from its operating mine in the region. – Logistics, general and administration, and other costs, are based on a global ADT figure provided in its economic assessment dated. These are not deemed to be material The QPs deem operating costs to meet PFS level.
Human resources	Employee complement by relevant category	Whereas no QP saw any details on the employee numbers by department, category, local vs expatriate, as the operation is in production, this is not deemed to be an area of concern. The Mining QP was aware that a significant number of expatriates are employed in the mining department in operations.

ITEM 13. MINERAL PROCESSING AND METALLURGICAL TESTING

13.1 Introduction

Testwork programs in support of the development of the Vareš Mine have been undertaken in several campaigns at the laboratory of Wardell Armstrong International (WAI) in Cornwall, UK:

- Preliminary testwork on three composites from Rupice, 2019;
- PFS testwork program on 9 composites from Rupice, 2020; and
- DFS testwork program on 6 composites and 44 variability samples from Rupice, 2021.

The samples in the preliminary Rupice program were of "average, "high" and "high copper" grades. The PFS program composites covered variations in zinc grade, variations in copper grade, zones of elevated precious (Au) and penalty (Hg) elements, and a composite representing the first year of proposed production. The DFS program tested a Year 1-3 composite and a Year 9-15 composite (based on the mine plan at the time), and of the 44 variability samples that underwent mineralogical examination, 19 were selected for flotation testwork, with four progressed to Locked Cycle Testwork (LCT).

13.2 Nature and Extent of Testwork

13.2.1 Head Assays

Head assays for all of the samples tested in the various programs are shown in Table 13-1 through to Table 13-4.

Table 13-1: Preliminary Testwork Head Assays

Orebody Phase		Rupice Preliminary		
Sample	**Unit**	**Average Grade**	**High Grade**	**Copper High Grade**
Cu	%	0.50	0.64	3.78
Pb	%	3.32	5.69	14.7
Zn	%	5.03	9.75	19.9
Ag	g/t	268	348	269
Au	g/t	1.79	3.22	3.48
$BaSO_4$	%	46.4	62.1	23.7
S_{TOT}	%	12.4	13.8	23.4
Fe	%	2.81	1.60	6.93
As	g/t	751	747	2680
Sb	g/t	2870	3460	3940
Hg	g/t	227	214	166
Cd	g/t	232	483	812

Table 13-2: PFS Testwork Head Assays

Orebody		Rupice								
Phase		PFS								
		Zinc Grade 2.5%	Zinc Grade 7.0%	Zinc Grade 13.0%	High Hg	High Au	Copper Grade 0.5%	Copper Grade 1.6%	Copper Grade 3.3%	Mine Plan Comp
Cu	%	0.49	0.56	0.71	0.61	0.42	0.51	1.69	3.50	0.87
Pb	%	2.44	4.35	6.70	7.14	5.22	4.46	13.7	16.7	6.74
Zn	%	2.81	6.21	13.7	8.68	5.20	4.97	21.8	24.6	12.6
Ag	g/t	433	533	459	1065	841	348	238	335	221
Au	g/t	2.34	2.74	4.34	5.49	4.51	1.40	2.64	4.79	3.00
$BaSO_4$	%	41.8	52.6	62.4	58.6	72.1	46.4	30.7	21.2	59.3
S_{TOT}	%	10.6	15.3	18.9	16.4	15.3	12.6	20.8	25.7	17.8
Fe	%	1.90	2.27	1.24	1.27	0.56	2.33	2.71	5.86	2.12
As	g/t	739	850	820	1100	580	800	1400	3400	1100
Sb	g/t	2260	4000	3400	4200	2600	7600	8900	6700	5200
Hg	g/t	256	506	160	662	324	180	182	274	135
Cd	g/t	-	-	-	-	-	-	-	-	-

Table 13-3: DFS Testwork Head Assays

Orebody		Rupice	
Phase		DFS	
		Year 1-3 Comp	Year 9-15 Comp
Cu	%	0.76	0.17
Pb	%	5.70	2.01
Zn	%	9.20	2.11
Ag	g/t	378	98.4
Au	g/t	3.11	1.73
$BaSO_4$	%	56.6	67.1
S_{TOT}	%	15.3	12.5
Fe	%	1.85	1.33
As	g/t	890	180
Sb	g/t	5100	1000
Hg	g/t	316	78.0
Cd	g/t	-	-

Table 13-4: DFS Testwork Head Assays – Variability Samples

		20	21	22	30	2	7	9	11	12
		RUP0330	RUP0004	RUP0009	RUP0280	RUP0014	RUP0270	RUP0297	RUP0407	RUP0447
Cu	%	0.72	0.35	0.40	0.29	0.63	0.31	0.23	0.066	0.005
Pb	%	4.55	4.79	6.45	5.15	2.22	2.72	1.67	0.42	2.90
Zn	%	7.60	9.51	11.0	10.5	2.34	2.92	1.97	1.48	0.069
Ag	g/t	321	454	425	118	86.7	476	64.6	89.7	17.3
Au	g/t	1.89	4.27	4.85	4.77	0.60	3.32	0.64	0.52	1.07
$BaSO_4$	%	76.1	74.6	68.7	74.1	10.5	87.4	10.4	8.94	90.1
S_{TOT}	%	18.4	16.3	17.9	17.1	11.1	14.5	13.7	7.19	13.4
Fe	%	1.43	0.32	0.45	0.43	6.03	0.22	8.02	3.74	0.24
As	g/t	580	380	530	450	1300	330	930	530	53
Sb	g/t	5400	2400	1500	2600	2200	3300	1700	8900	40
Hg	g/t	232	478	317	94.2	56.8	486	85.2	181	18.2
Cd	g/t	290	558	566	436	97	283	67	61	13

		17	23	24	25	31	34	36	37	39
		RUP0088	RUP0011	RUP0024	RUP0025	RUP0329	RUP0013	RUP0110	RUP0111	RUP0002
Cu	%	0.33	1.48	3.94	2.53	0.28	2.60	3.50	3.69	0.13
Pb	%	4.57	11.7	15.3	9.46	4.82	23.5	15.8	16.1	0.50
Zn	%	10.6	17.2	24.6	17.5	9.11	27.8	27.8	29.7	1.07
Ag	g/t	108	2026	240	155	419	345	283	275	58.3
Au	g/t	1.44	7.91	3.58	2.98	1.57	5.01	3.05	3.89	0.66
$BaSO_4$	%	72.0	51.0	20.3	44.9	74.6	17.0	20.6	13.6	10.5
S_{TOT}	%	17.6	20.6	28.7	23.9	16.1	25.7	27.5	28.6	14.8
Fe	%	0.60	1.95	6.54	4.46	0.69	3.12	5.24	6.45	9.07
As	g/t	190	1100	2500	2200	520	2000	2000	2500	380
Sb	g/t	6600	7500	1800	1700	3200	5000	2500	5000	650
Hg	g/t	62.9	624	107	98.7	750	361	115	133	52.4
Cd	g/t	400	>1000	>1000	731	363	>1000	>1000	>1000	43

		42	1	3	4	5	6	8	10	13
		RUP0396	RUP0007	RUP0058	RUP0070	RUP0073	RUP0195	RUP0275	RUP0374	RUP0482
Cu	%	0.27	0.038	0.047	0.18	0.013	0.38	0.007	0.045	0.91
Pb	%	0.72	1.70	0.76	0.40	0.72	4.09	1.41	2.86	0.48
Zn	%	0.70	0.64	0.60	0.38	0.41	10.7	0.11	0.069	0.68
Ag	g/t	36.3	27.6	103	44.0	20.2	125	26.8	203	27.7
Au	g/t	0.41	2.21	1.52	0.35	1.28	3.28	1.65	4.06	0.64
$BaSO_4$	%	4.05	74.0	84.0	14.8	74.4	72.3	69.6	62.3	90.1
S_{TOT}	%	3.46	11.5	13.0	11.0	11.7	18.4	10.6	9.85	15.9
Fe	%	2.15	0.34	0.46	7.13	0.66	1.79	0.31	0.52	1.88
As	g/t	490	90	60	250	90	820	50	160	750
Sb	g/t	2700	120	430	1500	140	5700	60	350	2800
Hg	g/t	30.0	46	76	20	69	228	16	92	48
Cd	g/t	29	33	35	22	26	337	14	6	13

		14	15	16	18	19	26	27	28	29
		RUP0483	RUP0485	RUP0492	RUP0095	RUP0184	RUP0196	RUP0199	RUP0201	RUP0274
Cu	%	1.24	0.89	0.38	0.30	0.28	0.38	0.37	0.30	0.89
Pb	%	4.43	3.77	5.10	3.01	4.08	4.50	7.00	6.30	12.0
Zn	%	3.23	1.86	7.53	6.09	9.69	9.89	14.6	14.0	11.8
Ag	g/t	48.7	57.7	159	108	128	360	337	447	727
Au	g/t	0.52	0.80	1.50	0.61	6.99	1.63	2.70	3.50	8.84
$BaSO_4$	%	80.4	84.6	46.4	83.0	75.7	76.0	64.7	68.2	55.9
S_{TOT}	%	16.8	16.6	16.2	15.6	17.7	17.2	18.7	18.6	18.4
Fe	%	2.10	2.12	4.28	0.40	0.99	0.52	76	0.72	1.81
As	g/t	1000	820	920	300	400	450	360	250	740
Sb	g/t	1800	4900	2100	1900	900	5200	2300	1900	1500
Hg	g/t	76	128	66	48	74	241	399	502	157
Cd	g/t	121	65	233	268	527	395	619	682	817

		32	33	35	38	40	41	43	44
		RUP0378	RUP0394	RUP0097	RUP0136	RUP0345	RUP0410	RUP0415	RUP0474
Cu	%	0.47	0.47	2.21	1.91	0.017	0.005	0.09	0.12
Pb	%	7.45	7.18	15.6	21.2	0.16	0.016	0.52	0.39
Zn	%	3.90	7.34	26.8	29.2	0.25	0.030	0.64	0.90
Ag	g/t	572	572	208	302	10.5	0.68	13.6	12.8
Au	g/t	2.92	1.51	1.93	1.54	0.13	0.010	0.10	0.12
$BaSO_4$	%	78.4	74.3	26.0	16.9	1.28	0.35	1.61	4.43
S_{TOT}	%	15.6	16.9	>20.0	>20.0	5.05	1.90	2.74	4.93
Fe	%	0.58	1.08	3.91	2.85	4.35	3.02	2.20	3.49
As	g/t	670	1000	1900	680	1300	320	170	290
Sb	g/t	2100	6000	6300	33300	220	110	1200	2000
Hg	g/t	830	357	124	262	38	16	8	11.0
Cd	g/t	315	353	>1000	>1000	9	1	28	33.4

13.2.2 Mineralogy

Mineralogical analysis, predominantly via QEMSCAN, formed a part of all of the metallurgical testwork programs. The base metal sulphide mineralogy at Rupice has been consistently shown to be relatively complex and fine grained. The following specific observations were made from the 44 geometallurgical samples analysed as part of the 2021 DFS:

- Lead is predominantly deported to galena (90%) with a minor amount of lead (10%) deported to bournonite. The bournonite deportment ranges from a low of <1% (i.e., all lead as galena) to a high of 40%.
- Bournonite is a copper, lead, antimony sulphide ($PbCuSbS_3$) which is expected to contribute to increased antimony and copper grade and decreased lead grade to the silver-lead concentrate as the proportion of this mineral relative to galena increases. High bournonite occurrences appear to be relatively isolated, so lead/silver concentrate quality are not expected to be affected significantly.
- Zinc is present exclusively as sphalerite and is found in no other non-sulphide minerals. The sphalerite is believed to be low iron sphalerite; therefore, achieving consistently high (>55% Zn) concentrate grades should be possible.
- Copper deportment is quite variable and is split on average between chalcopyrite (26%), tetrahedrite (45%) and bournonite (28%). This relatively complex deportment renders it difficult to produce saleable copper concentrates consistently due to the contribution of arsenic from tetrahedrite and lead from bournonite.
- The base metal sulphide mineralogy is quite fine grained, with galena grain sizes averaging 37 μm and liberation averaging 40% at a 60 to 65 μm primary grind. Sphalerite was generally coarser, with an average grain size of 80 μm and liberation averaging 62%. Liberation data points towards primary grinding requirements of a P_{80} of 40 to 65 μm, with fine regrinds required for the silver-lead circuit, and moderate regrinding required for the zinc circuit.
- Microprobe analysis of concentrates during the PFS confirmed that mercury is not present as a discrete mercury sulphide mineral, but in solid solution in other minerals that report to the concentrate.
- Gangue mineralogy is dominated by barite (51%), quartz (16%) and pyrite (6%).
- Trace amounts of acanthite (silver sulphide) were detected. No detailed silver deportment testwork has been undertaken.

The mineralogical investigations from the earlier program for Rupice follow these same trends.

13.2.3 Comminution

Comminution testwork consisted primarily of Bond Ball Mill Work Index (BBWi) tests, with some samples also subjected to Bond Rod Mill Work Index (BRWi), Bond Abrasion Index (Ai) and SAG Mill Comminution (SMC) Tests. The results of the comminution tests are shown in Table 13-5.

Table 13-5: Comminution Test Results

Orebody	Phase	Sample	BBWi (kWh/t)	BRWi (kWh/t)	Ai (g)	SMC "A*b"	SMC "ta"
Rupice	**Prelim**	Average Grade	8.54	-	-	-	-
	PFS	Zinc Grade 2.5%	10.7	12.7	0.3	64.5	0.46
		Zinc Grade 7.0%	8.1	9.71	0.115	120	0.77
		Zinc Grade 13.0%	5.6	7.66	0.038	140	0.8
		Mine Plan Comp	6.2	8.17	0.031	125	0.73
	DFS	7	5.09	6.83	-	-	-
		17	4.72	-	-	-	-
		23	7.12	7.8	-	-	-
		30	5.32	-	-	-	-
		31	5.78	-	-	-	-
		35	7.76	8.66	-	-	-
		37	7.84	-	-	-	-
		44	13.9	-	-	-	-
		HW	12.7	15.3	-	-	-
		FW	14.3	16.2	-	-	-
		Fault 5	13.2	-	-	-	-
		Fault 8	14.1	-	-	-	-

The comminution test results show that dilution material (HW, FW, Fault 5 and Fault 8) is expected to present much higher hardness than high grade ore. In general, the hardness (BBWi) decreased with increasing sulphide and/or barite content.

Regrind tests were undertaken using a 4 litre Netzsch (IsaMill) during the DFS. Based on the signature plots, the following specific energy requirements were determined:

- Pb rougher concentrate: 35.8 kWh/t to achieve a P_{80} of 10 μm; and
- Zn rougher concentrate: 13.5 kWh/t to achieve a P_{80} of 20 μm.

13.2.4 Flotation

In the preliminary testwork program for Rupice, a suite of 20 batch rougher flotation tests, 20 batch cleaner tests and five LCTs were undertaken on the Average Grade sample. Testing focused on two flowsheets:

- Bulk flowsheet – targeting production of a bulk copper/lead concentrate and separate zinc concentrate; and
- Sequential flowsheet – targeting production of separate copper, lead and zinc concentrates.

Both flowsheets required a primary grind P_{80} of 40 μm. Copper and lead rougher concentrates were reground to a P80 of 10 μm and zinc rougher concentrates to a P_{80} of 20 μm. The investigation into the bulk route culminated in four locked cycle tests, with the optimum test producing a copper/lead concentrate assaying 6.70% Cu, 45.3% Pb and 10.1% Zn at recoveries of 79.2%, 89.0% and 12.4% respectively. The copper/lead concentrate was also high in gold and silver, assaying 15.0 g/t Au and 3,443 g/t Ag at recoveries of 46.2% and 78.9% respectively. The zinc concentrate assayed 0.36% Cu, 1.31% Pb and 57.4% Zn at recoveries of 5.0%, 3.0% and 82.5% respectively.

Early testing using the sequential route was characterised by poor upgrading and/or low recoveries to the copper concentrate, as well as poor selectivity against lead. Later testing using a new reagent scheme to improve selectivity against lead yielded improved results. Testing culminated in a single locked cycle test that focussed on copper, producing a copper concentrate that assayed 22.9% Cu, 15.8% Pb and 5.45% Zn at recoveries of 63.0%, 6.9% and 1.5% respectively. Gold and silver grades were 14.1 g/t Au and 7,235 g/t Ag at recoveries of 11.0% and 43.1% respectively.

Analysis of selected cleaner and LCT concentrates for common penalty elements identified high levels of arsenic, mercury, antimony and cadmium. A mineralogical analysis of selected concentrates identified no discrete phases for mercury and cadmium, therefore it was concluded that they were most likely hosted in solid solution within the major sulphides. Microprobe analysis identified mercury within sphalerite, galena and bournonite. Cadmium was identified predominantly within sphalerite. Bournonite and tetrahedrite were identified as the main antimony-bearing phases, particularly in the copper/lead cleaner concentrate. Microprobe analysis also found antimony at very low levels within sphalerite – accounting for some 40% of the antimony within the zinc cleaner concentrate. The main hosts of arsenic were tetrahedrite and, in rare occurrences, seligmannite and enargite. Microprobe analysis also identified pyrite and bournonite as hosts of arsenic and could account for some 20% of the arsenic within the flotation concentrates.

The High Grade and Copper High Grade samples were each subjected to a single rougher test for both the bulk and sequential flowsheets, using the flotation conditions optimised for the Average Grade sample. The results indicated that they responded well to these conditions, although further investigation and optimisation would be required. A LCT on the High Grade sample was subsequently undertaken using the sequential flowsheet. This test generated a copper concentrate assaying 25.1% Cu, 14.6% Pb and 5.68% Zn at recoveries of 63.7%, 5.0% and 1.1%, respectively. The copper concentrate was also high in gold and silver, assaying 20.9 g/t Au and 9,550 g/t Ag at recoveries of 13.7% and 55.4%, respectively. The lead concentrate assayed 2.15% Cu, 51.8% Pb and 13.4% Zn at recoveries of 26.0%, 84.9% and 12.8%, respectively. It also contained high levels of gold and silver: 10.9 g/t Au and 1,003 g/t Ag at recoveries of 34.2% and 27.9%, respectively. The zinc concentrate assayed 0.28% Cu, 1.59% Pb and 60.3% Zn at recoveries of 4.4%, 3.4% and 75.8%, respectively. Additional analysis of the products found high levels of potentially deleterious elements in all products. The copper concentrate contained 2.00% As, 10.2% Sb and 863 g/t Hg; the lead concentrate assayed 0.23% As, 1.26% Sb and 373 g/t Hg; while the zinc concentrate assayed 2,940 g/t Cd and 912 g/t Hg.

During the PFS, the sequential flowsheet was tested at a primary grind size P_{80} of 40 μm. The testing involved rougher, cleaning and a single LCT on each of the nine composites. In some cases, a “scalping stage” was used, where the material floating in the first minute of rougher flotation was cleaned once and the product reported as final concentrate. The cleaner tails were combined with the remainder of the rougher concentrate and subjected to regrinding ahead of three stages of cleaning. The copper-lead and zinc rougher concentrates were reground to P_{80}s of 10 μm and 20 μm respectively.

Lead grades in the copper-lead concentrates ranged from 42% to 51% at recoveries of 81% to 94%. Copper grades were 3.8% to 8.3% at recoveries of 67% to 85%, although recoveries were generally above 80%. Levels of mis-reported zinc were generally low but up to as much as 32% in one instance. Six of the nine variability samples achieved a silver grade of >2,500 g/t Ag in the copper-lead concentrate. The reason for samples not achieving this target grade was attributed to a higher ratio of copper and lead to silver in the feed. Mercury levels in the copper-lead concentrates were variable but >2,000 g/t Hg in three samples.

Zinc grades in the zinc concentrates ranged from 55% to 61% Zn at recoveries of 58% to 81%, although recoveries were generally in excess of 70%. These lower zinc recoveries were due to zinc either misreporting to the preceding bulk copper-lead concentrate or to the tailings. Silver grades in the zinc concentrates were 145 to 638 g/t at recoveries of 3.7% to 19.6%. Gold grades were 2.6 to 10.4 g/t at recoveries of 9.8% to 29.8%. As with the copper-lead concentrates, mercury levels in the zinc concentrates were variable but >2,000 g/t in three samples.

The DFS commenced with testwork on a blended sample representative of the first three years of production, sourced from remaining material from the PFS. The primary aim of the study was to simplify and optimise the previously developed processing flowsheet and reagent scheme, covering primary grind size, reagent types and doses, and circuit configuration.

36 batch rougher tests were undertaken, followed by 15 batch cleaner tests, which then led into 4 LCTs, the last of which used water sourced from site. LCT3 (lab water) produced a Ag/Pb Concentrate assaying 6.36% Cu, 45.5% Pb and 13.2% Zn at recoveries of 80.7%, 83.6% and 15.1% respectively. Gold and silver grades in the Ag/Pb Concentrate were 11.4ppm Au and 2,628ppm Ag at recoveries of 40.7% and 72.9% respectively. Concentrations of major penalty elements included 0.49% As, 4.18% Sb and 831ppm Hg at recoveries of 60.4%, 86.3% and 27.7% respectively. A Zn Concentrate was produced assaying 54.6% Zn at 80.8% recovery. Gold and silver grades in the Zn concentrate were 6.37ppm Au and 484ppm Ag at recoveries of 29.3% and 17.3% respectively. The mercury content was 1,350ppm Hg at 58.2% recovery.

The use of site water did not appear to have any significant detrimental impact on flotation performance – the mass pull to both concentrates was increased by between 1% and 1.5%. The main effects of this were increased lead and silver recoveries to the Ag/Pb Concentrate at the cost of reduced lead grade, increased misplaced zinc, and reduced zinc recovery to the subsequent Zn Concentrate.

Variability testwork applied the flowsheet and conditions optimised in the initial study to selected Variability Samples to assess the effect of ore variability on flotation response. In total, 19 of the original 44 Variability Samples were selected for testing, as well as a new blend representative of the latter years of production (MP Yr9-15 Comp). A detailed flotation investigation culminated in LCTs on five of the samples. The five samples subjected to LCTs all produced saleable-grade Ag/Pb Concentrates, while four of the five produced saleable-grade Zn Concentrates – the poorer response of the fifth sample was attributed to its slightly more complex mineralogy and concentrate dilution due to elevated barite content, however batch cleaner testing did demonstrate it was possible to produce a >50% Zn concentrate from this sample, albeit at a reduced recovery.

The results of the flotation testwork are summarised in the following graphs, showing grade-recovery relationships from the LCTs for Pb to the Pb concentrate (Figure 13-1), Zn to the Zn Concentrate (Figure 13-2), Ag to both Pb and Zn concentrates (Figure 13-3) and Au to both Pb and Zn concentrates (Figure 13-4).

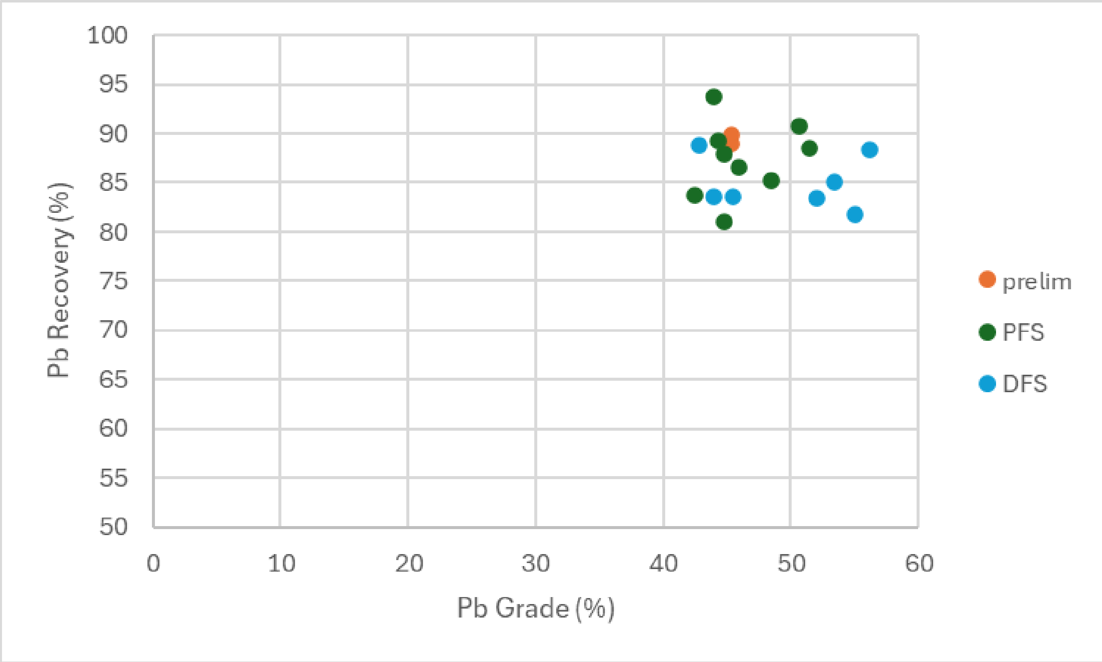


Figure 13-1: LCT Grade-Recovery Data, Pb to Pb Concentrate

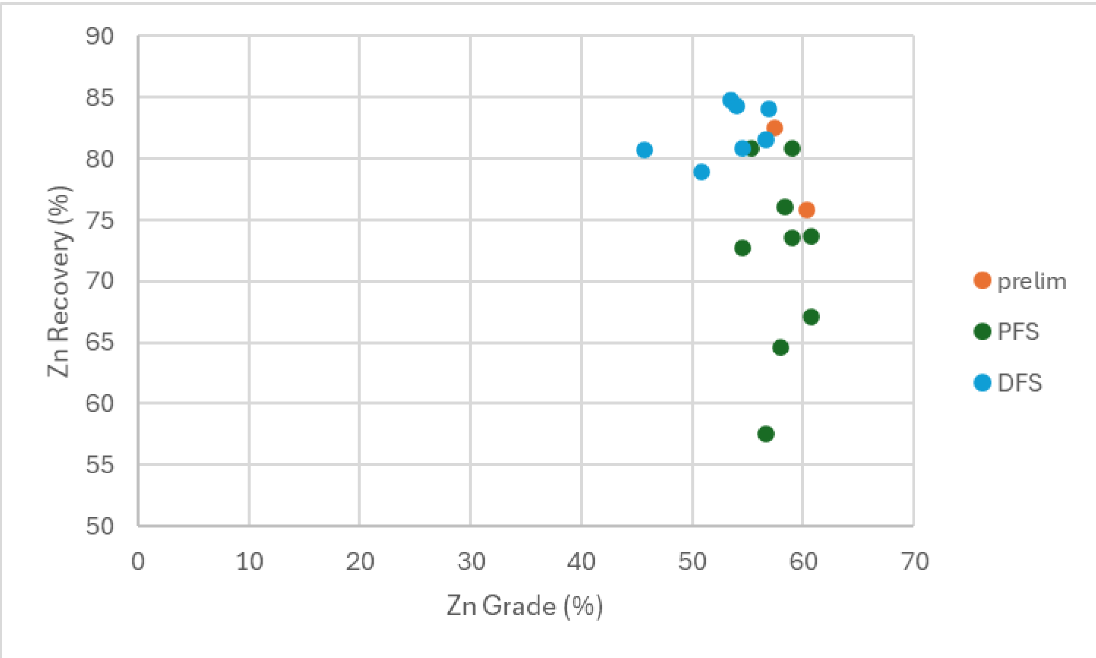


Figure 13-2: LCT Grade-Recovery Data, Zn to Zn Concentrate

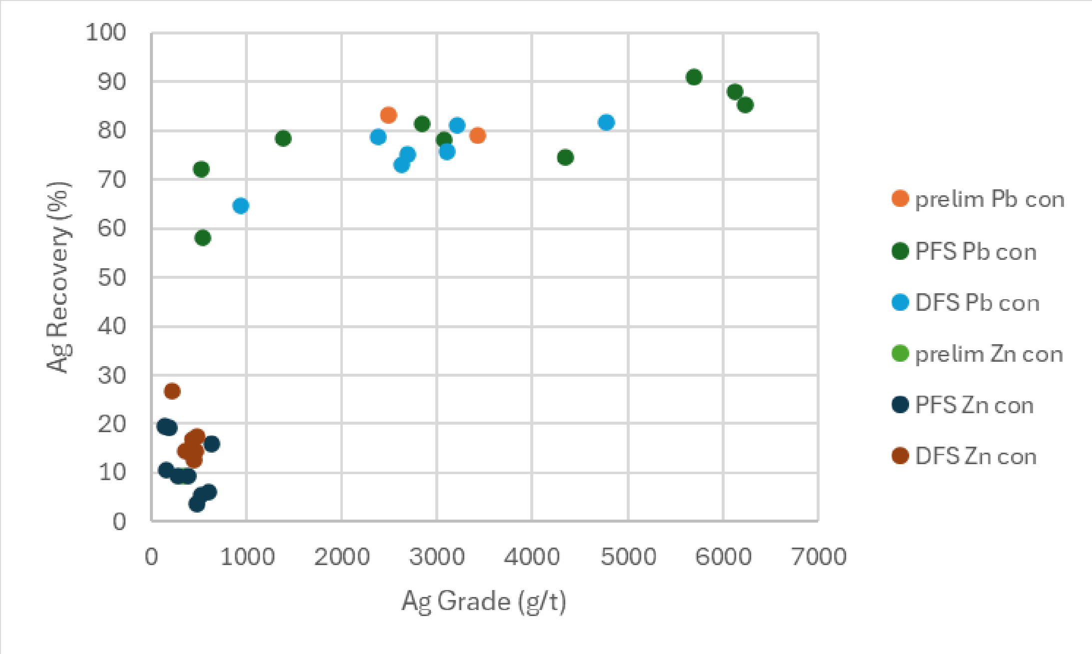


Figure 13-3: LCT Grade-Recovery Data, Ag to Pb and Zn Concentrates

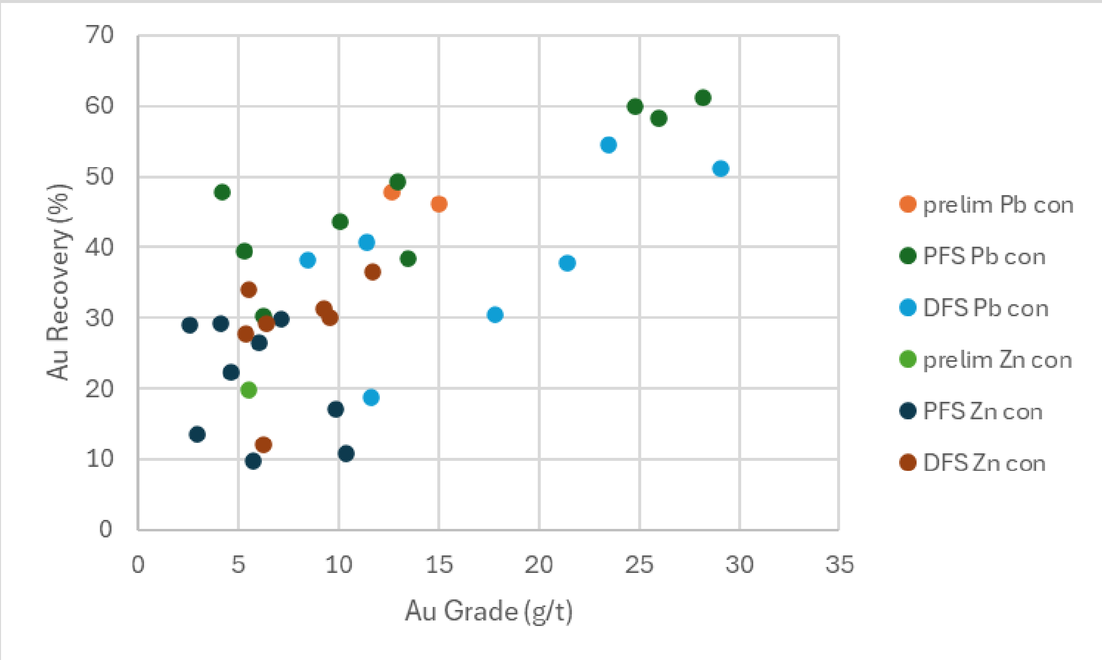


Figure 13-4: LCT Grade-Recovery Data, Au to Pb and Zn Concentrates

13.2.5 Dewatering

Samples of Ag/Pb Final Concentrate, Zn Final Concentrate and Final Tailings were prepared and shipped to Metso-Outotec for the purposes of thickening and filtration testwork. Upon completion of the dewatering programme, these samples were then forwarded on to the Alfred H Knight group for TML and FMP testing.

13.2.6 Other Testwork

As noted above, selected samples from the preliminary Rupice testwork program were subjected to mineralogical analysis. Samples were also cyanide leached as a diagnostic tool to help understand the gold deportment. Just over half of the gold in the head sample was cyanide recoverable, with the proportion of cyanide recoverable gold being higher in the flotation concentrate samples (Cu>Pb>Zn) than in the flotation tailings sample.

During the DFS, a short programme of gravity testing was undertaken to investigate the feasibility of removing mercury prior to downstream flotation processing. Testing was undertaken on a composite sample representative of the first three years of production. 20 kg of material was processed through a Knelson Concentrator. The results indicated there was no significant concentration of any metals within the concentrate. 1.6% of the lead, 2.2% of the gold, 0.9% of the silver and 0.7% of the mercury was recovered to a gravity concentrate accounting for 0.6% of the sample mass.

A sample of Final Tailings from the DFS LCTs 1-3 was submitted for a suite of environmental testing including:

- Detailed chemical analysis;
- Acid-Base Accounting (ABA) test;
- Net Acid Generation (NAG) test;
- Net Acid Production (NAP) test;
- Shake-Flask test (with deionised water);
- Synthetic Precipitation Leaching Procedure (SPLP) test; and
- Toxicity Characteristic Leaching Procedure (TCLP).

13.3 Basis of Recovery Estimates

Recovery relationships were developed by Ausenco during the PFS, based on the PFS LCT results. These are shown in Table 13-6.

In the DFS report, Ausenco noted that these equations had not been updated to include the DFS testwork results, due to time constraints. As a means of assessing the ongoing validity of these equations, the QP has calculated the grades and recoveries using these equations for all of the published LCT results (i.e. PFS, DFS and the preliminary program), and compared them to the reported testwork results. These comparisons are shown below for mass yield (Figure 13-5), Pb recovery to the Pb Concentrate (Figure 13-6), Zn recovery to the Zn concentrate (Figure 13-7), overall Ag recovery (i.e. to both concentrates combined) (Figure 13-8) and overall Au recovery (Figure 13-9).

Table 13-6: Recovery Equations (Ausenco, 2021)

Element	Concentrate	Recovery	Constraints
Bulk Circuit			
Cu	Pb_{ER} x $Feed_{Cu}$	81.529 x $Feed_{Cu\%}^{0.0407}$	Recovery: If Cu% in feed <0.25% then no conc produced Concentrate: If Cu% in feed <0.25% AND If Pb% in feed <0.5%, THEN no concentrate, ELSE Cu : Pb ratio > 0.9, THEN 29% Cu, ELSE Pb conc ER * feed grade Cu%
Pb	11.208 x $\ln(Feed_{Pb\%})$ + 28.772	78.047 x $Feed_{Pb\%}^{0.0676}$	If Pb% in feed <0.5% then no conc produced
Zn	(0.1292 x Pb_{ER} – 0.0441) x $Feed_{Zn}$	$Conc_{Zn}$ x $Conc_{mass}$ / $Feed_{Zn}$	Maximum zinc recovery of 30% Concentrate: If Zn : Pb ratio > 10 THEN no lead cct, ELSE If Zn conc factor > 0.8 THEN no lead cct (0.2274*Pb Conc ER+0.1292)*Zn conc factor))
Au	$Feed_{Au}$ x Rec_{Au} / Pb $Conc_{mass}$	30.435 x $Feed_{Au}^{0.357}$	
Ag	$Feed_{Ag}$ x Rec_{Ag} / Pb $Conc_{mass}$	31.019 x $Feed_{Ag}^{0.154}$	
Sb	$Feed_{Sb}$ x Rec_{Sb} / Pb $Conc_{mass}$	1.1046 x $Rec_{Cu\%}$	Maximum antimony recovery of 95%
As	$Feed_{As}$ x Rec_{As} / Pb $Conc_{mass}$	0.8704 x $Rec_{Cu\%}$	
Hg	$Feed_{Hg}$ x Rec_{Hg} / Pb $Conc_{mass}$	3.5346 x $Feed_{Hg}^{0.4016}$	
Zinc Circuit			
Cu	$Feed_{Cu\%}$ x $Rec_{Cu\%}$ / Zn $Conc_{mass}$	97.8% – $Pb_{cct\ Rec}$ – 4.2879 x $(Cu\%)^{0.7713}$	Maximum copper recovery of 97.8%
Pb	$Feed_{Pb\%}$ x $Rec_{Pb\%}$ / Zn $Conc_{mass}$	2.7669 x $\ln(Feed_{Pb\%})$ + 89.936 – $Pb_{cct\ Rec}$ – 0.1393 x $\ln(Feed_{Pb\%})$ - 1.2539	
		2.6276 x $\ln(Feed_{Pb\%})$ +88.6821– $Pb_{cct\ Rec}$	
Zn	53.834 x $Feed_{Zn\%}^{-0.966}$ x $Feed_{Zn}$	94.944 x $Feed_{Zn\%}^{0.0146}$ – $Pb_{cct\ Rec}$ – 6.2883 x $Feed_{Zn\%}^{0.0436}$	If Zn% in feed <1.0% then no conc produced
Au	$Feed_{Au}$ x Rec_{Au} / Zn $Conc_{mass}$	64.193 x $Feed_{Au}^{0.1568}$ – $Pb_{cct\ Rec}$ – 7.2305 x $Feed_{Au}^{0.1203}$	
Ag	$Feed_{Ag}$ x Rec_{Ag} / Zn $Conc_{mass}$	82.928 x $Feed_{Ag}^{0.022}$ – $Pb_{cct\ Rec}$ +1.154 x $\ln(Feed_{Ag})$ -10.281	
Sb	$Feed_{Sb}$ x Rec_{Sb} / Zn $Conc_{mass}$	97.643 x $Feed_{Sb\%}^{0.0086}$ – $Pb_{cct\ Rec}$ +2.44 x $\ln(Feed_{Sb\%})$ +1.566	
As	$Feed_{As}$ x Rec_{As} / Zn $Conc_{mass}$	90.777 x $Feed_{As\%}^{0.0246}$ – $Pb_{cct\ Rec}$ – 18.844 x $Feed_{As\%}^{0.5931}$	
Hg	$Feed_{Hg}$ x Rec_{Hg} / Zn $Conc_{mass}$	-4.184 x $\ln(Feed_{Hg})$ + 97.8 – $Pb_{cct\ Rec}$ -$Py_{cct\ Rec}$	
		-4.184 x $\ln(Feed_{Hg})$ + 97.8 – $Pb_{cct\ Rec}$ +0.0129 x $Feed_{Hg}$ –12.073	
		-4.184 x $\ln(Feed_{Hg})$ – $Pb_{cct\ Rec}$ +0.0129 x $Feed_{Hg}$ + 85.727	

Notes: ER – Enrichment ratio, CONC – Concentrate, Feed – Feed stream (i.e grade or tonnes), Cct – Circuit (i.e. silver-lead, zinc)

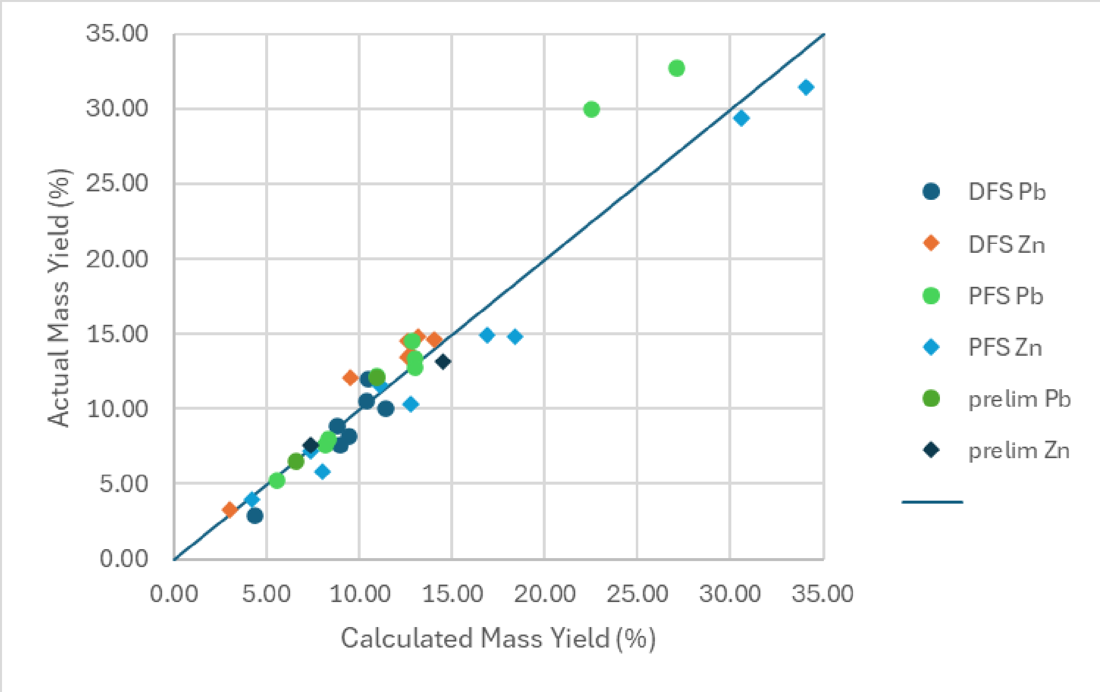


Figure 13-5: Comparison of Calculated and Actual Mass Yield

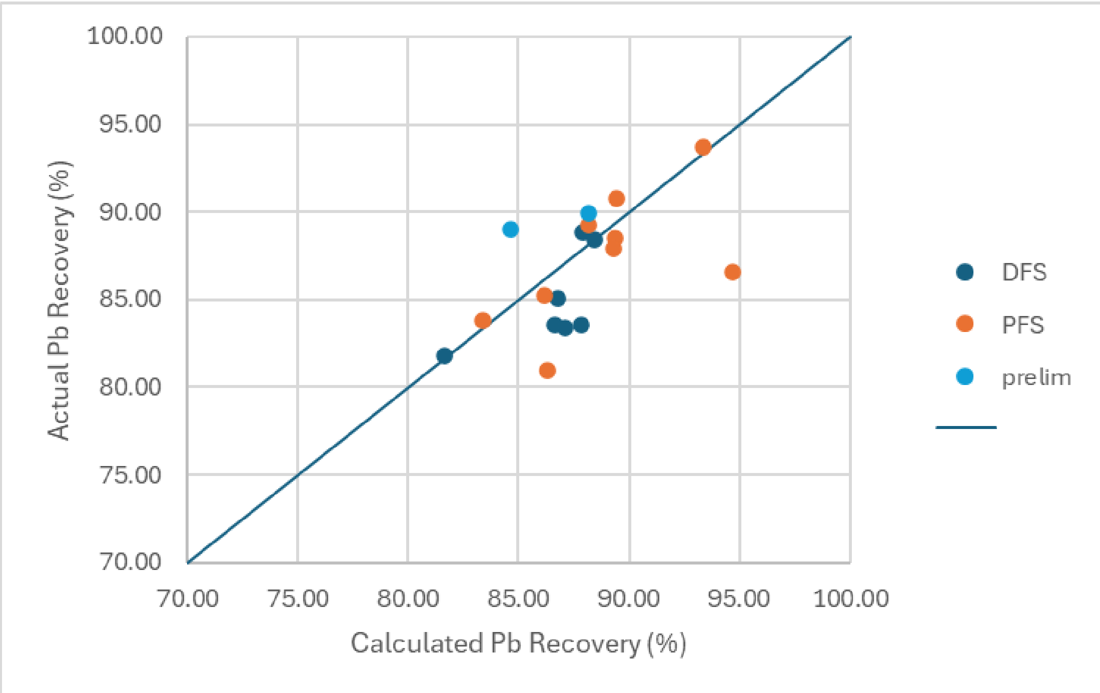


Figure 13-6: Comparison of Calculated and Actual Pb Recovery (to Pb Con)

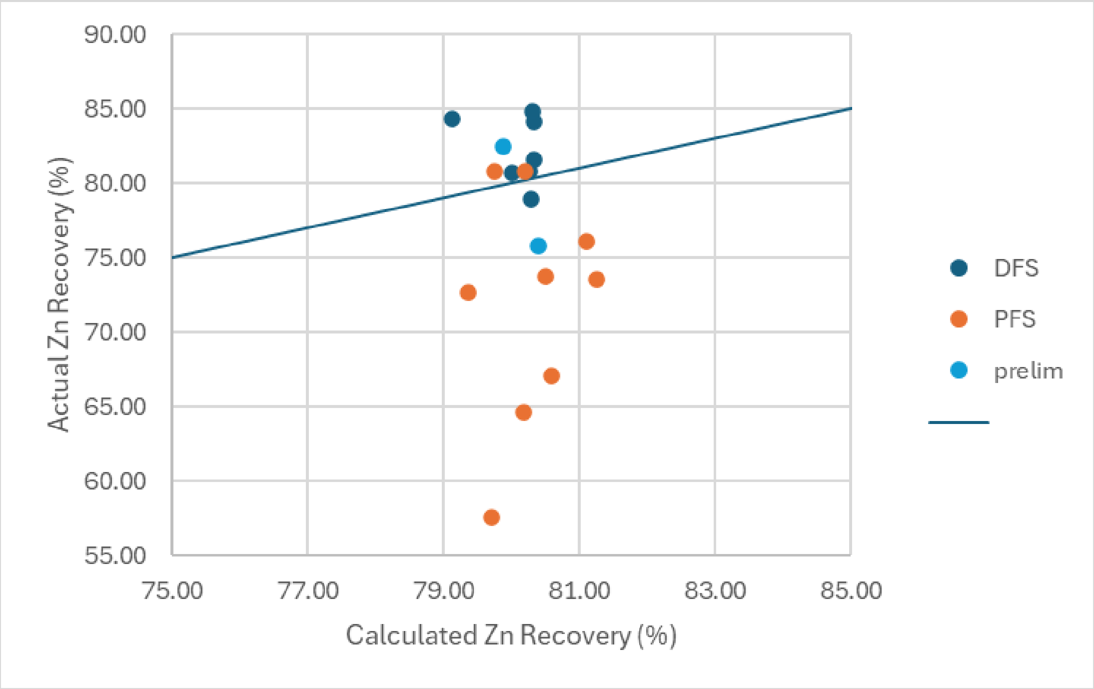


Figure 13-7: Comparison of Calculated and Actual Zn Recovery (to Zn Con)

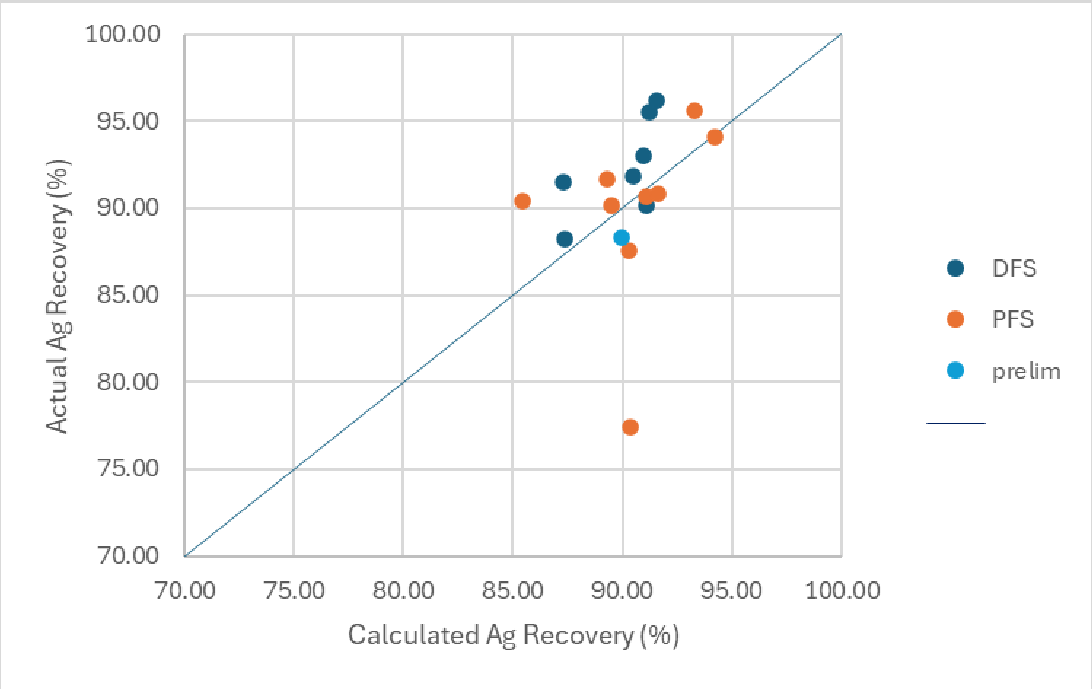


Figure 13-8: Comparison of Calculated and Actual Ag Recovery (Overall)

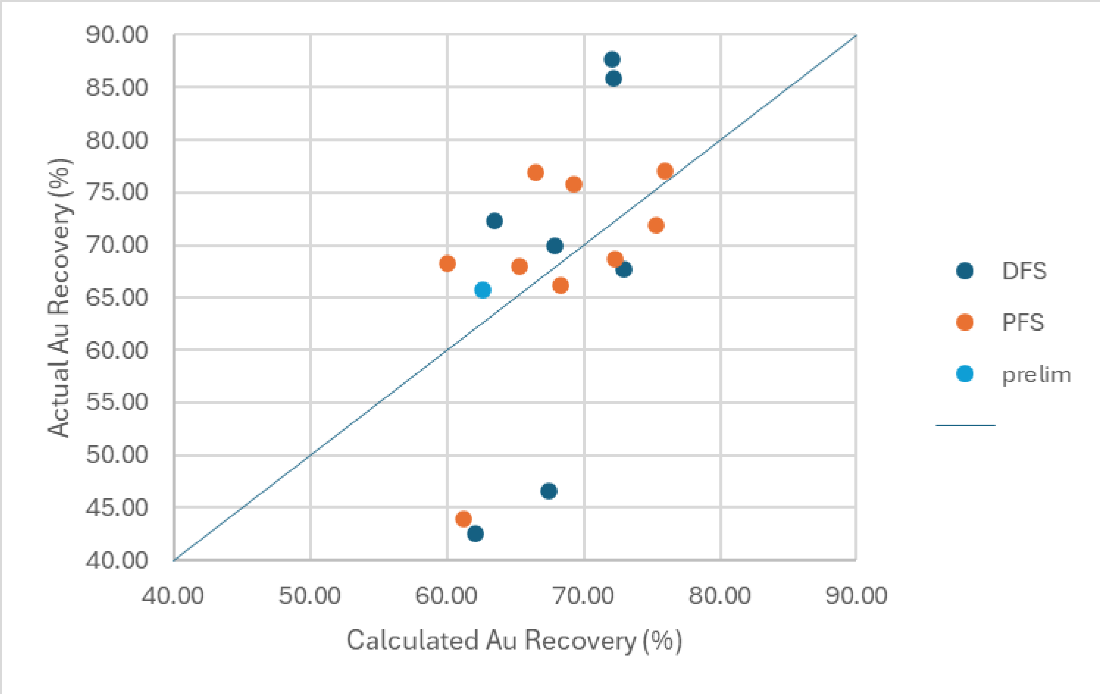


Figure 13-9: Comparison of Calculated and Actual Au Recovery (Overall)

The mass yields, which are calculated from regression equations for both recovery and concentrate grade, show a good agreement with the testwork (actual) values. There appears to be no material difference between the PFS and DFS figures.

The Pb recovery figures also show a reasonable agreement between the calculated and actual figures, and between the PFS and DFS figures, albeit with some scatter present. The Ag recovery and Au recovery figures exhibit similar behaviour, although with an increasing degree of scatter comparing Pb to Ag to Au.

The Zn recovery figures do not show good agreement between the calculated and actual values for the PFS results, although the correspondence (albeit over a limited range) is better for the DFS values. In the DFS report Ausenco also noted a poor correspondence between the projected and testwork Zn recovery figures.

Based on this analysis, the QP concludes that the equations developed on the basis of the PFS testwork results are consistent with the DFS testwork results.

13.4 Representivity of the Mineralisation

None of the WAI testwork reports contain details of the origin of the samples tested, i.e. drillhole names/numbers and interval depths, and so independent verification of the representivity of the samples tested has not been possible. There is a figure in the DFS showing an overlap of the DFS variability samples and the block model, which suggests that the variability samples provided reasonable coverage of the Rupice orebody.

13.5 Deleterious Factors

As noted above, chemical and mineralogical analyses of the ore and concentrate samples identified the presence of potential penalty levels of As, Hg, Sb, and Cd in the Pb and Zn concentrates.

In the DPM TEM, penalties are applied for Hg, As and Sb in the Pb concentrate, and for Hg in the Zn concentrate.

13.6 QP Comments on Section 13

The testwork with regard to comminution and flotation is of sufficient breadth and depth to inform a Feasibility Study level of project definition, leading into detailed design and construction. However other aspects, notably dewatering (thickening and filtration) testwork has been conducted on only one sample in each case (i.e. both concentrates and the flotation tailings) – this represents a risk to the robustness of the ensuing plant design and operation.

ITEM 14. MINERAL RESOURCE ESTIMATES

14.1 Estimation Summary

The Rupice 2024 Mineral Resource block model was jointly completed by the ADT resource team in Vareš and AMC Consultants based out of Perth and Melbourne, Australia.

The QP has reviewed the data, geology, interpretation, density and grade estimation methodology, RPEEE, classification and reporting aspects of the work presented in :

- ADT's 14 March 2025 MRE update report (Rupice Polymetallic Deposit – December 2024 - Mineral Resource Update Technical Summary) and in
- AMC's preceding 7 November 2024 MRE report (2024 Mineral Resource Statement : "Rupice Polymetallic Deposit : Mineral Resource Update")

Overall the QP considers the underlying data and geological interpretation to be robust. A detailed grade estimation approach has been used which uses industry standard methods; the wireframing is geologically realistic and comprehensively thought-out creating detailed grade estimation domains for each element of interest.

Tonnage estimation is based on a density-grade relationship determined from a comprehensive density dataset.

Classification has been undertaken using a pragmatic assessment of drillhole spacing with respect to defendable continuity of the various mineralised features.

Mineral Resource reporting by ADT-AMC used a silver equivalent cut-off grade which has not been changed since 2020, since when metal prices have changed, metal recovery information from the processing plant has become available, smelter terms realised by the project have become available and actual operating costs have realised since operations began have increased relative to the DFS.

The latter point resulted in a much higher cutoff grade being used when reporting Ore Reserves in March 2025 compared with that used in the DFS.

For these reasons the QP decided to re-report MRE from the ADT-AMC block model using updated cut-off criteria.

14.2 Underlying Database

14.2.1 Current Data Management

All drillhole data have been compiled, validated and maintained by ADT geologists and loaded into acQuire data management system on the company SQL server in Vareš.

When importing data, acQuire has validation rules to avoid any duplicates or omissions. ADT used dedicated data geologists to manage the data stream in acQuire.

Assay results are imported into the system and released to the end users by the data geologist as soon as the QAQC checks are within tolerance. All files (collar, survey, geology, assay, recovery, geotechnical, density, logging) were validated by the team and the system to ensure that the populated data is integrated, complete and accurate.

In addition to diamond drillhole data, there are 18 channel samples entered into the database as ‘drillholes’; these are horizontal channels cut into the side wall of cross cuts through the orebody. The channel samples provide meaningful assay data which in the QP’s opinion can be used along with the underground and surface diamond drillholes.

Geological Modelling

The host rock lithologies and stratigraphy have been modelled in 3D which provides an important reference for the grade modelling where the influence of faulting and folding can be more easily understood.

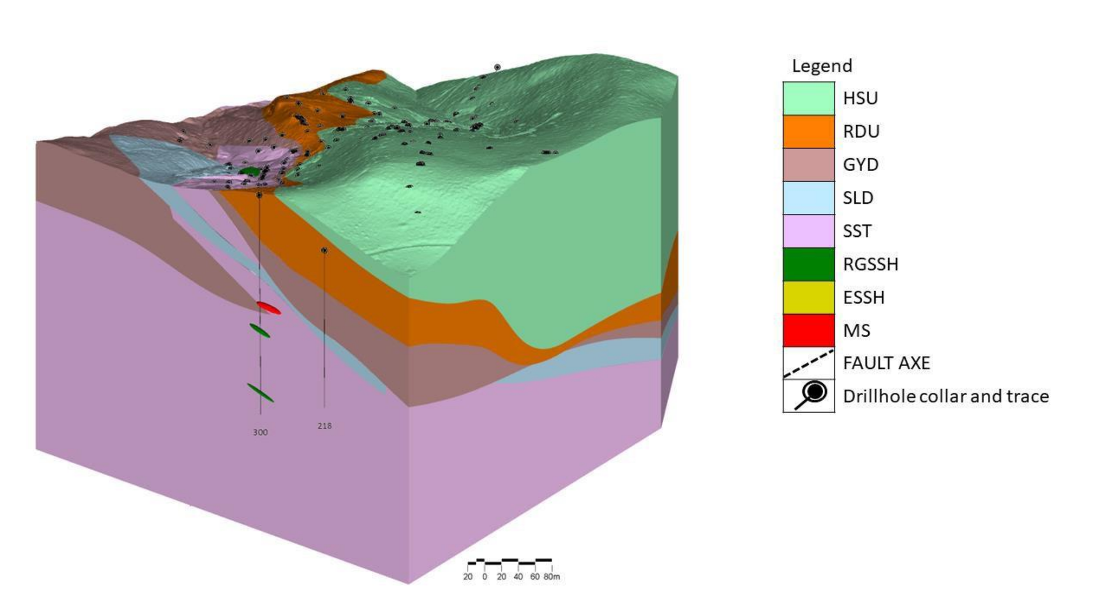


Figure 14-1: 3D Geological Model (after ADT-AMC)

Weathering

Most of the mineralisation is deeper than the weathering that affects rocks near surface so there has been no need to model weathering surfaces for the purposes of the MRE model.

Estimation Domains

The geological models that have been used for the grade estimation have been created as wireframes which outline drillhole intersections where grades are clearly elevated with respect to background.

3D low-grade and high-grade wireframes were generated for each of the metals of interest by generating contour lines on each cross section representing the grades as shown in Table 14-1.

Table 14-1: Grade Contour Values

Element	Low Grade	High Grade
Zn (%)	0.25 - 0.3	2 - 2.7
Pb (%)	0.25 - 0.3	1.1 - 1.5
BaSO4 (%)	5 - 9	30
Au (g/t)	0.4	1 - 1.3
Ag (g/t)	30 - 50	200
Cu (%)	0.1 - 0.13	1.1 - 1.3

The resultant 3D wireframes were used to code a block model such that each metal could be estimated separately into its respective high and low grade domains.

Figure 14-2 is a cross section looking northwest showing how the grade estimation domain has a folded form in keeping with the deformed nature of the geology.

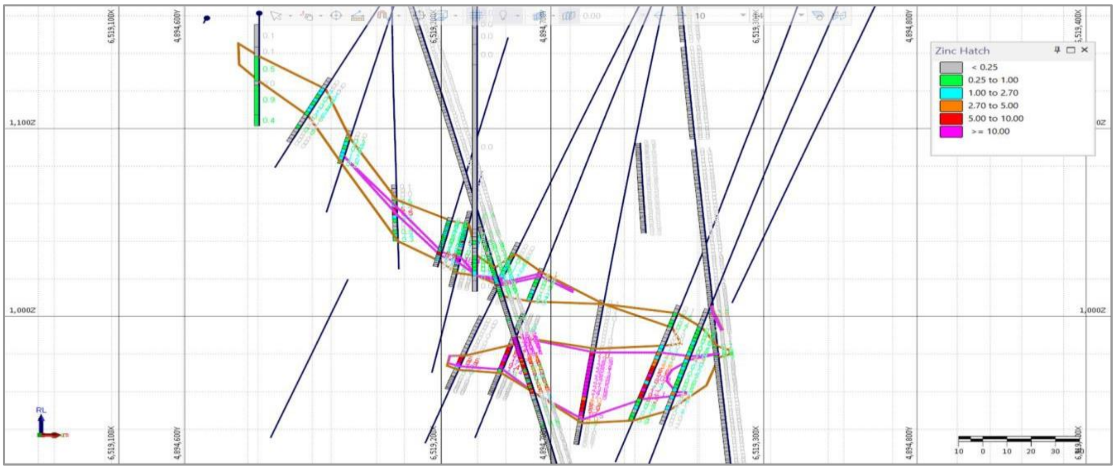


Figure 14-2: Example of Grade Estimation Domain

Figure 14-3 shows a 3D view of zinc grade estimation wireframes looking down towards the northeast.

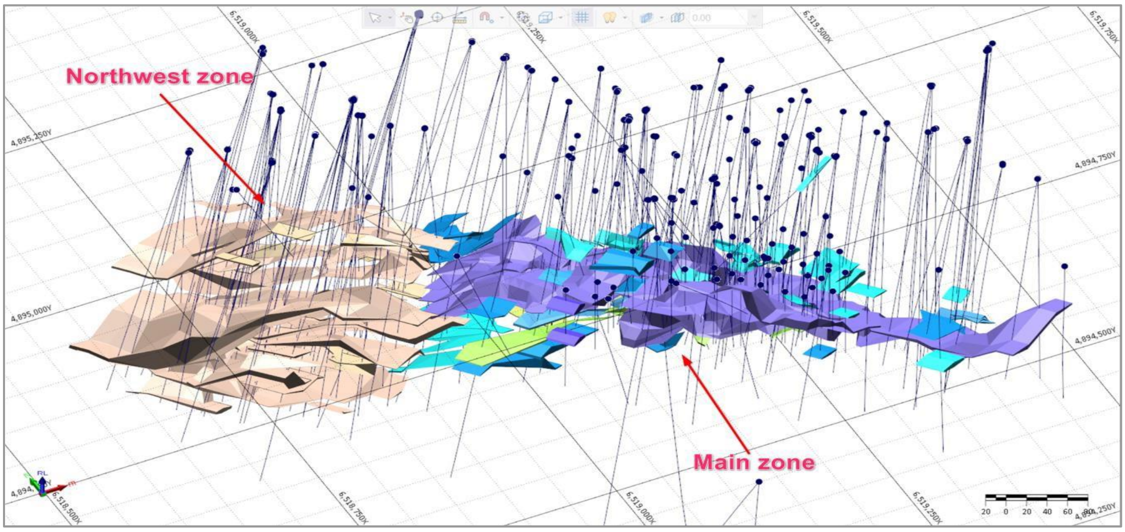


Figure 14-3: 3D view of Grade Estimation Domain Wireframes

QP Comment

The modelling has been carried out initially on cross sections which has resulted in some lost continuity in some areas. Whilst the image in Figure 14-2 shows successful interpretation and modelling of a folded feature in the Main part of the deposit, in the up-dip area part of the Northwest part of the deposit, in the QP's opinion, there remains an opportunity to improve the continuity of the deposit model by modelling a similar folded feature there too.

14.3 Statistics

Drillhole sample intervals were regularised to a 2m length using a standard compositing routine. Each composite was flagged according to the wireframe that contains it and then classic statistics were generated for each of the grade estimation domains which are summarised in Table 14-2 and Table 14-3.

Table 14-2: Classic Statistics: Main Zone

Domain (combined high and low grade)								
	Min	**Max**	**No of Points**	**Mean**	**Variance**	**Std. Dev.**	**COV**	**Median**
Zn (%)	-	39	3,102	3.49	36	6.03	1.76	0.79
Pb (%)	-	28	3,102	2.32	15	3.81	1.66	0.59
BaSO4 (%)	-	97	3,105	25	931	31	1.24	6.12
Au (g/t)	-	17	2,726	1.43	4.28	2.07	1.46	0.43
Ag (g/t)	-	5,030	2,751	154	84,680	291	1.96	39.60
Cu (%)	0.00	8.2	2,737	0.39	0.50	0.71	1.80	0.16
Sb (%)	-	3.3	2,668	0.20	0.08	0.29	1.47	0.09
As (%)	0.00	2.2	2,618	0.06	0.01	0.11	1.67	0.04
Hg (%)	-	0.6	3,105	0.01	-	0.02	2.19	0.00
S (%)	0.01	42	2,618	8.57	50	7.10	0.82	5.41

Table 14-3: Classic Statistics: Northwest Zone

Domain (combined high and low grade)								
	Min	**Max**	**No of Points**	**Mean**	**Variance**	**Std. Dev.**	**COV**	**Median**
Zn (%)	0.00	40	2,996	4.07	43	6.57	1.64	0.81
Pb (%)	0.00	39	2,996	2.52	19	4.38	1.76	0.47
BaSO4 (%)	0.01	98	2,996	25	1,054	32	1.33	4.05
Au (g/t)	0.00	22	2,996	0.75	2.75	1.66	2.22	0.15
Ag (g/t)	-	3,458	2,996	128	64,620	254	1.99	33.15
Cu (%)	-	16.7	2,996	0.35	0.81	0.90	2.53	0.08
Sb (%)	0.00	10.0	2,996	0.14	0.16	0.40	2.80	0.04
As (%)	0.00	1.0	2,996	0.05	0.01	0.10	1.86	0.02
Hg (%)	-	0.3	2,996	0.01	-	0.03	2.16	0.00
S (%)	0.02	40	2,996	8.78	56	7.46	0.85	5.11

Histograms of the original grade distributions were used to determine threshold values for each domain, above which grades were considered to be outliers rather than part of the main distribution curve. Table 14-4 summarises the threshold values identified by this process; these were used as capping restrictions in the grade estimation method.

Table 14-4: Threshold Values

Element	Main Zone		Northwest Zone	
	Low-grade	High-grade	Low-grade	High-grade
Zn (%)	6	-	5.47	-
Pb (%)	3.7	-	5	-
BaSO4 (%)	50	-	-	-
Au (g/t)	4	-	2.3	-
Ag (g/t)	-	N/A	-	3000
Cu (%)	-	-	-	-
Sb (%)	-	N/A	3.8	N/A
As (%)	0.93	N/A	0.92	N/A
Hg (%)	0.13	N/A	-	N/A
S (%)	35.7	N/A	36.3	N/A

Any grade values exceeding the threshold were reduced to the threshold value ahead of the compositing step.

14.4 Geostatistics

All variograms were calculated and modelled using the composited sample file constrained by the corresponding mineralised envelopes for each element. In cases, when low-grade and high-grade domains were modelled the samples were combined for both domains to achieve the most robust geostatistical analysis.

It was found that absolute semi-variograms were difficult to model and therefore, pair-wise relative semi-variograms were modelled for all elements. experimental variogram models were generated for each element to estimate the potential nugget effect (C0), which was subsequently used for the directional variogram models.

Directional variograms were created for each metal of interest in directions which represent the average plunge and dip of the deposit.

Nugget variance is typically in the range of 25% - 45% of total variance.

The balance of variance was modelled in 2 structures with combined ranges of

- Downhole : 20 m – 50 m (lowest for As)
- Plunge direction : 120 m – 200 m (lowest for As)
- Downdip direction : 100 m – 165 m
- Perpendicular direction : 30 m – 50 m

The longest ranges are for barite underpinning the significance of its presence in the mineralised package. The lowest ranges belong to arsenic (these variables were estimated in the block model although not reported in SRK's MRE statement).

14.5 Block Model Description

A block model has been used to represent the Rupice deposit, the details of which are given in Table 14-5; the framework completely includes the geological wireframes.

Table 14-5: Block Model Framework

Axis	Minimum	Maximum	Block size (m)	Minimum sub-celling size	No. of parent blocks
Easting	6,518,647.5	6,519,602.5	5	1	191
Northing	4,894,397.5	4,895,302.5	5	1	181
RL	597.5	1,252.5	5	1	131

14.6 Grade Estimation Parameters

Grade estimation has used search ellipses whose orientation varies according to the dip and strike of the estimation domain at any particular location, termed ‘dynamic anisotropy’, see Figure 14-4.

The QP considers this to be a well suited method for this type of deposit model; it copes with the slight variations in dip and azimuth, whilst it does not follow around fold nose closures the QP does not consider the extra effort of attempting an unfolded modelling and estimation approach is necessary as long as underground grade control drilling ultimately provides more detailed information in these areas.

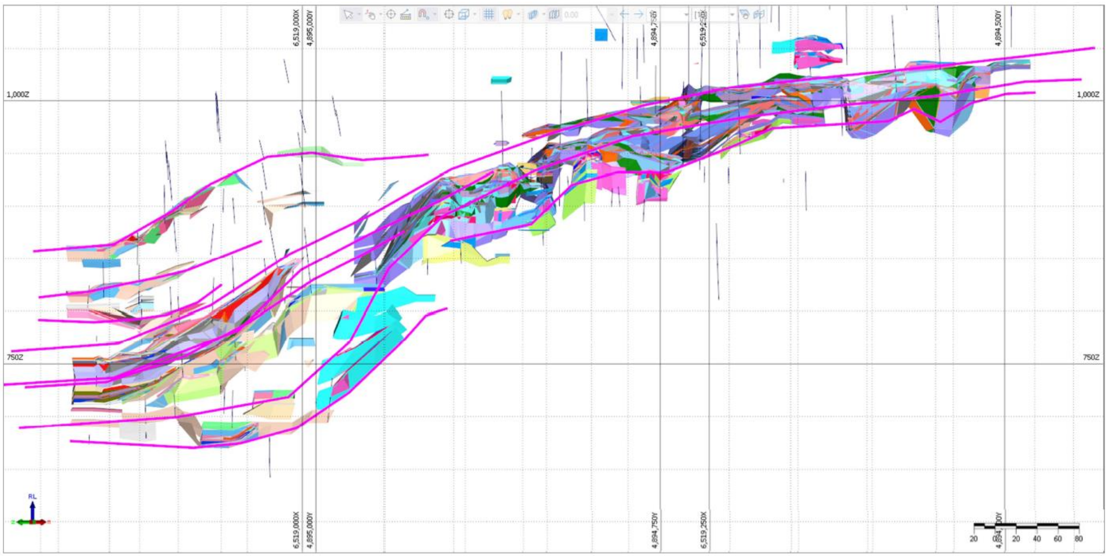


Figure 14-4: Dynamic Anisotropy Guidelines

A multi-pass estimation strategy was used. Blocks assigned a grade in the first pass were estimated by between 3 and 16 samples from at least 2 drillholes within a search ellipse with radii equivalent to 1/3 of the average variogram range. Any estimated blocks went to the second pass which required similar criterial within a search ellipse with double the radii length used in the first pass. The third pass required similar criterial within a search ellipse with triple the radii length used in the first pass. The fourth pass used between 1 and 16 samples within a search ellipse with 6 times the radii length used in the first pass.

Quadrant declustering was used which is good practice particularly if there are areas with different drillhole spacing.

14.6.1 QP Comments

Local Estimation Quality

Whilst ADT's report suggests that grades were estimated into 5x5x5m parent cells, the QP's review suggests that estimation was made into 1x1x1m sub-cells which is not ideal for local estimation quality; however the QP has visually checked the block grade distributions and there are no major concerns arising from risks associated with small estimation block size.

Sum to 100 issue

However the QP has noted that a small proportion of blocks carrying the highest grades have an issue where the assays representing the sulphides and the barite sum up to greater than 100%. This is a commonly encountered issue when estimating multiple grade variables representing minerals that make up the entirety of the rock. The QP ran checks to assess the materiality of this error and found that the overall effect is not concerning, the block grades have not been adjusted in the block model used for reporting current Mineral Resources and Ore Reserves in this report.

There is a risk however that metal values in very high grade areas will be overstated on a local basis unless block grades are normalised to sum to 100%.

Density weighted estimation opportunity

Density in the deposit is highly variable and correlated with metal grades; in the QP's opinion it would be most appropriate to estimate a density value for every composite sample used in the block model grade estimation and to use that density value as a supplemental weighting factor which most grade estimation software is set up to allow.

Without implementing this density weighting step, there is a likelihood that high grades are somewhat underestimated and low grades may be somewhat overestimated.

14.7 Tonnage Estimation

The density values were estimated into the block model using regression formulas applied to the estimated block grade values. ADT and their consultants reportedly derived these formulae using scattergrams for density vs barite, lead, copper and zinc grades.

14.7.1 QP Comments

The QP was unable to review the detailed logic behind the density formulae. Given how variable the density is in Rupice and how sensitive metal content and therefore project revenue are to density, the QP undertook a reasonably detailed check exercise. Firstly, multielement assay values were assigned the drillhole intervals which were originally used to determine density values. Then, the element assay values were used to estimate sulphide and barite mineral proportions. Textbook mineral densities were combined in these proportions along with assumed gangue density to estimate the density of the whole rock for each sample.

A spot check was undertaken to confirm that the QP estimate generally compares well with the Archimedes density determination. A subsequent spot check was undertaken on block estimated grade values and the QP density estimate based on block grade values was compared with the density estimated in the block model by ADT-AMC; these also compared reasonably well but it was clear in some blocks that failing to account for the Fe assay and the contribution to density from pyrite may have resulted in underestimated density in iron-rich areas.

In summary the QP has adopted the ADT-AMC density estimate and expects in reality that slightly higher densities will actually exist in more pyritic ore.

14.8 Validation

Validation of the grade estimates was completed by:

- Visual checks on screen in cross section and plan view to ensure that block model grades honour the grade of sample composites.
- Statistical comparison of sample and block grades.
- Generation of swath plots to compare input and output grades on easting, northing and elevation plots

Figure 14-5 is a cross section through the block model showing the successful application of high and low grade domains and how the sub-blocking method gives an accurate representation of the wireframe geometry.

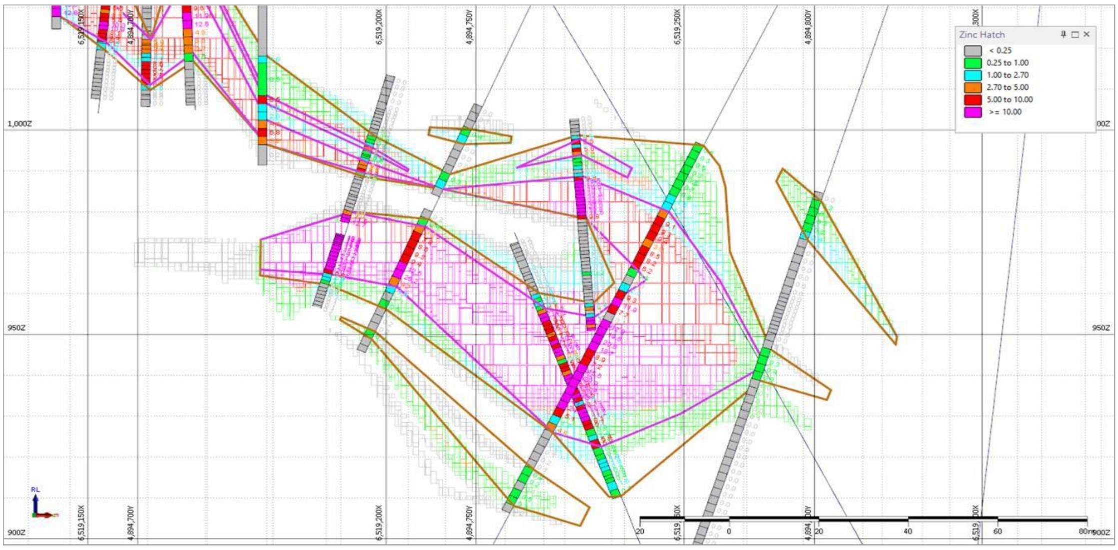


Figure 14-5: Example Cross Section through the Grade Block Model

14.8.1 QP Comments

The QP has similarly undertaken visual and statistical checks, and considers the estimate to be reasonably robust, notwithstanding comments in 14.6.1.

14.9 Depletion

The mine survey pick-up was done by the ADT mine engineering team. The mine survey data contained a union solid wireframe of access development and stopes to 31 December 2024. The wireframe rendition of the as-built survey was verified and validated by the mine engineering team. This was then used to code blocks as having been excavated so the ore tonnage and metal could be subtracted from the block model.

Ore production started in August 2024, the main stoping activities were on the 1050-1075 and 950-975 levels. Some 165 Kt was depleted from the orebody model in this time, the undiluted grades according to ADT-AMC's report from the block model were:

- Ag 243 g/t
- Zn 5.1 %
- Pb 3.4 %
- Au 2.3 g/t
- Cu 0.5 %
- Sb 0.2 %

In addition to the 31 December 2024 "as-built" depletion described above, to forward-deplete to 1 April 2025 a further 67 kt was subtracted from the report (based on Q1 production) at the following grades:

- Ag 183 g/t
- Zn 4.3 %
- Pb 2.4 %
- Au 1.4 g/t
- Cu 0.4 %
- Sb 0.1 %

14.9.1 QP Comments

The QP has not been able to compare the depleted tonnage and grade according to the block model with production records and stockpile movements and cannot therefore comment on overall reconciliation.

Stockpiled material is assumed to be zero for the 1 April 2025 report.

14.10 Classification

ADT-AMC used the classification terminology given in the JORC Code which is very similar to that given in the CIM Code, the QP considers the terms to be interchangeable between the codes.

The classification coded into the block model by ADT-AMC reflects the following :

- Measured: Not reported, the QP agrees this is more appropriate after grade control data is available and after a robust reconciliation exercise has been completed.

- Indicated classification is assigned to blocks which are estimated by drillholes spaced at less than approximately 40 m by 40 m and where at least two mineralisation intersections exist on a drill section. In addition the geological structures must be relatively well understood and robustly interpreted.
- Inferred classification is assigned to blocks lying outside the Indicated wireframes, where there is reasonably expected strike continuity and generally no further than 50m from drillhole and trench intersections.
- Figure 14-6 shows in plan view, the blockmodel coloured green for Indicated and orange for Inferred. This shows that many areas are very well supported by drilling, whilst areas with sparser drilling coverage and more distant flanks are appropriately classified in the low confidence Inferred Mineral Resource category.

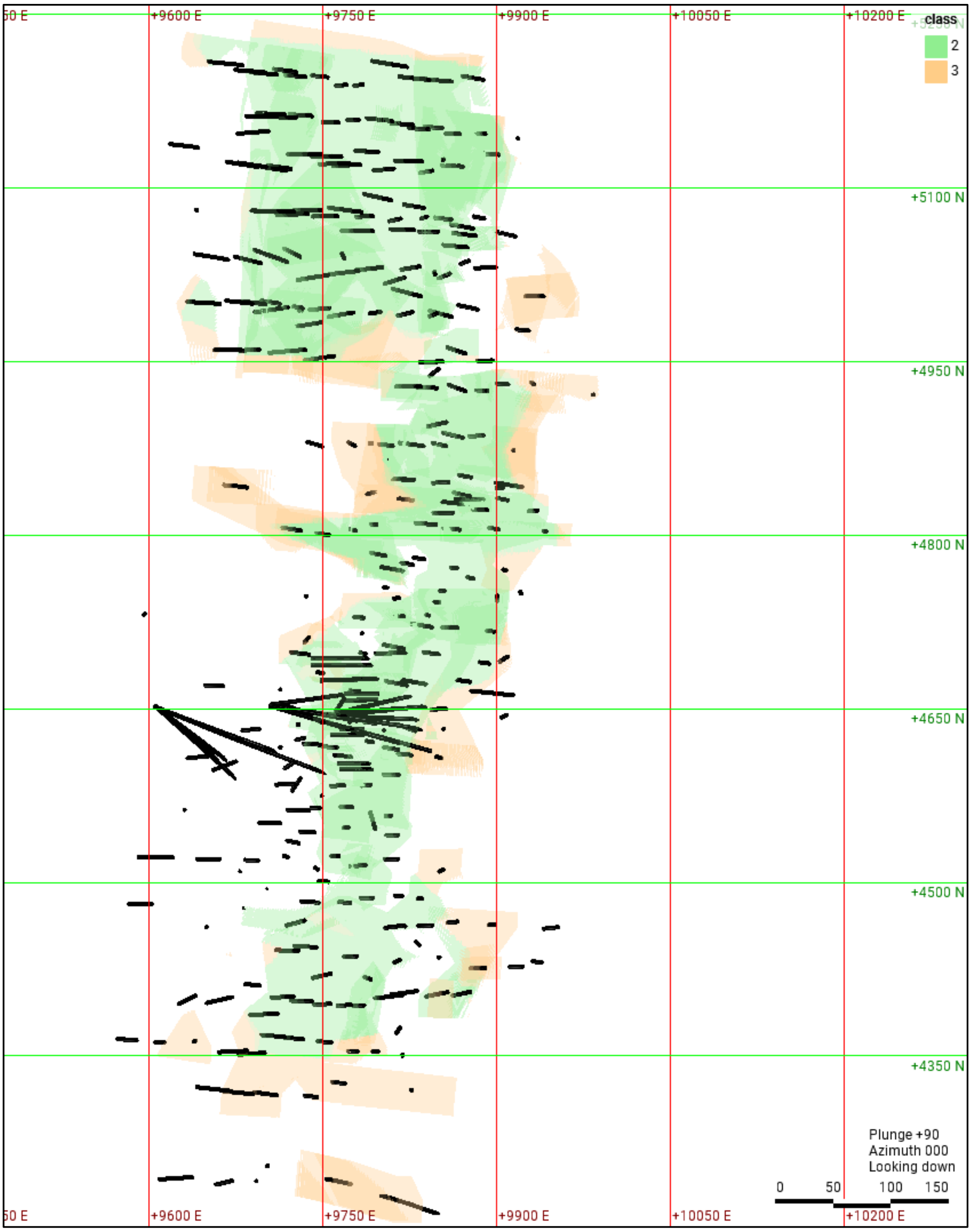


Figure 14-6: Block Model Classification with respect to Drillhole Location

14.10.1 QP Comments

The QP agrees that the majority of the drilled deposit has been sufficiently covered by good quality diamond drilling which allows for reasonable confidence in the geological interpretation and grade estimation in most areas. Much of the Inferred Mineral Resource comprises thin extensions extrapolated beyond the well drilled thicker parts of the deposits and also some isolated thin mineralised features stratigraphically above and below the main mineralised horizon; some of these are small features centred on single drillholes.

Although not stated in the ADT-AMC reports, the data quality and absence of bias are also important considerations for Mineral Resource classification; the QP believes comprehensive measures were and are in place ensuring good quality control for sample preparation and assaying; the drillcore inspected by the QP was good quality and the logging and sampling procedures are of a good standard and the equipment for density determinations was well designed and in good condition. The data quality is sufficient in the QP's opinion to support Indicated confidence.

14.11 Reasonable Prospects of Eventual Economic Extraction

14.11.1 Technical-Economic

The QP has reviewed the DPM cash flow model and has used the metallurgical recoveries, the net smelter return parameters, the royalties, the long term metal prices and the forecast operating costs from the model.

For the purposes of assessing RPEEE and to derive a cut-off value for reporting the Mineral Resource, a 25-30% premium was applied to each of the metal prices.

For each of the revenue deriving metals, a net revenue factor was calculated which combines

- metallurgical recovery,
- attributable concentrate shipping costs,
- attributable smelter treatment costs and refining charges and
- royalty payments

For each block the QP calculated the contained metal, multiplied this by the metal price including premium, then multiplied this by the net revenue factor to calculate net dollar revenue attributable to each metal; Table 14-6 gives these parameters. The values for each metal were summed to calculate a total net value for each block.

Table 14-6: Net Block Value Parameters used for Mineral Resource Reporting

Contained Metal	MRE Price (incl. Premium)	Net Revenue Factor
Zn (t)	3,450	60%
Pb (t)	2,600	74%
Cu (t)	11,500	18%
Au (oz)	2,900	44%
Ag (oz)	35	75%
Sb (t)	2,990	10%

According to the cash flow model a cut-off value of USD 100/t will be sufficient to cover the underground mining cost, the processing cost and the general and administration cost. This has been used as a cut-off value when reporting the Mineral Resource.

14.11.2 Environmental-Social

The environmental and social licence to operate is based on the permitting described in this report and the fact that the mine has already been in operation.

14.12 Mineral Resource Statement

Mineral Resources are not Mineral Reserves. There is no guarantee that those Mineral Resources yet to be converted to Mineral Reserves will eventually be converted to Mineral Reserves.

No Measured Mineral Resource was reported. The Indicated Mineral Resource that was not modified to produce the Mineral Reserve do not have demonstrated economic viability.

There is no guarantee that further work will be able to increase confidence of the Inferred Mineral Resources to Indicated Mineral Resources.

Table 14-7 provides the QP's Mineral Resource statement.

Table 14-7: Rupice Mineral Resource Statement – 1 April 2025

Mineral Resource	Tonnage (Mt)	Ag (g/t)	Zn (%)	Pb (%)	Au (g/t)	Cu (%)	Sb (%)
Indicated	10.7	264	7.4	4.8	1.9	0.65	0.22
Inferred	0.9	150	3.5	2.8	0.8	0.37	0.15

Rupice Mineral Resource Accompanying Notes

Basis of Mineral Resource estimation

- The QP responsible for the Mineral Resource is listed in Item 2.2.
- The Indicated Mineral Resources stated here are inclusive of those Indicated Mineral Resources that have been modified to produce the Mineral Reserves.
- Indicated and Inferred Mineral Resources are not added and presented as a total, following the CIM Definition Standards.
- The Mineral Resources are reported above a cut-off MRE_NSR value of USD 100t; it is a direct report from the ADT block model without consideration of mining shape optimisation. The MRE_NSR value resulting from the average metal grades in the MRE (approximately USD 540/t above a cut-off value of USD 100/t).
- The Mineral Resources are reported on the basis that they are planned to be mined via long hole open stoping, processed via a known demonstrated process route, and sales concentrate delivered to market. At presented this is supported by technical studies perceived to be at PFS or FS level of confidence. Risks associated with the technical feasibility and economic viability of extraction remain, relating to unknowns, though these are greatly reduced as mining has commenced, the process plant has been commissioned, and early concentrate sales have taken place, thereby shedding light on numerous previous unknows have now been identified and are being addressed.
- Mineral Resources may further be materially affected by any known environmental, permitting, legal, title, taxation, socio-economic, marketing, political, or other relevant factors.

14.13 MRE Sensitivity

The tonnage and average NSR value will change according to the cut-off value according to the relationship shown in Figure 14-7. The tonnage will decrease and the average NSR value will increase in response to any increase in the cut-off value, and vice versa.

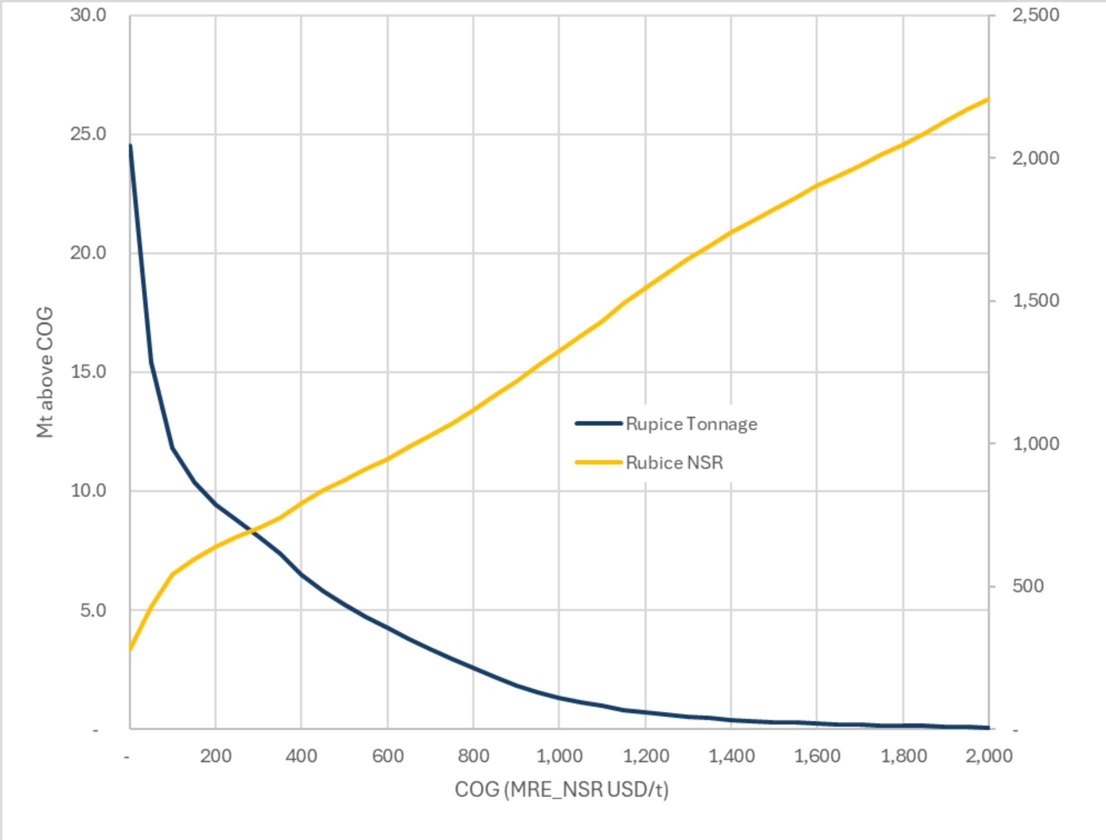


Figure 14-7: Grade Tonnage Curve

14.14 Comparison with Previous Estimates

The previous Mineral Resource statement produced by ADT is provided in Table 6-1. Whilst the QP has used the same block model as was used for this, unmodified by updated drilling information, there is a considerably lower tonnage in the QP statement. This is due to having updated the cut-off grade to reflect that used in the Mineral Reserve statement which incorporates much higher operating costs than were used in previous cut-off grade determinations.

ITEM 15. MINERAL RESERVE ESTIMATES

15.1 Historical Mineral Reserve Estimates

The previous Mineral Reserve estimates are presented in Item 6.4.

15.2 Mineral Reserve Statement

The Rupice Mineral Reserve Statement and Accompanying Notes dated 1 April 2025 were signed off by the QP and is presented in Table 15-1.

Table 15-1: Rupice Mineral Reserve Statement – 1 April 2025

Mineral Reserve	Tonnage (Mt)	Ag (g/t)	Zn (%)	Pb (%)	Au (g/t)	Cu (%)	Sb (%)
Proved	-	-	-	-	-	-	-
Probable	9.46	228	6.8	4.3	1.7	0.57	0.18
Total	9.46	228	6.8	4.3	1.7	0.57	0.18
Rupice Mineral Reserve Accompanying Notes							

Basis of Mineral Reserve estimation

- The QPs responsible for the Mineral Reserve are listed in Item 2.2.
- The Mineral Reserve was derived from the Mineral Resource dated 1 April 2025, presented in Table 14-7.
- The entire Indicated Mineral Resource has been considered for the Mineral Reserve. Therefore the only opportunity to increase the Mineral Reserve would be to increase the Indicated Mineral Resource, through upgrading of Inferred to Indicated or further exploration.
- To enable the depletion of the Mineral Reserve to the date of 1 April 2025, the QP used the Q1 2025 production tonnage and estimated grades. Actual production will differ, which is not deemed material to the Mineral Reserve Statement. No stockpiles were included.
- The Mineral Reserve is reported on a 100% attributable basis.

Hydrogeology

- There are gaps in the hydrogeological understanding that present a risk to mine production and project costs, if dewatering inflows exceed currently planned capacity. Additional drilling and testwork will be required to manage these risks.

Geotechnics

- As ADT has advanced underground development and stoping, the geotechnical conditions are now better understood. Whereas the ore is mostly competent rock, the waste rock is variable with some weak to very weak zones. ADT has put much effort into improving ground support and demonstrated that this can be adequately managed. The QP considers that the measures put in place by the mine operations team to deal with the geotechnical challenges are appropriate and conform to industry best practice. The impact on cost has been material / significant and is included in the economic analysis. DPM has further changed the mining method, which is expected to have a positive impact.

Mining

- The mining method and design will change under DPM ownership, from longhole open-stopes mined underhand, downwards, from upper levels, to longhole open-stopes mined overhand, upwards, from lower levels. Some mechanised cut-and-fill stoping will also be introduced. The QP deems that the mine plan generated by DPM is achievable and meets a pre-feasibility level of study as a result of the designs and scheduling being preliminary, and cost estimation limited. The QP notes that the geometry of the deposit and applicable mining method result in a mine plan that will require fine attention to multiple well sequenced activities.
- Modifying factors for unplanned dilution and loss (external to stope shapes) were determined for each stoping type and average 12.5% and 6.5% respectively.
- NSR cut-off grades of USD100/t for longhole open stopes and USD120/t for mechanised cut-and-fill stopes were used to select designs for inclusion in the Mineral Reserve. The long term commodity prices applied in the estimation of the Mineral Reserve are: zinc USD 2,661/t, lead USD 2,064/t, copper USD 9,348/t, gold USD 2,212/oz, and silver USD 28/oz. In order of priority,

revenue is generated from silver, zinc, followed by lead and gold, and minor contributors are copper and antimony.

- The QP notes that the projected full production rate is 850 ktpa run of mine, with no planned expansion. Underground development for the change in mining methods is yet to be commenced. To steadily ramp up to full production, stoping activities and production rate are dependent upon the permitting and commissioning of the paste backfill plant. Delays in permitting of the paste backfill plant remain a key risk and will have a direct impact on production.

Processing

- The process plant flowsheet as built is consistent with the design as per the DFS. The recovery relationships used in the NSR calculation were derived from the PFS testwork, however the subsequent DFS testwork results were consistent with these relationships. Ramp up to full steady state production has not yet been achieved. The metal recoveries are well supported by test work, however actual metal recoveries are not yet known with confidence, and meaningful reconciliation is some time away.

Tailings Management

- The Veovaca TSF is being constructed within the historic Veovaca open pit and is designed as a filtered stack to store tailings not required for backfilling. The tailings have been classified as potentially acid-forming, with the potential to leach metals and sulphides if exposed to atmospheric conditions. To mitigate environmental risks, the TSF is lined to prevent groundwater contamination, and contact water will be collected in a catchment pond and reused in the VPP. Progressive closure of the TSF will involve capping it with an impermeable clay layer, waste rock, and topsoil to promote natural vegetation growth. Prior to the completion of the Veovaca TSF, a temporary lined TSF was developed north of the VPP to accommodate tailings during initial mining operations. Once the Veovaca TSF is operational, the tailings from the temporary facility will be relocated to the Veovaca TSF.

Water Management

- The water treatment and sediment management capacity are being increased. The surface water management at the mine site is being changed and will be able to inform a more robust water balance, that incorporates aspects like climate change.

Infrastructure

- The mine infrastructure is mostly built.
- The haul road to transport tailings needs to be built as the temporary road can only be used until 2 June 2025.

Processing

- An understanding of waste rock geochemistry is available through previous testwork but the waste management strategy needs to be re-visited for the revised LoM plan by DPM

Permitting

- There are uncertainties relating to the status of permitting and compliance. DPM is an operator in the Balkans, and is focused on putting commensurate effort to address permitting shortcomings in collaboration with the appropriate regulatory authorities.

Costs

- Initial capital costs amounting to USD 76 million and sustaining capital costs amounting to USD 133 million have been projected (excluding USD 24 million as a closure cost allowance), along with life of mine operating costs totalling USD 1,050 million.

Economics

- The economic analysis undertaken results in a positive NPV of USD 1,608 million at a discount rate of 5%.

Integration Plan

- DPM is developing an Integration Plan as part of DPM taking over ownership and operation of the Vareš Mine. This is a short term plan which will be deployed until the point at which the Vareš Mine is projected to achieve full production (Dec 2026). DPM is developing an Integration Plan as part of the Transaction. This is a short term plan which will be deployed until the point at which the Vareš Mine is projected to achieve full production (Dec 2026). The QP expects the Integration Plan to address DPM's planned change to the mining method, mine ventilation, revision to paste backfilling and reticulation, waste rock disposal, remediation of the temporary tailings storage facility, improvements to the power supply (notably to underground operations and the process plant), increase in water treatment capacity, and the condition of the haul road.

Study Level

- The overall level of study is deemed to be at pre-feasibility study, whereas some components are at feasibility level (refer to Table 2-2) and some are now actuals and known. Whereas pre-feasibility is a lower confidence level of study than the DFS issued in 2021, DPM now has the benefit of construction and initial production having identified a number of unknowns which are being addressed.

ITEM 16. MINING METHODS

16.1 Geotechnical Considerations

16.1.1 Referenced Information

The study information provided at the time of the review is listed in Table 16-1. Several documents were referenced in the larger study reports. However, these were not specifically supplied, namely the more recent 2021 and 2023 Avoca Geotechnical Ltd. ("AGL") study update reports. Additionally, no recent operational reports from ADT were available to assess in detail. Instead, these are interpretations of items determined from the site visit discussions in March 2025.

Table 16-1: Available Geotechnical Information

Document Title	Author/Source	Date	Available for Review
A Geotechnical Study of the Vareš Project	Avoca Geotec	September, 2019	Yes
A Geotechnical Study of the Rupice Project	Avoca Geotec	August, 2021	No
Vareš and Rupice Feasibility Study Report	Ausenco	September, 2021	Yes
Stope Stability Modelling at Rupice Mine	Avoca Geotec	May, 2022	No
Rupice Ore Reserves Report	AMC	December, 2023	Yes
Rupice North West Structural Model	Transition-Elements	February, 2024	Yes

The AGL report details the geotechnical investigation at the FS study level. There is further updated mine design and numerical analysis reporting completed but not made available to the QP. Therefore, this review is limited to the pre-mining study reports, along with observations and discussions during the site visit.

In general, ADT indicated that the rock mass conditions were expected to be variable as determined from the study investigations, primarily sourced from the surface diamond drilling program logging (11 drillholes) and core rock strength testing (documented in AGL, 2019). The litho-structural model of the Rupice orebody indicated the Veovača prospect is a very complex tectonic assemblage of sediments, intensively faulted and folded with frequent reverse faulting. A series of well bedded porous dolomitic limestones, limestones, dolomitic marl, marl limestones, shales and various sandstones, host the mineralised brecciated orebody. A variable degree of alteration influences the rock mechanical properties at the sub 10 m scale.

As discussed by ADT during the March 2025 site visit, the mine commencement encountered challenging rock conditions which impacted rates of development and increased ground support costs. The development process was established from this experience and appropriate methodologies were formulated to deal with the challenging conditions and advance rates.

The QP interprets rock mass conditions as having variable strength and fracturing that is difficult to categorise uniformly at the stope scale (20-25 m height and length), and also at the tunnel development scale (5-7 m height).

16.1.2 Rock Mass Characterisation and Geotechnical Domains

The QP assessed the pre-mining rock mass characterisation, structural geology modelling, and direct observations of the inspected conditions present in the early developed mine. Typical cross sections of each deposit area are illustrated in Figure 16-1. The modelled lithologies and a sample of the geotechnical rock quality rating (Q Classification) are illustrated in sections relative to the extents of mine access, stope design extents, and immediate hangingwall. The QP created Leapfrog Geo model using supplied meshes and drilling information.

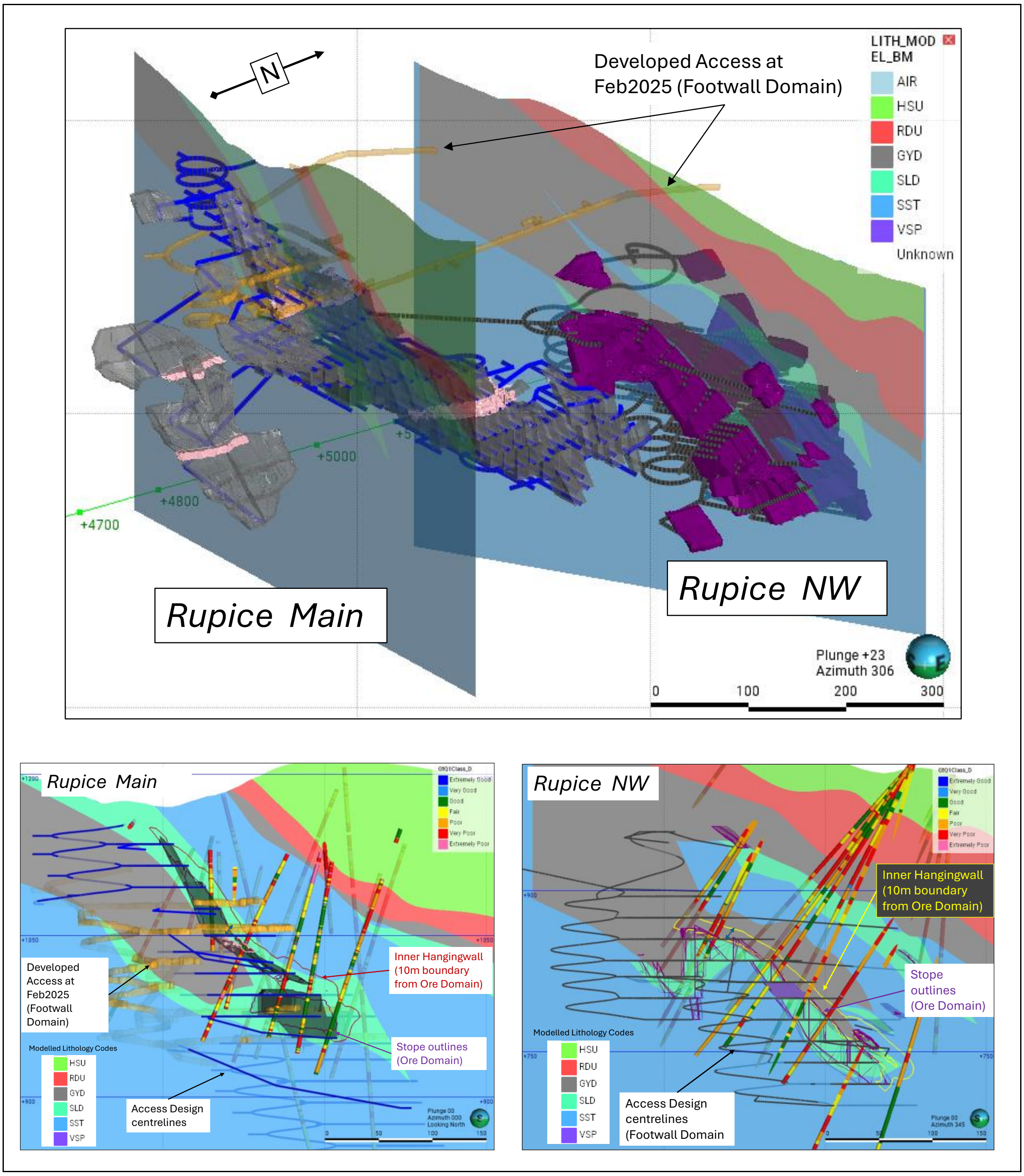


Figure 16-1: Example cross sections of mine access and stope design, and geotechnical drilling with Q Class Rating

A structural modelling study was reported in February 2024 by Transition-Elements. This study considered the complex layering, contrasting rock strength and the recorded RQD and strength index in geotechnical logging. A structural model (fault/shear model) was reported in the document. However, the supplied digital files did not qualify as representing all the modelled faults indicated by the study report. Therefore, this detail was not available for this review.

'Clay Zone' structures were reported and roughly modelled in the 3D data set applied by ADT early mine development mapping. These are considered as weak features with very poor rock quality that have contributed to large overbreak and heavy ground support installation. Ore drive construction in the Footwall area on the 1050 level was abandoned due to the clay zone faults and the access was transferred to the hangingwall side of the orebody for stoping on the upper levels.

The QP notes that the AGL (2019) study approach and summary is only pertinent to RUP Main deposit and does not include the RNW area.

Independent domaining of the deposit areas into 'Mining Domains' was completed by the QP to provide a zonation of the rock quality independent of lithology type. The calculated Q rating from drillcore logging is presented in box plots with interquartile range and median values, corresponding Q rating class for the mining domains of each deposit area, as presented in Figure 16-4. In general, the interpretation is:

- Footwall (mine access area, Figure 16-1) in both domains are variable with a wide range of Q Rating from 'Poor' to 'Fair'.
- Ore (economic boundary for stope extraction, Figure 16-1). Generally 'Fair' rating and areas of 'Good' rock quality with a narrow spread of Q rating.
- Hangingwall Inner (10 m zone from the Ore boundary on the hangingwall side, Figure 16-1). The HW inner has a high proportion of 'Poor' rating in the RNW deposit, whereas this is rated from 'Poor' to 'Fair' in the RUP main deposit.

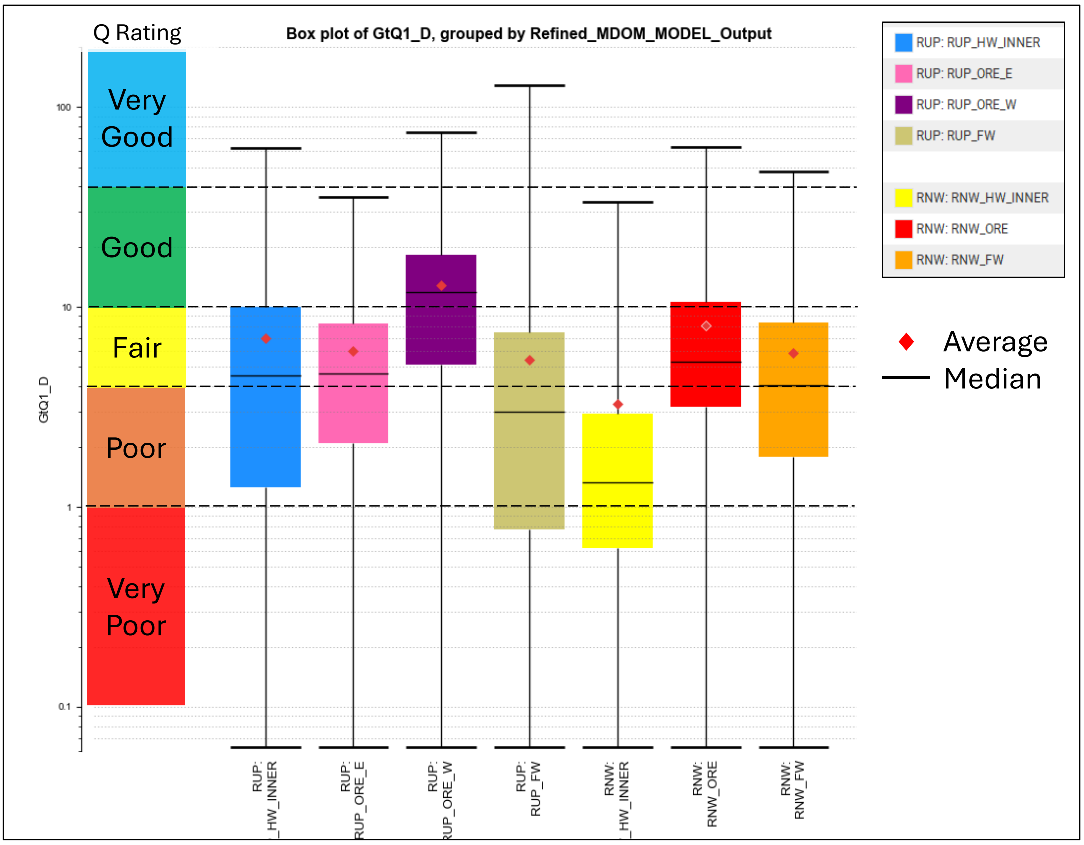


Figure 16-2: Box-plots of Q rating ranges generated by the QP from the logging database for RUP and RNW mining domains (FW/ORE/HW Inner)

Strength: AGL (2019) report, the laboratory results for Rupice show that the mean values of the UCS for the individual lithological units are relatively low, mainly because of the angle of foliation/bedding in most of the core samples submitted. The QP agrees that it is difficult to select samples due to the angle of drilling relative to the dip of the bedding. Therefore, the observations and discussions with ADT supplement the strength estimation for use in mine design.

Structure: AGL (2019) do not consider logged structures in their assessment of the initial 11 drillholes. This dataset has increased since 2019 and across both deposit areas, which was made available to DPM/SRK. A summary of the discontinuity logging, obtainable by core orientation, is illustrated in Figure 16-3.

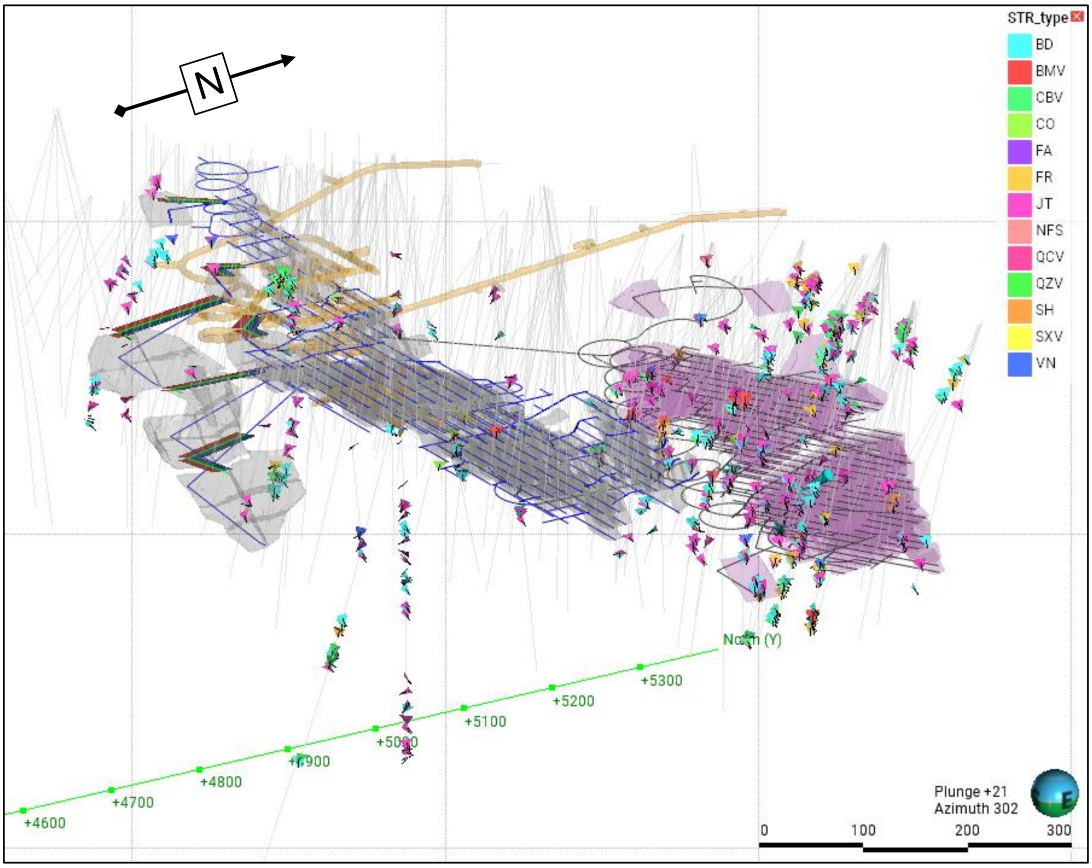


Figure 16-3: Logged discontinuities available in database

Several photos of the rock mass conditions in ore drives, stope walls and decline development faces are presented in Figure 16-4.

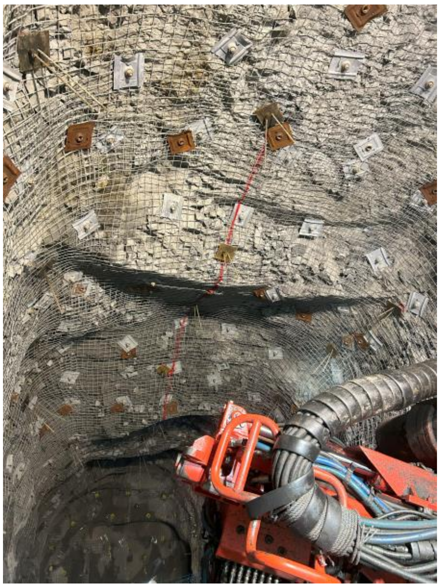
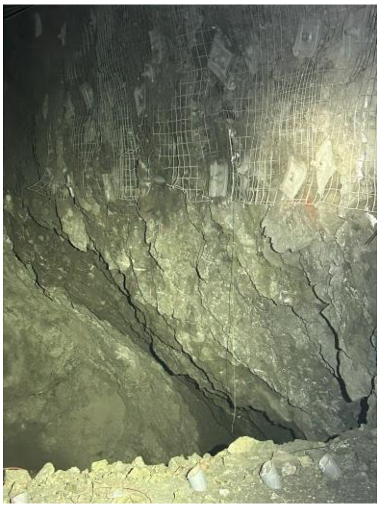
Rock Quality Comments	Example Photos at named locations and mining domains	
FW Domain 'Poor' Rock Quality. Low strength (50-80 MPa)	 Decline Development Face 925 level	 Ore drive 1050 level
Ore Domain 'Fair' Rock Quality. Moderate Strength (100-120 MPa)	 Ore drive 975 - Ore	 Ore drive wall 950 - Ore
Ore Domain boundary and HW inner 'Very Poor' Rock Quality. Very Low strength (<50 MPa)	 Stope side wall 1050 – Ore/HW Inner Domain	 TLHOS stope wall 1075 – Ore Domain

Figure 16-4: Rock quality ranges from underground observations (SRK Photos March 2025)

16.1.3 Current Stope and Performance/Condition

Design of transverse long hole open stoping (TLHOS) stope dimensions was completed in 2019 and updated in 2022 by ADT based on AGL study support. The interpretation of the stability chart method by AGL was to limit stope heights to 20 m originally (2019). However, on screen display of the 2022 AGL document viewed by the QP indicated, in the introduction paragraph, that there was a request for AGL to numerically assess the 25 m sublevel spacing and, therefore, stope height. The QP assumes AGL supported the 25 m sub level spacing to commence mining.

The early stope production has therefore progressed with 25 m stope heights from the 925 to 1075 levels, and level access elevations placed as such to extract these in top-down primary and secondary transverse stopes in alternating pattern (Figure 16-5). These are evenly designed at 15 m stope width (blast ring width) and 20 m transverse stope lengths (direction of ring firing) to form the vertical primary stope excavations. The ore drive access are centrally placed with cable bolted crowns (6.5 m lengths) and downhole production blast holes used for all extraction. Slot commencement with side cuts is completed at the hangingwall end of the stope. The experience of weak hangingwall rock mass at the ore boundary has required the installation of resin injected hollow rock bolts to pre-stabilise the opening in order to carry out slot raise drilling and firing.

At the time of the March 2025 site visit, five primary stopes had been extracted with variable performance versus expectation. Stope performance is assessed by observations and drone lidar scans of the void after each firing. The 950 - 975 level primary stopes were extracted with large upper over break on the hangingwall side related to ‘Very Poor’ rock mass conditions. The progressive stope openings are lidar scanned to track the wall fallout and volume increase rate and thus determine the maximum stable length before stope filling. This tolerable length has ranged from 15-27 m in early stope extraction reported by ADT before CAF fill placement. The development decline, footwall access, ore drives and extracted stope surveys are illustrated in Figure 16-5. Several observation photographs are presented in Figure 16-6.

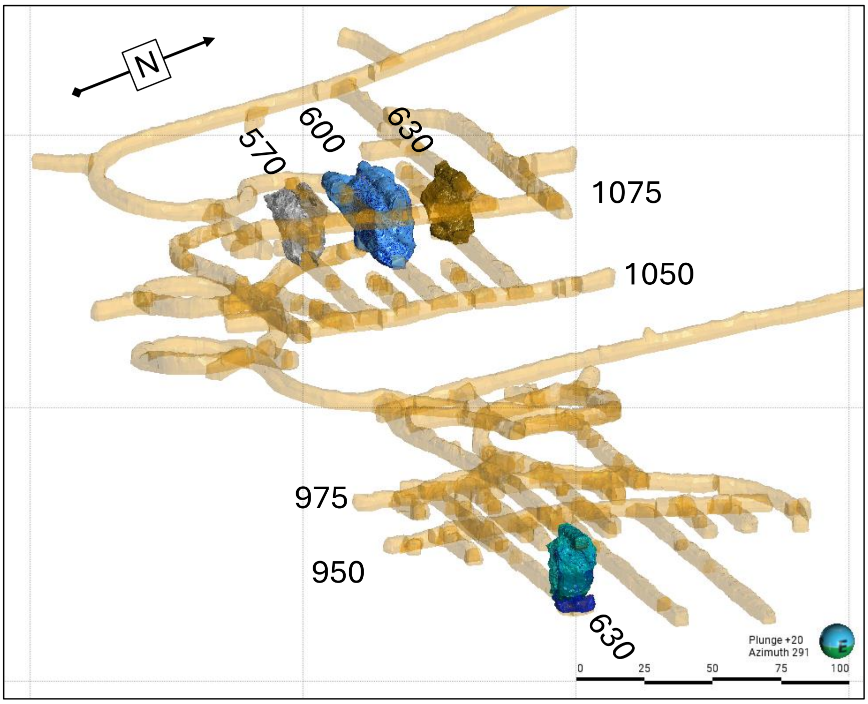


Figure 16-5: February 2025 development and stope scans – 950-1075 levels

975-630 TLHOS – left wall fallout. Note Spiling required in ore drive development

975-660 Stope at 20 m length – good condition with remaining drilled rings

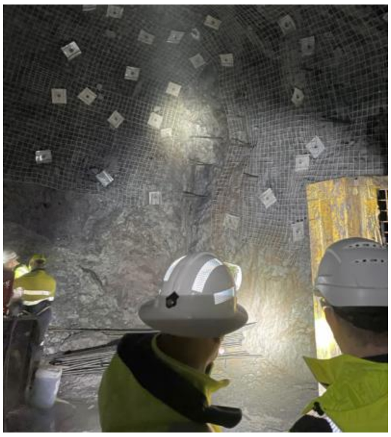
 950-630 Open Stope Bottom	 1075 660 CAF filled primary stope
 Future Secondary Stope pillar - multiple ground support tyeps installed	 1050-645 Slot end - resin injection bolts

Figure 16-6: Examples of stoping and ground support – 950-1075 levels

16.1.4 Stope Dimensioning

The QP is not authoring the stope design, rather making comment on the current analysis completed to date using an independent check method and indicating where inputs to the stability chart inputs are different to AGL initial 2019 studies, for which the QP does not disclaim responsibility. A summary table of suggested stope design parameters for the various mining methods that support the DPM mine design and plan are included in this section.

Stability chart assessment (Modified Stability Chart) conducted as a comparison to the AGL 2019 and updated for both deposit areas is summarised in Table 16-2. The inputs are:

- Q' rating from the mining domain median values determined by the QP domain modelling are used per deposit area (Figure 16-4)
- Rock UCS strength estimation from testing summary scaled by observations underground, and logged discontinuities from the supplied database for Factor A
- Dominant discontinuity sets from the logging database for Factor B and C

Table 16-2: Comparison of AGL and the QP Estimated UCS and Rock Quality

Mine Domain	Lithology	AGL 2019		SRK 2025	
		UCS (MPa)	Q' Range	UCS (MPa)	Q' Range
Footwall	**sST/SP**	22.32	0-71	80	1 - 5
Ore	**ORE**	75	0.1-68.1	100	5 - 10
Hangingwall	**LRR**	12.11	0.06-23.23	50	0.1-2
Hangingwall	**SD**	30.41	0.23-52.5	50	0.1-2
Hangingwall	**sSD**	48.91	19.67-35.42	50	0.1-2

The AGL values are based on borehole logging and laboratory testing of the 11 geotechnical boreholes drilled for the PFS. The QP estimates use the same dataset but adjusted to include visual observation of ground conditions encountered during the underground visit along with recorded stope behaviour.

The main discontinuity sets determined from the logging database are listed in Table 16-3.

Table 16-3: Major Joint Sets

Set	Dip (°)	Dip Direction (°)	Comment
J1	45	55	
J2	35	215	
J3	50	350	
J4	28	135	Orebody only

Based on the updated rock mass and structural data presented in Table 16-2 and Table 16-3, the QP used the stability graph method to provide geotechnical design guidance on stope dimensions for the DPM mine design. This guidance is summarised in Table 16-4.

Table 16-4: TLHOS Stope Stability and Design Verification Summary

Deposit / Domain/ Dip	N'	Stable HR Unsupported	Stope Height (m)	Max Stope Length (m)	Stope Width (m)	Support requirements
TLHOS		P Side wall	Fixed sub-level	P Side wall	P & S crown	
RUP Ore- Vertical	3.5	3.9	20	20-25	15	Unsupported
RUP HW End (50˚)	0.4	1.8	20	-	15	Support required
RUP FW End (50˚)	0.5	2	20	-	15	Support required
RNW Ore-Vertical	10.3	5.7	20	25-30	15	Unsupported
RNW HW End (60˚)	0.6	2.2	20		15	Support required
RNW FW End (60˚)	3.0	3.7	20		15	Support probable
LLHOS		HW side	Vertical/ Inclined	HW side		
RUP HW (55˚)	0.6	2.1	20/27	15	12	Support required
RUP FW (55˚)	0.8	2.3	20/27	15	12	Support probable
RNW HW (60˚)	0.6	2.2	20/23	15	12	Support required
RNW HW (60˚)	3.0	3.7	20/23	15	12	Support probable

RUP: Rupice Main P: Primary N': Modified Stability Number
RNW: Rupice NW S: Secondary HR: Hydraulic Radius

Transverse Stoping (TLHOS)

DPM has adjusted the stope heights for the TLHOS methods to 20 m for the extraction design planning and this vertical height is utilised for revised stope parameters comments in this review. Bottom-up extraction in primary and secondary sequencing with uniform 15 m width is the base case design. These dimensions are supported by the updated stability graph assessment.

Longitudinal Stoping (LLHOS)

Longitudinal stope orientation is designed in ore width <15 m. The stope heights in ADT are 25 m sub-level spacing and not changed by the dip of the ore. No LLHOS access or ore drives were developed at the time of the site visit. The LoM design had 15 m stope length (along strike).

DPM adjusted the stope heights for the LLHOS methods to 20 m for the mine design and planning and this vertical height is utilised for revised stope parameters.

Mechanised Cut and Fill (MCAF)

DPM is planning a significantly different approach to the narrow ore extraction with mechanised cut and fill and drift and fill approach, particularly in areas <50˚ dip. This is described in further detail in Section 16.4.4.

16.1.5 Current Development and Ground Support Conditions

Rock stability and support challenges were observed by the QP during the site visit and described by ADT personnel. The poor ground conditions, particularly in the footwall, resulted in several areas of excessive over break requiring spiling in the back and shoulders and shorter development cuts to 2 m in the worst areas, reducing the advance rate. This is particularly evident in the footwall decline and footwall level access, and where clay zones were intersected.

The ore drives have mostly had ‘normal’ full length advance (4.7 m), other than the upper 975 level in weaker ground at the top of the Ore domain. Ground support has been mainly conventional mesh and split sets, with areas having fibre-reinforced shotcrete (“FRS”) applied as well as mesh.

Ground support categories based on the Grimstad and Barton Q Support chart were adopted as the initial ground support instruction. These are illustrated in Figure 16-7 with a screen photograph of mine development coloured by the categories, as briefly described below:

- Category 1/2: Welded mesh and friction bolts (47 mm split sets) in 1.5 x 1.5 m pattern to 1.5 m from the floor (Figure 16-8, left)
- Category 2/3: The combination of friction bolts (47 mm split sets) and mechanical anchored Dynamic Rock Bolts (47 mm MD Bolts) are used in alternating 1.2-1.5 m rings. Mesh initially pinned and then 50 mm FRS layer (Figure 16-8, right)
- Cable bolts are installed (twin 15.2 mm bulbed strands) in the crown of transverse ore drives as well as in development intersections. These are hand installed with cement grout currently but are to be updated with dedicated Sandvik cable bolting rig with resin grouting for faster curing time to minimise delays.

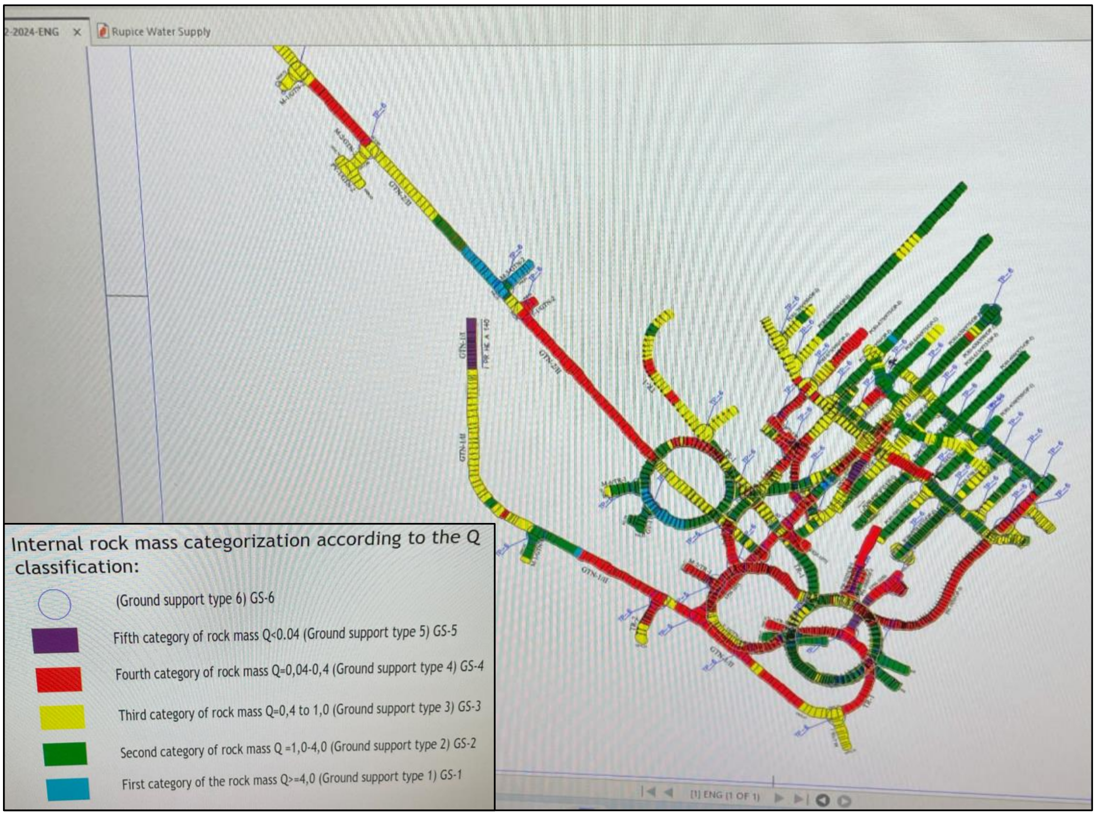


Figure 16-7: Top view of ground support categories adopted by ADT (and as installed) based on the Q support chart system (Screen photograph by SRK)

 1050 Ore drive transition from Category 2 (nearfield) to Category 1 (farfield) ground support	 950 Ore drive Category ¾ ground support, and crown cablebolts

Figure 16-8: Various ground support categories installed (Photographs by SRK)

16.1.6 Geotechnical QP Comments

The rock mass conditions at the mine provided challenges with regards to development advance, rock support and stoping performance and behaviour. Observations during the site visit indicated that the site team is very experienced and many of the geotechnical challenges are in the process of being overcome. This has been achieved by use of rock support appropriate to specific ground conditions, modifications to development advance cycles in weak ground conditions (spiling, reduction in blast length) and moving access to better ground in the hangingwall.

In order to manage the ground conditions going forward, the operation will need to ensure that geotechnical and structural models are regularly updated. Probe drilling for advance information on ground conditions should be undertaken as standard if it is not already in progress. Televiewer logging is recommended in some of the drilling to revise the understanding of fracturing and joint sets.

Stope performance also proved challenging with overbreak of stopes in places even though cable bolting of stope backs is carried out. Stope dimensions are still being tested. The 25 m high TLHOS primary stopes currently being mined are considered to be at the limit for the prevailing hangingwall ground conditions. The QP guidance for the DPM mine design is 15 m wide by 20 m high stopes, open to a maximum distance of 20 to 25 m. This guidance generally provides for a relatively low risk stope design from a geotechnical perspective.

The QP notes that secondary stopes have yet to be mined and, consequently, the performance of backfilled stopes remains to be determined. ADT reports a time dependant increase in fall-off from the walls of open stopes which can be countered by timely filling.

The QP considers that, at present, the geotechnical condition of the deposit rock mass represents a moderate risk to the successful operation of the mine. However, as mining continues and deposit knowledge increases, stope and support design can be optimised to improve stability and reduce dilution. As a result of this, over time, the geotechnical risk to the operation is reduced. In order to achieve this, appropriate data collection, interpretation, analysis and monitoring will need to be in place and run by an experienced geotechnical team.

16.2 Hydrogeology

16.2.1 Hydrogeological Characterisation

The hydrogeological setting is described in Item 5.3.

Hydrogeological investigations undertaken to support the DFS at the mine site comprised pumping tests undertaken at four wells, with water level observations in six monitoring boreholes/piezometers. Holes were drilled up to a maximum depth of 140 m below ground level, whereas the proposed underground mine progresses to a depth of around 400 m below ground level. Groundwater levels have been measured since 2018 using automated loggers.

Baseline groundwater quality at Rupice is characterized by neutral to slightly alkaline pH and a calcium bicarbonate water type, distinct from the more magnesium and sulphate-rich groundwater observed at the process plant site. Monitoring data indicate consistent exceedances of various metals.

At the processing plant and TSF area, groundwater is sampled from a single monitoring borehole, as well as from the embankment of the historical tailings storage facility (TSF) and below the base of the Veovača pit.

16.2.2 Estimation of Inflows

Groundwater inflows to the underground mine were predicted in the DFS to be low, at around 1 L/s, based on analytical estimation techniques. The QP understands that numerical groundwater modelling was undertaken by WAI subsequent to the DFS, but it is unclear as to whether the inflow estimates changed as a result as the QP did not review this work.

16.2.3 Dewatering and Inflow Management

The proposed dewatering design comprises a number of main sumps and pump stations located on six levels between the 825 RL the 1005 RL, the latter being the main transfer pumping station to send water up the decline to surface. Flow rate duties range from 4 L/s up to 16 L/s at the main transfer pumping station, the majority of which is derived from service water recirculation. Challenge Weartuff or Mono helical rotor pumps are specified for each of the main pumping stations. A secondary dewatering system will transfer water from the mine working areas to the main pumping stations using gravity drainage and portable electrical submersible pumps.

During the site visit, a single mono pump was installed with an estimated pumping capacity of around 25 L/s. It is understood that a second pump set is to be installed later in 2025.

ADT report that all underground drill holes are routinely grouted. Surface exploration drill holes are not grouted, although AM state that this is not required as the holes self-seal along the clay rich Jurassic-Triassic thrust boundary, sealing any potential connection between the underground mine and the near-surface karst-fed Jurassic aquifer.

16.3 Mining Method Selection

The selection of mining methods has evolved during the progress of establishing the Vareš Mine.

The DFS considered small span longhole open stope mining with backfill comprising cemented aggregate fill (CAF) and cemented paste aggregate fill (PAF). Stopes were primarily aligned laterally, in wide areas of orebody, with longitudinal alignment in narrow areas. A top-down underhand sequence was adopted for significant parts of the orebody. Mechanised trackless mining was assumed.

The 2023 Ore Reserve continued with the longhole open stope mining method, including underhand extraction as the basis of the strategy. The Ore Reserve estimate included material from the Rupice North-West zone. No change to the backfilling strategy was contemplated.

The DPM plan introduces mechanised cut-and-fill mining in orebodies considered too small, narrow or flat dipping for effective longhole open stoping. The majority of the Mineral Reserve is mined by transverse longhole stoping (76%), as for previous plans, with minor quantities extracted by longitudinal longhole stoping (2%) and mechanised cut-and-fill (16%). Recovery of sill pillars by uphole stoping (6%) is also deployed.

The DPM plan contemplates most of the Mineral Reserve mined with a bottom-up overhand sequence, reducing the need for the high strength backfill that would be needed to provide stable conditions for an underhand approach.

16.4 Mining Method Descriptions

The DPM plan uses 4 mining methods to extract its 9.5 Mt inventory:

- Transverse longhole open stoping (TLHOS) with backfill (7.2 Mt)
  - Applied in wide steeply dipping zones
- Longitudinal longhole open stoping (LLHOS) with backfill (0.2 Mt)
  - Applied in narrow steeply dipping zones
- Uphole recovery of sill pillars (URSP) (0.6 Mt)
  - Sill pillar extraction
- Mechanised cut-and-fill (MCAF) (1.5 Mt)
  - Applied in narrow steeply dipping ore bodies

16.4.1 Transverse Longhole Open Stoping

TLHOS has the stope long axis oriented across the orebody with a floor-to-floor sublevel interval of 20 m. Each transverse stope is extracted using blasthole rings drilled between a centrally positioned cross-cut on the crown of the stope. The blasthole rings are progressively fired, retreating from the hangingwall orebody contact towards the footwall contact. The blasted ore falls to the extraction cross-cut located at the floor of the stope. Stopes are 15 m wide with corresponding 15 m separation between cross-cut centre lines. Stopes will be mined to 20 m length (across the orebody) prior to backfilling, with repetitions as needed to fully extract the orebody, to a maximum of 5 stopes.

The stopes are identified as Primary or Secondary. Primary stopes expose no backfill walls during their extraction, whereas Secondary stopes will create one or more walls of exposed backfill. Downhole drilling and blasting are used, except in some edge areas where uphole blasthole rings are used to better match the stope shape to the orebody profile in orebody boundary areas.

As each stope is mined, it is backfilled, preferentially with cemented pastefill, or cemented rockfill if filling is required prior to pastefill being routinely available from March 2026.

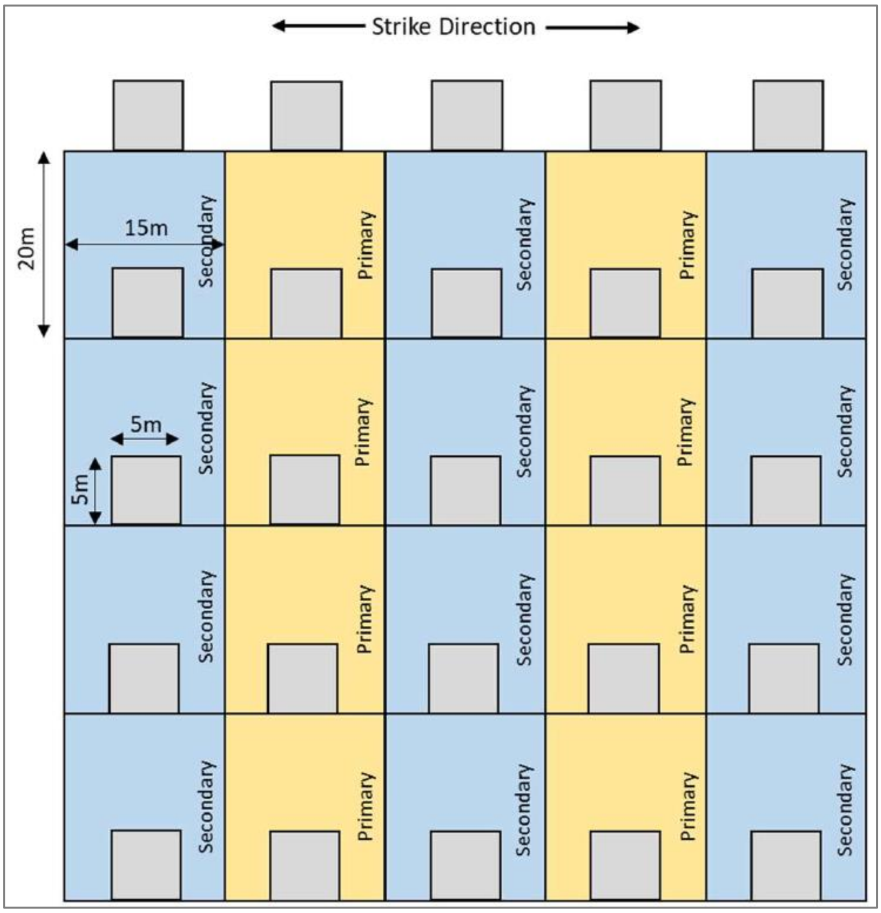


Figure 16-9: Rupice Transverse Long Hole Open Stoping Layout (Source: Ausenco)

16.4.2 Longitudinal Longhole Open Stoping

LLHOS stopes have the stope long axis oriented along the strike direction of the orebody with a floor-to-floor sublevel interval of 20 m. Longitudinal stopes are extracted using downhole blasthole rings drilled between a central drill drive on the crown of the stope and an extraction drive at the floor. The rings are progressively retreat blasted from one end of the orebody towards the other. Blasted ore is recovered from the extraction drive located at the floor of the stope. Stopes are mined to the width of the orebody, 5 to 15 m wide. Stopes are extracted to 15 m length before pastefill is introduced to maintain stability. This cycle is repeated as needed to fully extract the strike length of the orebody, which reaches a maximum of 7 stopes.

The stopes are identified as Primary or Secondary, but only the last stope in the retreat sequence can be treated as a secondary and filled with development waste. Downhole drilling and blasting are used except in some edge areas where uphole blasthole rings are used to better match the stope shape to the orebody profile in orebody boundary areas.

As each stope is mined, it is backfilled with cemented pastefill.

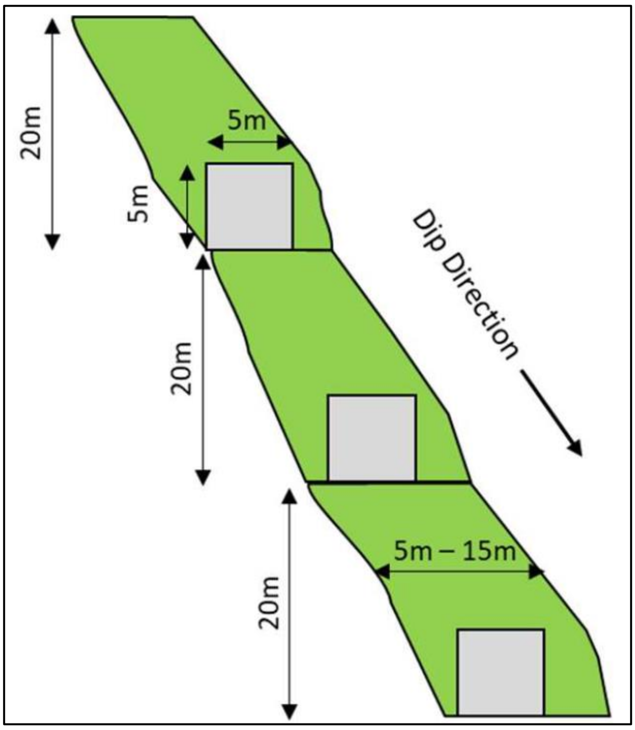


Figure 16-10: Rupice Longitudinal Long Hole Open Stoping Layout (Source: Ausenco)

16.4.3 Uphole Recovery of Sill Pillars

Sill pillars are demarcated during mining to be preserved until late in the mine life when they can be recovered using the URSP method. Sill pillars are used to separate areas and enable multiple independent stoping blocks to be exploited simultaneously, supporting an increased rate of production.

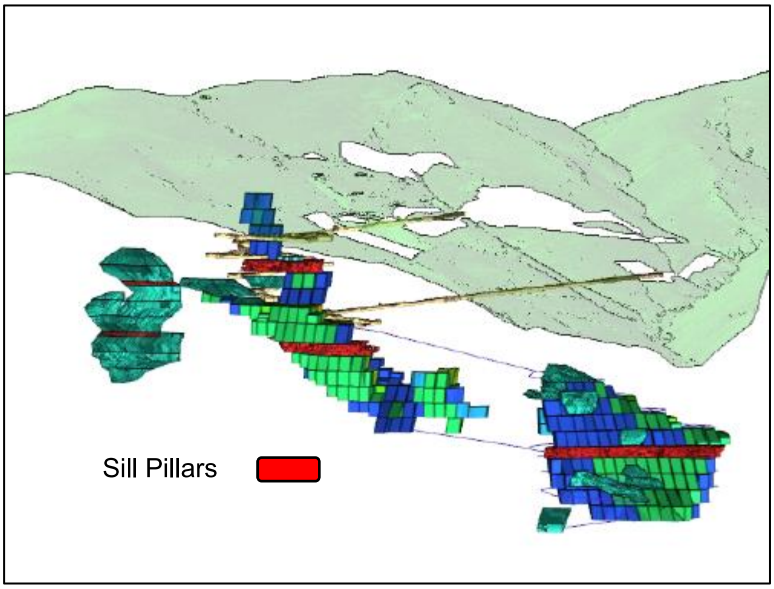


Figure 16-11: Sill Pillar Locations (Source: SRK)

Sill pillars are extracted using uphole fans drilled from the upper drill drive of the underlying stopes, which were backfilled with higher strength paste fill or CAF as a sill mat. The uphole extraction undercuts the overlying completed stopes and creates horizontal exposures of the cured fill. A very low recovery is assumed for the sill pillars to allow for potential loss of ore if there are stability problems with the backfill roof.

16.4.4 Mechanised Cut-and-Fill

MCAF is used to extract low volume orebodies which do not justify the development requirements or incur excessive ore loss or dilution if mined by longhole open stoping. Flatbacking with horizontal holes drilled by development jumbos are used for most parts, with drift-and-fill used where required by the combined effects of large orebody width and poor ground conditions.

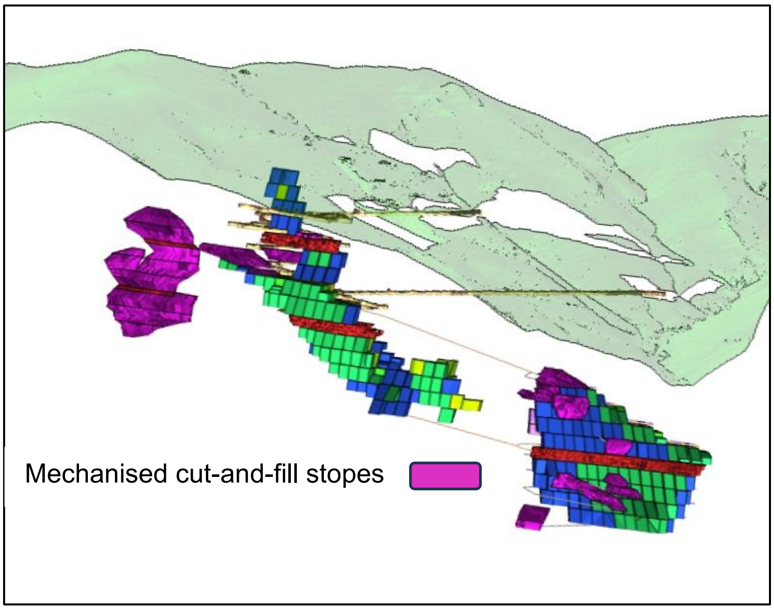


Figure 16-12: Cut and Fill Stope Locations (Source: SRK)

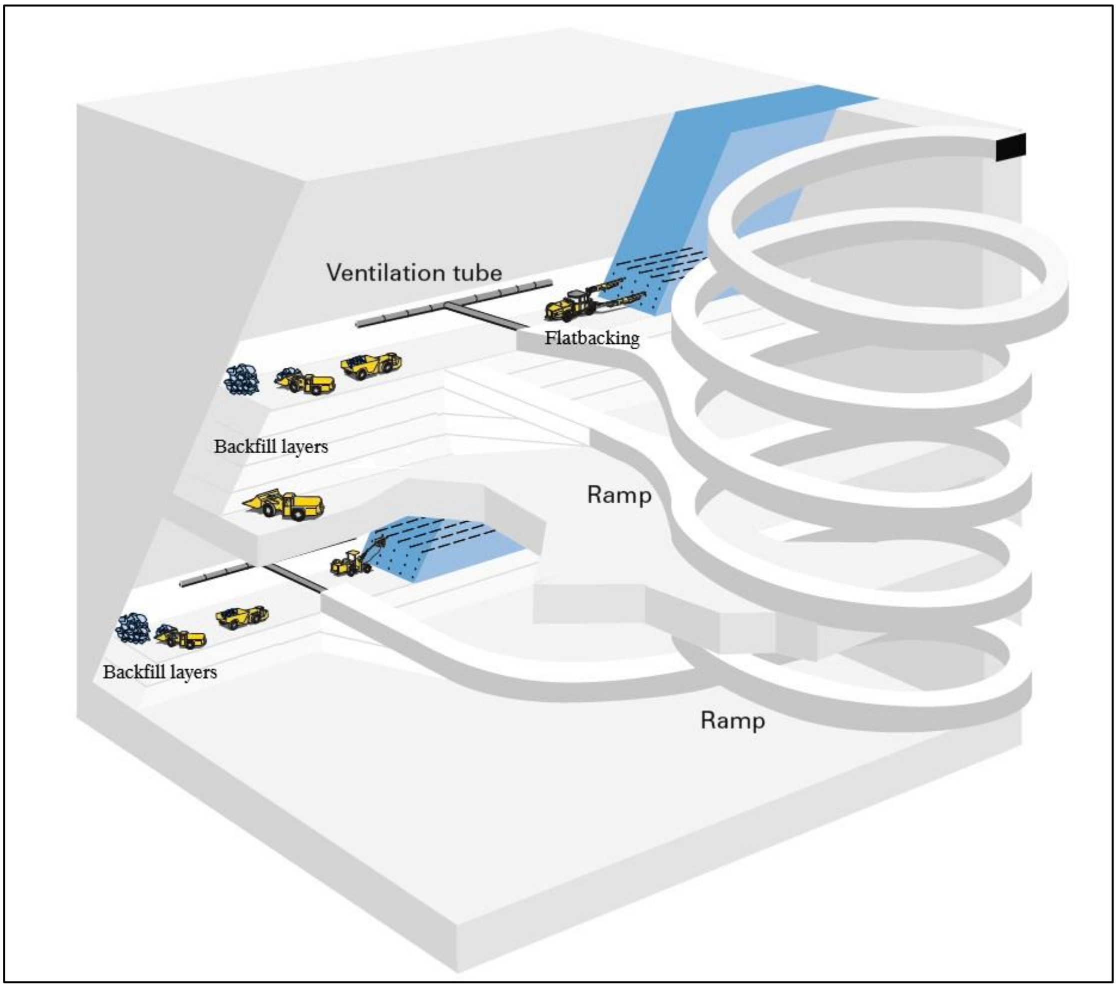


Figure 16-13: Rupice Mechanised Cut and Fill Stoping Layout (Source: Atlas Copco)

16.5 Strategic Options Assessment

16.5.1 Introduction

DPM varied the mining strategy from previous plans to increase the selectivity of mining by reducing the sublevel spacing from 25 to 20 m, and introducing MCAF to extract narrow and flat dipping orebodies. The benefits include:

- Reducing planned waste in stope designs through improved selectivity
- Improving stability to reduce unplanned dilution and ore losses
- Maximizing the use of development waste as stope backfill, minimising haulage costs, and reducing waste storage requirements on surface
- Minimising processing costs by reducing the dilution in the ore stream
- Minimising tailings production and need for storage

16.5.2 Conclusions and Results

DPM's mine plan produces a smaller mining inventory at an increased grade (from 1 April 2025, 9.5 Mt @ 230 g/t Ag compared to the 31 December 2024 ADT Mineral Reserve of 12.3 Mt @ 192 g/t Ag) indicating that DPM's strategic initiatives may be successful.

Reducing the intensity of use of surface facilities by generating less waste products and maximising return to underground creates an opportunity to use free capacity in support of opportunities to increase LoM inventories.

16.6 Backfill

16.6.1 Backfill Strategy

DPM's mine plan strategy for backfilling underground replicates industry practice after the pastefill plant is commissioned in January 2026. The strategy follows that developed for the DFS and is typical for this type of operation:

- All stopes developed on a sill level have high strength fill placed in their lower half to ensure stability for subsequent URSP pillar recovery. Primary stopes are topped up with strong fill to control the risk of dilution when adjacent secondary stopes are extracted. Secondary stopes are topped up with low strength fill unless wall exposures are anticipated.
- Remaining Primary LHOS stopes are filled with strong pastefill to ensure the stability of fill walls exposed by secondary stopes. Secondary LHOS stopes are filled with low strength paste, cemented rockfill or uncemented rockfill, depending on the final configuration of stopes.
- MCAF stopes are filled either with development waste or pastefill with a strength able to support the mining equipment necessary to undertake the production mining activities.

16.6.2 Material Qualities

The backfill technical plan was prepared by consultants Paterson & Cooke (UK) Ltd ("P&C") as an Interim Feasibility Study Report as part of the 2021 Definitive Feasibility Study. The fundamentals of the P&C plan were adopted for the DPM mine plan.

P&C evaluated two types of backfill for use at Rupice, Cemented Aggregate Fill ("CAF") and Paste Aggregate Fill ("PAF"), with included solids derived from:

- development waste, crushed to -75 mm (CAF) or -12 mm (PAF)
- process plant tailings, filtered

ADT concluded from P&C's evaluation that the required backfill strengths are nominally 2 MPa for primary TLHOS stopes, 1 MPa for secondary TLHOS stopes and 1 MPa for all LLHOS stopes. P&C notes that a floor suitable for working mobile equipment, such as for a MCAF application, requires a strength of 750 kPa, which can be achieved with 0.5 to 1.0 m thickness of waste rock, or a capping of high strength paste fill on an underlying filled stope.

For backfilled stopes which are undercut, a strength of 4 MPa was proposed by P&C.

P&C did not conduct comprehensive evaluation of pastefill without aggregate ("PF"), DPM's predominant chosen type for the planned sequence of overhand mining.

16.6.3 Design Parameters

The backfill system designed by P&C is characterised by these design parameters:

- Mixing plant fed from dry stockpiles by front end loader
- RF loaded into mine trucks for transport underground to the destination stopes

- PF pumped by positive displacement pump to boreholes leading to the underground workings and distributed throughout the mine by an engineered pipework network to discharge points on the upper horizon of open stopes, or through the access ramps of HCAF stopes
- A nominal paste fill pumping rate of 50 m^3/hr with maximum and minimum rates of 55 m^3/hr and 45 m^3/hr respectively to maintain continuity of flow

16.6.4 Testwork

P&C conducted paste fill testwork to determine the characteristics of the raw materials and their performance as components of the backfill. Testwork included testing or characterising:

- Raw materials
  - Particle size distribution
  - Particle solids density
  - Mineralogy
  - pH, conductivity, TDS (process water)
  - ISO
  - ISObar testing (cement)
- Backfill
  - Unconfined compressive strength (various binder %, cure time)
  - Yield stress (rheology) (various solids %)

16.6.5 Design Blends

P&C determined preliminary recipes for the two backfill types (Table 16-5) and noted that further testwork and modelling is required to optimise strengths and binder content with regard to stope type, location in stope, and exposure type.

Table 16-5: Nominal Backfill Recipe

Parameter	CAF	PAF
Constituents	Crushed Aggregate Cement Water	Filtered Tailings Crushed Aggregate (<12 mm)
Aggregate % (of solids before cement)	100%	35%
Average Binder % (of total solids)	5.0%	6.6%
Solids Mass Concentration	96%	76%

DPM's plan assumes pastefill achieves the required strength with a 28-day curing time, and the strength for the more demanding locations, such as multiple wall exposures, undercutting and remining through fill is achieved through increasing binder content and addition of aggregate.

16.6.6 System Design and Operation

DPM's plan adopts the design and operating principles and characteristics developed by P&C.

"A backfill plant will be situated at the Rupice site to the south of the main mining portal, adjacent to the ventilation decline exit to the east. The backfill plant will produce both CAF and PAF (not simultaneously) throughout the mine life. The plant has been sized to accommodate a nominal backfill production rate of 50 m3/h with a maximum requirement of 55 m3/h of either CAF or PAF.

CAF will be discharged from the backfill plant and transported underground using haul-trucks as a backhaul from the ore haulage. PAF will be pumped underground using a positive displacement pump.

A backfill reticulation route was established to access the top of all longitudinal and transverse long-hole open stopes displacement pump through an underground reticulation system. The reticulation piping is only for the distribution of PAF, as the CAF must be trucked and tipped in-place. Backfill is reticulated vertically through a series of boreholes, with lateral footwall drive piping running across the strike of the orebody.

Where possible, existing planned development will be used for reticulation, however, on each level, development must be undertaken to establish a borehole "cuddy". A cuddy is an area of development where a borehole breaks through from the level above, and/or the borehole to the level below commences. The cuddies will also contain a pressure transmitter (for remote assessment of the pipeline pressure at the base and top of each borehole), a rupture disc (to protect the pipeline in case of over-pressure), and emergency dump tees (for dumping of the paste to rescue the boreholes in the event of a blockage). A sump will be provided at the base of each borehole, sized to accommodate the quantity of PAF in the line prior to that point. The emergency dump tee can be triggered remotely using explosive charges to dump the PAF into the sump. The rupture disc discharge in each cuddy is also directed to this sump."

DPM extrapolated P&C's DFS design for the mine plan and adopted the principles of P&C's design as the implementation designs.

For DPM, the paste plant will only be producing paste and not cemented aggregate fill. The required strengths will be achieved by adding additional cement. Thus, the basic design of the plant remains unchanged.

The QP notes that P&C's plan has not been re-engineered for DPM's plan so the estimated operating and capital costs have reduced confidence, compared to the +/- asserted by P&C.

16.7 Mine Design

16.7.1 Design Process

DPM prepared its mine design following the industry standard workflow:

- Create a mining model from the resource block model with optional inclusions, which can include metal equivalencies, geometallurgy and processing, revenue factors, costs, loss and dilution, regularisation;

- Create potentially economic stope shapes, manually or using optimisation tools applying cut-off criteria (costs, metal prices, recoveries) and geotechnical design parameters and constraints. DPM used manual methods;
- Prepare development designs to provide access and extraction of the stope shapes;
- Create a plausible schedule of development and stoping incorporating fundamental precedents, dependencies and potential constraints; and
- Verify positive economics of the mine plan and schedule.

16.7.2 Net Smelter Return and Cut-off Value

DPM prepared estimates of Net Smelter Return ("NSR") to recognise the relative contributions to project value from each of the revenue generating products (zinc and lead concentrates). The NSR was calculated using formulas reported in the DFS, updated with modified assumptions for costs, processing performance, prices, treatment charges and penalties.

The NSR was coded into the resource block model and used as the measure of cut-off grade (CoG) to identify economic stope shapes. Where the stope NSR was above the operating costs of extracting the minerals, the stope is considered as ore and included in the inventory of potential Mineral Reserves. Other considerations such as remoteness from access development could lead to exclusion from the final Mineral Reserve.

DPM estimated operating costs and selected NSR CoGs for SLOS and MCAF mining methods are shown in Table 16-6.

Table 16-6: Operating Costs and NSR

Item	Longhole Open Stoping (USD/t milled)	Mechanised Cut and Fill (USD/t milled)
Mining	48.68	67.21
Processing	33.37	33.37
General and Administration	10.39	10.39
Sustaining costs	6.16	6.16
Total	96.6	117.1
NSR CoG	100	120

16.7.3 Stope Optimisation and Design

DPM prepared a mine design comprising stope blocks representing the four selected stoping methods (TLHOS, LLHOS, URSP and MCAF) for extraction of the ore which is suitable for each method. Development layouts were created providing general access and access for production activities.

DPM´s TLHOS and LLHOS stope block designs were prepared manually to closely follow variances in orebody shape, strike and dip, to minimise the inclusion of planned dilution and maximise recovery of economic material.

Extraction of URSP and MCAF stopes is designed to closely honour the geological wireframe shapes with modifying factors used to account for the transformation from mineral resource to reserve.

Main design considerations include:

- Sub-level spacing = 20 m.
- Transverse stopes:
  - Orebody width is >12 m.
  - If orebody width is >20 m, multiple transverse stages (up to 5) are established to keep the span within stable limits between filling campaigns, typically in 20 m increments.
  - FW dip >50° to maximise recovery of blasted ore.
  - HW dip:
    - >68° full stoping up to HW limit contact.
    - <68° the ore wedge adjacent to the HW is mined first to allow a vertical face for the next stope to be established.
  - Cut-off slots 3 m wide are developed across each transverse stope stage by the longhole slot-rise and strip method
- Longitudinal stopes:
  - Stope length limited to 15 m.
  - Stope width >5m and <12 m.
  - FW dip >50° to maximise recovery of blasted ore.
  - HW dip >68° for practical drill and blast of slot.
- MCAF:
  - Recovery of ore at the orebody edges with minimal waste dilution.
  - For orebody dip <68° and width <12 m.
  - Stope width >6m to minimise loss of ore in inaccessible wedges along sidewalls.
- Sill Pillars:
  - 15 m high uphole stoping between LHOS lifts.
  - 5 m high uphole stoping between MCAF lifts.

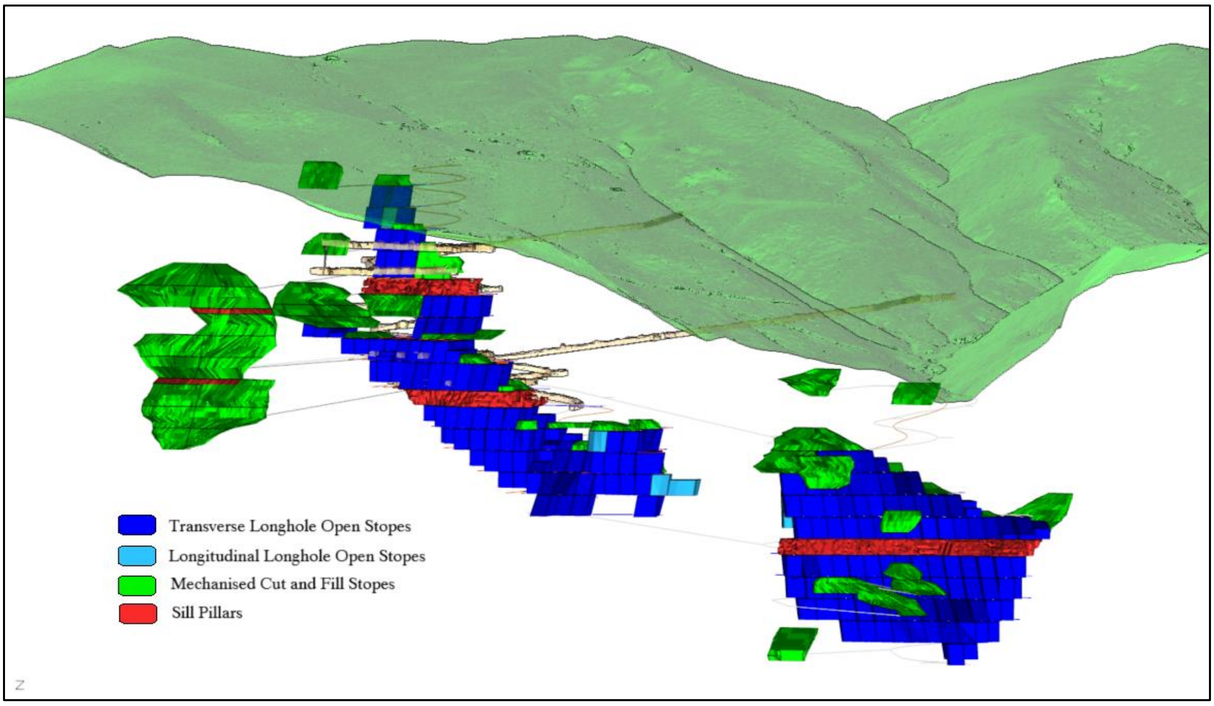


Figure 16-14: Rupice Stope Types

16.7.4 Modifying Factors

Modifying factors to account for ore loss and dilution were determined based on empirical and analogue experience. Conditions accounted for include:

- Dilution
  - Hangingwall contact – 2.0 m
  - Footwall contact – 1.0 m
  - Backfill wall exposure – 0.4 m
  - Undercut backfill stope – 1.0 m
  - Backfill floor – 0.4 m
  - MCAF - =< 10 m wide, 15%, >10 m wide, 10%
  - Uphole stope trough stripping
- Losses
  - Backfill floor – 0.5 m
  - Blind uphole stopes – 0.5 m
  - Sill pillars – 50%
  - MCAF – 5%
  - Downhole stope haunches for stability

The resultant loss and dilution factors by stope type are presented in Table 16-7.

Table 16-7: Loss and Dilution Factors by Stope Type

Stope Type Category	Losses %	Dilution %
HCF (thickness <10m)	5.0	15.0
HCF (thickness >10m)	5.0	10.0
LHOS upholes	8.3	31.4
LHOS longitudinal	5.6	10.0
LHOS trans primary	5.7	7.7
LHOS trans secondary	6.7	13.0
Sill (thickness < 10m)	50.0	39.3
Sill (thickness > 10m)	50.0	24.3
Weighted Average	6.5	12.5

16.7.5 Development Design

The Rupice mine is designed with access through two declines from surface approaching the Rupice and Rupice North-West orebodies from the footwall side. The Upper Decline portal is at the 1070 mRl horizon and the Lower Decline portal is at the 965 mRl horizon. Spiral ramps are developed off the access declines in both inclined and declined directions to provide break-offs at each sublevel interval (20 m) for cross-cuts to the orebodies, and for site infrastructure including stockpile and truck loading bays, pastefill reticulation, ventilation raises, escapeways, dewatering facilities and electrical reticulation.

At each sublevel, a waste crosscut is driven off the ramp to a point standing off from the orebody by 20 m. A footwall drive is driven from that point to the strike extents of the orebody.

Cross-cuts are then driven from the footwall drive across the orebody, for the dominant TLHOS areas. Strike drives are driven on ore to prepare LLHOS blocks. Access ramps are developed to MCAF blocks.

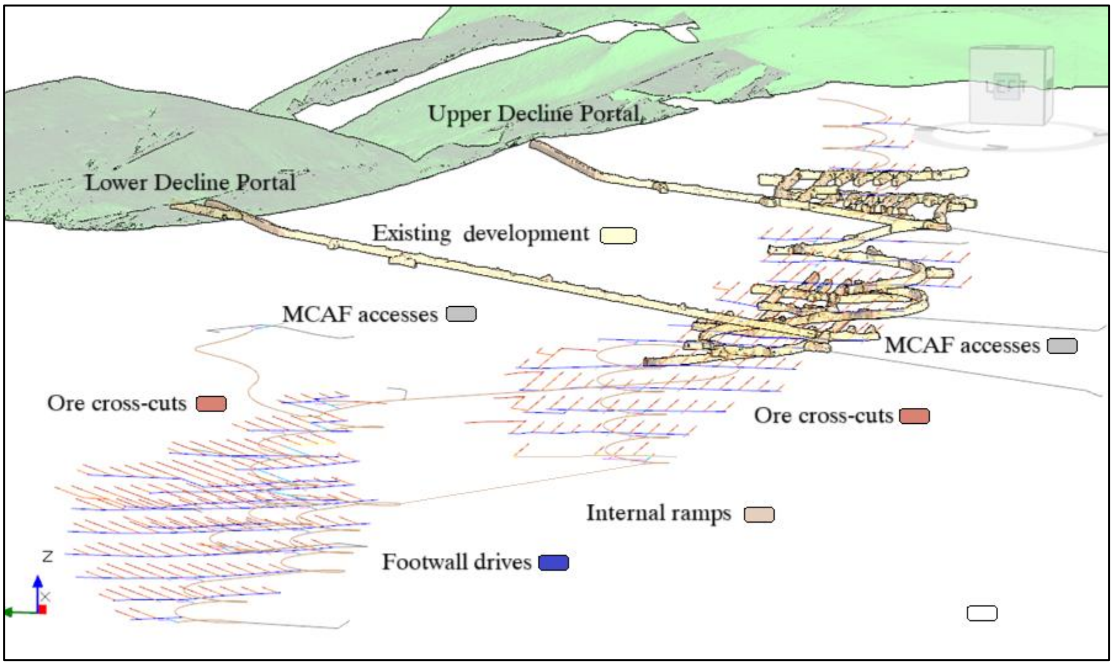


Figure 16-15: Rupice Development Layout

16.7.6 Development Profiles

All lateral development is sized at 5 m W x 5 m H and are refined for different functions during future studies. The current sizing is chosen to be adequate to accommodate all envisaged equipment and functions.

Ventilation raises are planned to be raise-bored at 3 m diameter.

16.7.7 Mine Access

Access to the mine is provided by the two existing declines developed from surface. The declines provide routes for transport of men, materials, and equipment, for haulage of ore and waste, routes for utilities and for intake fresh air. Jointly, they offer two means of egress.

Broken rock is preferentially transported out of the mine via the Upper Decline to the nearby RoM Pad, which provides a more efficient route than that which is possible over the steep surface terrain from the Lower Decline.

16.7.8 Ventilation

Standards

The standard referenced for the mine ventilation design is “Rules on Technical Norms for Underground Exploitation of Metallic and Non-Metallic Mineral Raw Materials” - Foreign Investment Promotion Agency of Bosnia and Herzegovina (FIPA).

Other standards reflecting global best practice are also incorporated.

Strategy

DPM’s mine plan ventilation strategy aims to satisfy four main criteria:

- Provide adequate air to sustain a healthy environment, including temperature, humidity and oxygen content
- Provide adequate diluting air for internal combustion engine fumes, blasting fumes and dust
- Ensure low air velocities in travel ways
- Minimise the requirement for sole purpose development for ventilation

Design

The current airflow system uses the Upper Decline as the primary intake airway and the Lower Decline as the primary exhaust. The Lower Decline is equipped with an exhaust fan which is fitted to a bifurcation of the decline and draws fresh air through the mine from the Upper Decline. The Lower Decline is also used for access and is fitted with airlock doors to manage the potential short-circuit with the bifurcation.

Secondary air circulation is achieved with a series of internal connecting rises and drives with fixed and temporary fans and other ventilation controls used to direct airflows. Ventilation of producing stoping areas is achieved using fan forced ventilation and flexible ducting where flow through ventilation to connected levels is not possible.

DPM's plan includes developing by raiseboring, a new fresh air raise from surface to the upper part of Rupice NW to supply air to this new part of the mine not contemplated in the DFS design. DPM's planned location for the fresh air raise is illustrated in Figure 16-16.

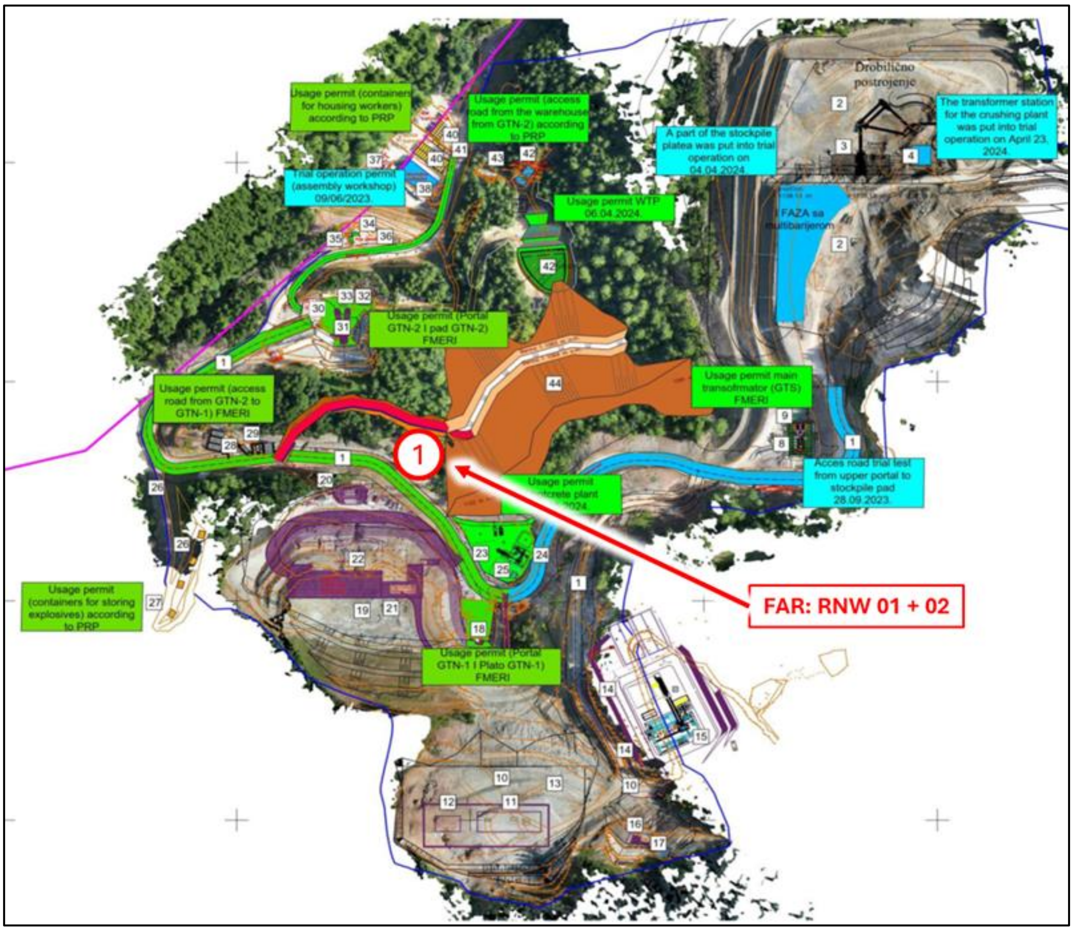


Figure 16-16: Surface location of new Fresh Air Raise from surface (Source: DPM)

16.7.9 Waste Rock Storage

Over DPM's life of mine plan, commencing 1 April 2025, 1,286 kt of development waste is produced and 1,185 kt is consumed by scheduled rock fill. The opening stockpile of waste is 22 kt. The surplus of waste reaches a maximum of 650 kt in December 2029, and 123 kt of waste remains at the end of the mine life.

16.8 Underground Infrastructure

16.8.1 Materials Handling

Blasted rock is mucked from production and development locations with 15t capacity underground Load-Haul-Dump units ("LHD"s). The broken rock is transported and direct loaded into waiting trucks, or dumped in a stockpile bay for subsequent reloading into trucks.

Blasted ore and waste are transported from the mine by 45t capacity articulated low profile haul trucks. Trucks enter and leave the mine via the Upper Decline, which has its portal close to the surface RoM pad. The road from the Lower Decline portal to the RoM pad is sinuous, and with steep gradients, so offers no benefits compared with hauling all rock out of the Upper Decline.

16.8.2 Backfill

Backfill is reticulated underground through an engineered distribution system of steel and HDMI pipework. The reticulation route follows exiting development where possible and utilises vertical or subvertical dill holes where convenient for gravity assisted transfer from one level to another.

At each sublevel requiring pastefill, a dedicated excavation will be developed to accommodate infrastructure necessary for system monitoring and trouble-free operations of the system, including:

- Break-through of drillhole from upper level
- Collar of drillhole to next lower level
- Pressure transmitter for monitoring pipe pressure
- Pipe connections from the upper drillhole to the lower one and take-off to the sublevel
- Emergency rupture disc to protect the pipeline in the event of over-pressure
- Emergency dump t-piece to empty the line to avoid or remove blockages
- Sump capacity for storage of the dumped contents

16.8.3 Electrical

Electrical power is reticulated throughout the mine via armoured cables supported by hangers installed in the backs of main drives, suspended in drillholes where convenient, or supported by wall hangers for temporary working areas.

Power is provided to the mine site at 10 kV and stepped down to 0.4 kV by a transformer located locally.

16.8.4 Ventilation

The underground ventilation circuits use secondary fans, ventilations controls (walls, barricades, regulators) and flexible ducting to direct fresh air to working areas.

16.8.5 Utilities

Utilities (compressed air and service water) are reticulated in steel and HDPE pipes through the mine workings along drives, cross-cuts, declines, and through vertical drillholes and ventilation rises to destination working areas as required.

16.8.6 Dewatering

Dewatering infrastructure comprises a network of main sumps and pump stations to collect and remove service water and natural inflows (refer to Item 16.2.3). Water flows to the sumps under gravity or small electric pumps. It is then pumped from the mine via the declines for treatment and disposal on surface.

16.8.7 Communication

DPM will include coverage through the mine for radio communication and fibre optical cables to support telemetry to monitor and record equipment status, performance, activities and location.

16.9 Life-of-Mine Schedule

16.9.1 Schedule Strategy

DPM has prepared a mine production schedule to deliver the targeted processing rate of 850 ktpa. The schedule incorporates the strategic features:

- Schedule start date 1 January 2025
- A 3-month hiatus in stoping activity from July 2025 to September 2025 inclusive, to allow DPM's Integration Plan to be implemented
- Ramp-up rates
  - 9 months 2025 - 77 kt
  - 2026 – 405 kt
  - 2027 – 850 kt

16.9.2 Constraints

Constraints considered in DPM's schedule include:

- Development rates, including time for ground support installation by jumbo
- Production stoping rates for the different methods and configurations
- Backfilling rates (UCRF and CPF) including stope preparation, fill placement and curing times. One month each is allowed for preparation and placement, and curing times.

16.9.3 Assumptions and Estimates

The strategic assumptions provided in the schedule are:

- Primary stopes backfilled with CPF, secondary stopes filled with CPF or UCRF
- Fundamental precedents and dependencies relating to adjacency to other producing and filled stopes
- Bottom-up sequencing within simultaneous production from discrete blocks separated by sill pillars (RUP – 3 blocks, RNW – 2 blocks, Figure 16-6)
- Stoping sequence from the centre outwards along strike where length allows
- Multiple transverse stopes mined from hangingwall to footwall
- Stoping from the deepest block of RUP from July 2026, the upper block of RNW from February 2027, and the deepest block of RNW in September 2030

16.9.4 Production Schedule

The resulting LoM production schedule from 1 April 2025 is presented in Table 16-8.

Table 16-8: LoM Production Schedule

Item	Unit	Total	P2025*	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039
Ore Tonnage																	
MCAF Ore	kt	**1,543**	-	4	105	119	98	133	38	93	111	147	244	263	148	30	11
LHOS Ore	kt	**7,341**	77	401	745	730	754	717	813	758	690	572	502	326	258	-	-
Sill	kt	**576**	-	-	-	-	-	-	-	-	51	132	105	13	56	155	63
Total	kt	**9,459**	77	405	850	848	846	850	846	850	850	850	850	617	462	185	74
Ore Grade																	
Ag	g/t	**228**	271	230	238	247	254	263	281	244	235	177	182	187	169	201	207
Au	g/t	**1.7**	3.2	2.2	2.0	2.0	2.1	1.9	2.1	1.9	1.5	1.1	1.3	1.2	1.1	1.2	1.2
Zn	%	**6.8**	7.3	7.2	6.8	6.8	6.2	7.3	8.1	7.7	6.5	5.9	6.3	6.3	6.7	6.1	6.4
Pb	%	**4.3**	4.4	4.1	4.1	4.4	3.8	4.6	5.3	5.1	4.7	3.7	4.1	4.0	4.1	3.9	4.1
Cu	%	**0.6**	0.6	0.6	0.5	0.6	0.5	0.6	0.8	0.7	0.7	0.4	0.5	0.4	0.4	0.4	0.4
Sb	%	**0.2**	0.1	0.2	0.3	0.2	0.3	0.2	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1
Hg	ppm	**153**	155	128	137	168	164	170	180	153	135	150	147	138	133	169	173
As	%	**0.1**	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0
S	%	**11.9**	11.9	11.0	11.3	11.6	10.7	11.9	12.8	11.6	11.5	12.6	13.0	12.2	12.6	12.0	12.4
Ore Tonnage																	
Stoping	kt	**8,434**	72	339	623	698	761	788	752	759	717	782	808	612	462	185	74
Development	kt	**1,026**	4	65	226	149	86	62	94	91	133	68	42	5	-	-	-
Total	kt	**9,459**	77	405	850	848	846	850	846	850	850	850	850	617	462	185	74
Development																	
Ore	km	**11.1**	0.1	0.7	2.5	1.6	0.9	0.7	1.0	1.0	1.4	0.7	0.5	0.1	-	-	-
Waste	km	**19.1**	1.5	2.9	2.9	2.5	3.0	2.4	2.0	1.3	0.8	-	-	-	-	-	-
Total	km	**30.2**	1.5	3.6	5.3	4.1	3.9	3.0	3.0	2.3	2.2	0.7	0.5	0.1	-	-	-
Backfilling																	
Paste	kt	**4,169**	-	196	376	491	413	386	299	420	297	342	367	237	293	52	-
Rock	kt	**1,185**	-	19	67	54	104	189	187	118	145	93	70	83	56	-	-

* P2025: partial year, 9 months starting 1 April.

16.10 Underground Equipment Selection

16.10.1 Equipment Types and Capacity

DPM's plan utilises medium sized mobile equipment to develop, produce from, and backfill the mine. The main equipment selected by DPM is presented in Table 16-9. All equipment uses diesel power for mobility. Development and longhole drills operate with electrical power sourced through umbilical trailing cables connected to distribution boards.

Table 16-9: Mine Equipment Types

Item	Manufacturer	Model	Capacity
Development jumbo	Sandvik	DD421	Twin boom
Longhole drill rig	Sandvik	DL421 / DL432i	38 m depth
LHD loader	Sandvik	LH515i	15 t
Articulated truck	Sandvik	TH545i	45 t
Cable bolter	Sandvik	DS422i	25 m long cables
Shotcrete sprayer	Normet		20 m^3/hr
Transmixer	Normet Utimec	LF600	5.6 m^3

16.10.2 Equipment Fleet

DPM has prepared a schedule of equipment purchases addressing:

- Items transferable from ADT upon commencement of DPM operations
- New purchases
- Purchases required to replace aged fleet

DPM currently has no plans to deploy battery electric or trolley assist mobile equipment.

All purchases after 2028 are to replace aged equipment.

The schedule of purchases is presented in Table 16-10.

Table 16-10: Mine Equipment Purchase Schedule

Mining Equipment	Make & Model	Units Qty		ADT Units Qty	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039
Jumbo, 2 Boom	Sandvik DD421	3	Required	2	2	3	3	3	3	3	3	2	2	1	1	1	1	1	1
			Purchase	-	1	-	-	-	1	1	-	-	-	-	-	-	-	-	-
Jumbo, 2 Boom	Sandvik DD320	1	Required	1	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
			Purchase	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Production Drill	Sandvik DL421	2	Required	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
			Purchase	-	-	-	-	-	2	-	-	-	-	2	-	-	-	-	-
Production Drill	Sandvik DL432i	1	Required	-	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
			Purchase	-	1	-	-	-	-	1	-	-	-	-	1	-	-	-	-
Emulsion Charger	Normet Charmec SF605D	2	Required	-	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
			Purchase	-	2	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Mine Truck, 45 t	Sandvik TH445	3	Required	3	3	3	3	3	3	0	0	0	0	0	0	0	0	0	0
			Purchase	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Mine Truck, 45 t	Sandvik TH545i	6	Required	-	-	3	3	3	3	6	6	6	6	6	6	5	4	2	2
			Purchase	-	3	-	-	-	-	2	1	2	1	-	-	-	-	-	-
LHD	Sandvik LH515i	5	Required	4	4	5	5	5	5	5	5	5	5	5	5	4	3	2	2
			Purchase	-	1	-	-	-	-	2	2	1	-	-	-	-	-	-	-
Cable Bolter	Sandvik DS422i	2	Required	1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
			Purchase	-	1	-	-	-	-	-	1	-	-	-	-	-	-	-	-
Shotcrete Sprayer	Normet	2	Required	1	2	2	2	2	2	2	2	2	2	1	1	1	1	1	1
			Purchase	-	1	1	-	-	-	-	-	1	-	-	-	-	-	-	-
Transmixer	Normet Utimec LF600	3	Required	-	1	2	3	3	3	3	3	3	2	1	1	1	1	1	1
			Purchase	-	1	2	-	-	-	-	-	1	-	-	-	-	-	-	-

16.11 Labour

The QP was not provided with a labour breakdown or schedule for the life of the mine. As the mine is operational, the QP does not deem it to be material. Rupice is currently reliant on a core contingent of highly skilled expatriate staff filling training and supervisory roles.

16.12 QP Comments to Item 16 (other than 16.1 and 16.2)

16.12.1 Mining

Since development commenced, the mine has endured challenging rock conditions which have impacted rates of development, rates of production and ultimately, costs. Subsequent to the March 2025 site visit, the QP concluded that operations had reached a stable state where appropriate methodologies were developed to deal with the challenging conditions, and long term productivities were understood.

The selected mining methods are fit for purpose with the current level of design detail considered by the QP to be at PFS level, particularly with regard to the MCAF accesses and stopes, which comprise 16% of the LoM inventory.

DPM's bottom-up mining sequence and backfilling strategy reduces some risks of the former (DFS) mining strategy. However, the DFS backfill system design and specification were reported by its author to be incomplete or preliminary in some respects, and this low confidence level is exacerbated by the adoption by DPM of a different mining sequence and methods. The technical aspects of the backfill system and design specifications need to be updated and aligned with the new strategy to progress beyond the PFS level of confidence.

The QP reviewed DPM's calculations supporting the NSR cut-off grades, including a high level review of the methodologies used and the results of the NSR estimates depicted in DPM's cashflow model. The QP concluded they are fit for purpose.

DPM's designs for development and stoping are fit for purpose and satisfy the requirements for PFS confidence technical studies. Certain parts of the designs are not adequately detailed (including MCAF accesses and stoping, interactions between MCAF and LHOS operations, dewatering facilities, backfill reticulation, backfilling strategy, primary and secondary ventilation circuits, waste rock storage) to satisfy the FS level of confidence.

DPM has provided a basic ventilation plan to cater for the extensions to depth of 125 m (to 700 m), and laterally by 350 m (to 850 m total length) to accommodate RNW, which was not included in the DFS. This requires detailed re-engineering to progress beyond the PFS level of confidence.

DPM's production schedule indicates a peak surplus of approximately 650 kt of mine waste which requires provisions to be made for temporary storage on surface during the mine life. The end of mine life balance is 123 kt which requires long term storage on surface. At the time of the Technical Report, ADT had submitted a permit application for a waste storage facility for 600 kt.

DPM's plan for pastefill pumping and reticulation is not updated from that upon which the DFS was based. The extended footprint of mining resulting from the inclusion of RNW requires the pastefill plan to be re-engineered to progress beyond the PFS level of confidence.

The QP reviewed DPM's production schedule and observed that the target ore production requires frequent turn-over of the modest sized stopes in the mine plan (average 22 kt each), including actions needed to prepare stopes for filling, and allowing time for the backfill to cure before any adjacent mining. Extraction of the equivalent of more than 3 complete stopes per month will be required to achieve the schedule.

The QP prepared a check schedule to confirm the achievability of the target production rate using Deswik mine planning software, as an alternative to the manual spreadsheet based method used by DPM. DPM's schedule result was confirmed as credible and achievable though the check schedule required an ore stockpile to be available to mitigate some shortages in production which appeared from time to time. The check schedule indicated that the RoM stockpile may be larger than the DPM's current estimate of <100 kt. This is to ensure shortfalls relating to delays for fill curing and development advance do not impact the final schedule result. The QP considers this outcome is not definitive but indicates that more work is required to develop a definitive schedule to progress the mine plan beyond the current PFS level of confidence, particularly if provision for storage of a large ore stockpile on surface is needed.

The QP considers DPM's nominated mine equipment types and sizes to be fit for purpose for the Rupice mine plan. The QP notes that DPM's scheduling methodology does not include scheduling ore development as metres, the equivalent volume was included as stope production. Consequently, the fleet of drill jumbos was deemed to require one additional unit, which was added.

16.12.2 Hydrogeology

The current dewatering design assumes very low groundwater inflows over the life of mine. This assumption is uncertain given that hydrogeological investigations at the mine site to date are limited in coverage compared to the proposed mining extent. Gaps in the hydrogeological understanding also present a risk of sudden inrush due to intersection of karstic features and high storage compartmentalised blocks, with limited controls currently in place e.g. cover drilling. The mine dewatering system is also highly constrained by the water treatment plant capacity. A higher than predicted groundwater inflow rate would result in higher-than-expected dewatering and water treatment costs as well as potential impacts on mining production rates assumed in the Mineral Reserve estimation. In addition to posing a safety risk, a sudden inrush event could materially impact the mining production rates assumed in the Mineral Reserve estimation process.

ITEM 17. RECOVERY METHODS

17.1 Introduction

The overall process flow diagram is illustrated in Figure 17-1 and described in Item 17.2. The feasibility study design is based on treating ore from the Rupice underground mine through a sequential flotation process to produce a silver-lead concentrate and zinc concentrate. The process design is based on testwork conducted by Wardell-Armstrong International, Metso-Outotec, Ausenco’s extensive database of reference projects, and in-house modelling programs.

The key considerations for the selection of the process flowsheet included the variable nature of the orebody in terms of feed grade and comminution characteristics, the use of quality equipment from reputable vendors, and a minimised process plant capital cost without compromising reliability.

A summary of the expected process performance is as follows:

- design mill throughput of 800 ktpa (for a mining rate of 850 ktpa, see QP comment in Item 17.6);
- crushing circuit availability of 65%;
- grinding and flotation plant availability of 91.3%; and
- filtration plant availability of 82.2%.

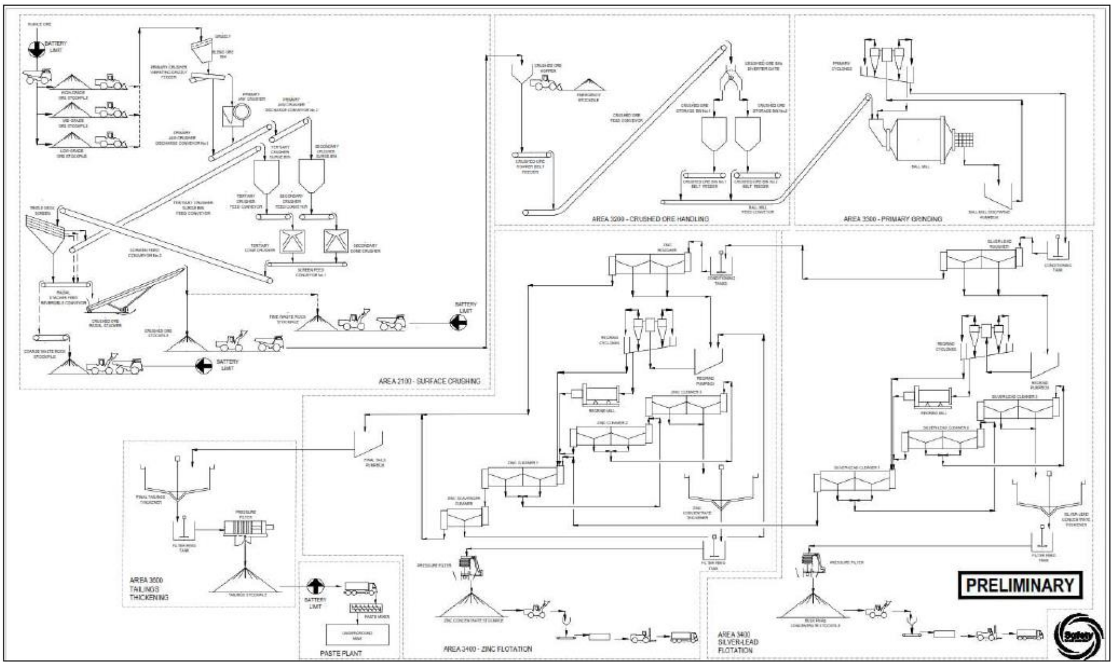


Figure 17-1: Overall Process Flowsheet (Ausenco, 2021)

17.2 Process Flowsheet

17.2.1 Overview

The Rupice site is a greenfield location and consists of three differently graded stockpiles from the underground mine that are reclaimed by means of front-end loaders into a three-stage crushing plant. Waste rock is processed through the same crushing plant to produce the required aggregate materials for the paste backfill operation. Crushed ore and aggregate material are loaded onto trucks and transported to the Vareš Processing Plant and backfill paste plant respectively. The paste backfill plant and associated stockpiles and ancillary facilities are located near the underground portal at the site. A haul road connects the Rupice site to the Vareš Processing Plant site.

The Vareš Processing Plant is located on a brownfield site. Existing infrastructure was either demolished or repurposed for future use. Notably, the historical tailings thickener was re-used as the process water tank in the design.

Ore and waste rock are received from the underground mine at the Rupice site which includes the following process areas:

- RoM stockpile pad;
- three-stage crushing plant;
- ore and waste rock stockpiles;
- paste backfill plant; and
- ancillary surface infrastructure (truck maintenance facilities, sewage treatment, and warehousing).

The process plant includes the following process circuits:

- crushed ore handling and storage;
- ball mill grinding circuit;
- flotation:
  - silver-lead flotation; and
  - zinc flotation.
- concentrate handling by means of thickening, filtration and loading for silver-lead and zinc concentrates;
- tailings handling by means of thickening, filtration and loading;
- reagents handling and storage; and
- plant services.

17.2.2 Rupice Crushing Plant

Run-of-mine (RoM) material is deposited at one of three RoM stockpiles. A front-end loader reclaims ore from the stockpiles in accordance with the blending regime and deposits the ore into the blend ore bin. The ore bin has a capacity of 85 t and is equipped with a 600 mm static grizzly to prevent oversize material from entering the crushing circuit. A vibrating grizzly feeder feeds the material from the bin to the jaw crusher which allows finer material to bypass the crusher.

The primary crusher is a single-toggle jaw type crusher and is designed to reduce the feed size from 80% passing of 427 mm to 150 mm. The crushed material is combined with the undersize material from the grizzly feeder which lowers the 80th percentile of the particle size distribution from 150 mm to 121 mm. The ore then reports to the secondary cone crusher which is operated as an open circuit. The secondary crushing stage further reduces the 80% passing size of 121 mm to 51 mm. The secondary crusher discharge is then conveyed to the triple deck sizing screen. Oversized material on the sizing screen decks reports to the tertiary cone crusher.

The tertiary cone crusher is operated in closed circuit and reduces the feed size from an 80% passing size of 50 mm to 12 mm. The tertiary crushed product is combined with the secondary crusher product prior to reaching the triple deck sizing screen. The undersize of the sizing screen provides the final product of the crushing circuit and produces an 80% passing crushed ore product of 7.12 mm.

The same crushing plant is also used to provide paste aggregate fill (PAF) and cemented aggregate fill (CAF) to the paste backfill plant. When producing PAF, the crushing circuit operates exactly as described previously, but it is fed with waste rock. A diverter gate system directs the undersize of the sizing screen to a dedicated PAF stockpile that provides a 100% passing size of 12 mm.

The crushing plant can also provide 0-12 mm waste rock product and 12-75 mm waste rock product at the same time if required.

When producing CAF, the waste rock crushing operation is truncated to bypass the tertiary crusher closed loop circuit. The undersize of the screen is redirected to a CAF stockpile that provides a 100% passing size of 75 mm.

Crushed ore and waste rock rely on front-end loaders to reclaim the material and load haul trucks for it to be transported to either the processing plant or paste backfill plant respectively.

The feed to the crushers is controlled by adjusting the speed of the vibrating feeders.

17.2.3 Crushed Ore Handling

The crushed ore handling circuit includes a dump hopper, conveyor, coarse ore bins, and ball mill feed conveyor.

Crushed ore passing -12 mm is trucked from the Rupice site to the Vareš processing plant and is end-dumped into a crushed ore loading hopper with a capacity of 45 t. The crushed ore is fed by means of a belt feeder to a belt conveyor at design capacity of 300 t/h. The belt conveyor transports the crushed ore to a diverter gate, where it can be discharged into two coarse ore bins. Each bin provides a live residence time of 23 hours and a corresponding capacity of 2,260 t of ore on a wet basis. Ore is reclaimed from the bins by belt feeders and discharged to the ball mill feed conveyor at design capacity of 110 t/h. The ball mill feed conveyor weightometer is used to control the throughput of ore into the mill.

In the event of a process upset, the material can be stockpiled at a nearby coarse ore storage pad with 12 hours of storage capacity and reclaimed with a front-end loader.

The crushed ore bins provide surge capacity between the crushing plant and the ball mill. Crushed ore is independently filled and discharged from the bins. The feed throughput to the mill is controlled by adjusting the feed of the crushed ore bin belt feeders based on the ball mill feed conveyor weightometer output.

17.2.4 Grinding

The grinding circuit consists of a ball mill and cyclones. The grinding circuit is designed to reduce ore from an 80% passing size of 7.12 mm to 40 μm.

The ball mill is a single pinion overflow mill operating in a closed circuit. The mill has an inside diameter of 4.3 m and an effective grinding length (EGL) of 7.5 m. The mill receives crushed ore and process water at a variable flowrate to achieve the correct pulp density. Lime, zinc sulphate, and sodium metabisulphite (SMBS) are also dosed to the ball mill to condition the feed prior to the flotation circuit. The ball mill discharge passes over a slotted trommel screen with an aperture size of 10 mm x 25 mm. The ball mill is charged with high chrome grinding media at a diameter of 25 to 40 mm by means of the grinding building hoist and ball kibble.

Operators monitor the grinding mills discharge density, cyclone overflow and underflow densities, power draw, cyclone pressure, and other parameters to maintain a product size of 40 μm.

17.2.5 Flotation

The flotation circuit at the Vareš processing plant consists of silver-lead flotation and zinc flotation circuits.

The purpose of the silver-lead flotation stage is to recover a silver-lead concentrate. Copper mineralisation also reports to the silver-lead concentrate. The mill cyclone overflow reports to a horizontal vibrating trash screen to remove any oversize particles or material prior to flotation. The screen undersize then reports to a conditioning tank where collector is added. The resulting slurry then flows by gravity to bulk rougher flotation at a nominal density of 40% w/w and pH 8. The process design takes advantage of the ball mill receiving lime, SMBS and zinc sulphate to condition the slurry pH prior to the dosing of collector and removing the need for a second conditioning tank.

The silver-lead rougher flotation cells are conventional forced air tank cells. The concentrate of the silver-lead rougher flotation tanks reports to the silver-lead regrind surge tank, while the tailings report to the zinc flotation circuit. Frother is dosed into the feed box of the first flotation cell.

The regrind circuit consists of a cyclone cluster and stirred horizontal regrind mill operating in open circuit. Slurry from the surge tank is pumped to the cyclones to densify the feed to the regrind mill. The overflow targets a product size of 10 μm. The cyclone overflow reports to the silver-lead cleaner circuit, while the underflow flows by gravity to the regrind mill. The regrind mill uses ceramic media with a 2 to 3 mm diameter. The mill discharge reports to the silver-lead cleaner circuit.

The silver-lead cleaner circuit consists of three sequential stages of cleaning. The first stage is dosed with collector and frother to promote concentrate recovery. The flotation concentrates flow from the first stage through to the second and third stages, and concentrate from the third stage reports to the silver-lead concentrate thickener. The tailings flow counter-current to the concentrate, and first cleaner tailings report to the zinc cleaner flotation circuit, bypassing the zinc rougher flotation step.

The purpose of the zinc flotation circuit is to recover a zinc concentrate. Tailings from the silver-lead flotation circuit report to conditioning tanks prior to the zinc circuit, where lime, copper sulphate and collector are added. The conditioned slurry is then pumped to the zinc rougher cells. The zinc flotation circuit follows the same arrangement as the silver-lead circuit. The resulting slurry is then pumped to bulk rougher flotation at a nominal density of 40% w/w and pH 9.

The zinc rougher flotation cells are conventional forced air tank cells. The concentrate of the zinc rougher flotation tank reports to the zinc regrind surge tank, while the tailings report to the zinc rougher scavenger cells. The scavenger concentrate also reports to the zinc regrind surge tank, while the tailings report to the final tailings thickener. Frother is dosed into the feed box of the first flotation cell of each bank.

The regrind circuit consists of a cyclone cluster and stirred horizontal regrind mill operating in open circuit. Slurry from the surge tank is pumped to the cyclones to densify the feed to the regrind mill. The overflow targets a product size of 20 μm. The cyclone overflow reports to the zinc cleaner circuit, while the underflow flows by gravity to the regrind mill. The regrind mill uses ceramic media with a 2 to 3 mm diameter. The mill discharge reports to the zinc cleaner circuit.

The zinc cleaner circuit consists of three sequential stages of cleaning. The first stage is dosed with collector and frother to promote concentrate recovery. The flotation concentrates flow from the first stage through to the third, and concentrate from the third stage reports to the zinc concentrate thickener. The tailings flow counter-current to the concentrate, and tailings from the first stage reports to the final tailings thickener.

17.2.6 Concentrate Handling

The concentrate handling circuit consists of thickening and filtration equipment required to dewater the silver-lead and zinc concentrate prior to loadout and shipment.

Each concentrate stream reports to a dedicated high-rate thickener, where flocculant is added to assist in the settling of the solids. The thickener overflows report to the process water thickener, while the underflows report to dedicated filter feed tanks which have a residence time of 12 hours.

The silver-lead and zinc thickener underflows each report to a dedicated concentrate filter at nominally 65% solids. The filters are vertical tower filter presses that discharges filter cake at a target moisture content of 8.1% and 9.4% for the silver-lead and zinc concentrates respectively. The filter discharges to two indoor stockpiles, one for silver-lead concentrate and one for the zinc concentrate, each with a 12-hour storage capacity.

The concentrates are reclaimed from the stockpiles by a front-end loader and loaded into a hopper and conveyor feeding system to fill the shipping containers. The containers are stacked by a forklift outdoors and subsequently loaded onto trucks for shipment. The yard has sufficient space for four days of production of each concentrate.

Thickener performance is controlled to achieve the target underflow densities required for filtration. The filter cycle times are adjusted as necessary to achieve the required filter cake moistures.

17.2.7 Tailings Handling

Tailings from the flotation circuits reports to a tailings thickener, where flocculant is added to promote settling of the solid particles. The overflow reports to the process water thickener, while the underflow reports to a filter feed tank at 65% solids. The filter feed tank has a residence time of 12 hours and feeds a horizontal plate and frame membrane filter press. The filter produces a filtered tailings product at a target moisture content of 9.3% and discharges to a covered stockpile. The tailings are recovered by a front-end loader and transported by haul truck back to the Rupice site for use as backfill. Alternatively, the tailings are deposited at the tailings storage facility.

The thickener performance is controlled to achieve the target underflow densities required for filtration. The filter cycle times are adjusted as necessary to achieve the require filter cake moistures for transport to the Rupice site during underground operation or for trafficability at the TSF.

17.2.8 Reagents Handling and Storage

The reagents and operating consumables used in the process are summarised in Table 17-1 on the basis of an 800 kt/a mill throughput and averaged over the LoM for Rupice ore. Reagent and consumable consumption rates were derived from testwork. The Vertical Pressure filter Air through blow (VPA) and Fixed Filter Plate (FFP) filtration cloth consumption is based on an expected cloth life of 6,000 and 3,000 cycles, respectively.

Table 17-1: Schedule of Process Reagents and Operating Consumables

Item	Consumption (g/t)	Consumption (t/a)
Reagents		
Lime (Quicklime)	605	484
Depressant (SMBS)	1350	1080
Depressant (Zinc Sulphate)	675	540
Activator (Copper Sulphate)	350	280
Collector (Aerophine 3418A)	85	68
Frother (MIBC)	120	96
Collector (SIPX)	175	140
Flocculant (Concentrate)	20	16
Flocculant (Tailings)	40	32
Consumables		
Ball mill media (20 - 45mm)	-	576
Bulk Re-grind mill media (2 - 3mm)	-	0.307
Bulk Re-grind mill media (2 - 3mm)	-	0.126
Filtration cloth, VPA (no. of cloths)	-	14
Filtration cloth, VPA (no. of cloths)	-	600

17.3 Process Design Criteria

The key process design criteria for the mineral processing facilities are listed in Table 17-2, which also summarises the grade and recovery data.

Table 17-2: Process Design Criteria

Criteria	Unit	Value
Annual Throughput (Design)	t/a	800,000
Operating Days per Year	D	365
Operating Availability - Crushing	h/a	5,694
Operating Availability - Grinding and Flotation	h/a	8,000
Operating Availability - Concentrate and Tailings Handling	h/a	7,200
Design Throughput - Crushing	t/h (dry)	290
Design Throughput - Grinding and Flotation	t/h (dry)	100
Design Throughput - Silver-Lead Concentrate Filtration	t/h (dry)	10
Design Throughput - Zinc Concentrate Filtration	t/h (dry)	12
Crushing Feed Size, 100% Passing	mm	600
Crushing Product Size, 80% Passing - Crushed Ore	mm	7.12
Crushing Product Size, 100% Passing - Paste Aggregate Fill	mm	12
Crushing Product Size, 100% Passing - Cemented Aggregate Fill	mm	75
Grinding Product Size, 80% Passing	µm	40
Ball Mill Circulating Load	%	250
Bond Ball Mill Work Index - Design	kWh/t	9.5
Bond Abrasion Index - Design	g	0.168
ROM Head Grade, Lead - Average	%	2.9
ROM Head Grade, Copper - Average	%	0.5
ROM Head Grade, Zinc - Average	%	4.6
ROM Head Grade, Gold - Average	g/t	1.37
ROM Head Grade, Silver - Average	g/t	159
Metal Recovery Method	-	polymetallic sequential flotation
Copper Recovery to Silver-Lead Concentrate	%	81.2
Silver-Lead Concentrate Grade, Copper	% Cu	7.4
Lead Recovery to Silver Lead Concentrate	%	87.4
Silver-Lead Concentrate Grade, Lead	% Pb	47.4
Silver Recovery to Silver-Lead Concentrate	%	75.0
Silver-Lead Concentrate Grade, Silver	g/t	2,266
Zinc Recovery to Zinc Concentrate	%	80.2
Zinc Concentrate Grade	% Zn	57.9

17.4 Reagents, Consumables and Utilities

17.4.1 Reagents and Consumables

Lime

Quicklime is received on site from bulk road tankers and pneumatically transferred to a silo with a seven-day storage capacity. The purpose of lime in the process is as a pH modifier in flotation.

Lime is slaked in a tank as required, nominally four times per day, to create a slurry with a density of 20% w/w solids. The slurry is stored in a tank with a 12 hour residence time and circulated in a ring main for distribution throughout the plant. The ring main flowrate is nominally five times the demand flow rate.

Depressants

Sodium metabisulphite (SMBS) and zinc sulphate heptahydrate are received on site as a dry powder in 25 kg bags. The bags are emptied into tanks and mixed with raw water to a solution concentrations of 20 and 15% w/w respectively. The tanks have a residence time of six hours; reagents are pumped to the required locations by dosing pumps.

Activators

Copper sulphate pentahydrate is received on site as a dry powder in 25 kg bags. The bags are emptied into a mixing tank and mixed with raw water to produce a solution at 15% w/w concentration. The reagent is then dosed to the circuit by pumps as required.

Collectors

Aerophine 3418A is received on site in liquid form in 1.4 tonne intermediate bulk containers (IBC). The totes are unloaded into storage tanks with a 24 hour residence time; the solutions are dosed to the process by pumps as required.

Sodium isopropil xanthate (SIPX) is received on site as a dry pellet in 150 kg steel drums. The solution is mixed with raw water to a solution strength of 10% w/w in a tank with a 24 hour residence time. The solution is dosed to the process by pumps as required.

Frother

Methyl isobutyl carbinol (MIBC) is received on site in liquid form in 1.4 tonne IBC containers and stored in a tank with a 24 hour residence time. The solution is dosed to the process by pumps as required.

Flocculant

Flocculant is received on site as a dry powder in 25 kg bags. The powder is stored in a hopper with a five day residence time, and mixed to a strength of 0.25% w/v. The solution is stored in a tank with a 12 hour residence time and pumped to the process as required.

17.4.2 Water

Process Water

The existing 50 m diameter tailings thickener is used to store process water. The thickener receives water from the concentrate and tailings thickeners, as well as from the site water collection ponds. Process water is distributed to the plant by process water pumps that operate in continuous recirculation with the thickener. Process water passes through a filtration system before being used as wash water for the concentrate and tailings filters.

Raw Water

Raw water is received at the raw water tank, which has a live capacity of 24 hours. Raw water is distributed to the plant by raw water pumps which operate in continuous recirculation with the tank. The design raw water consumption for the facility is 2.5 l/s.

Fire Water

Fire water is sourced directly from the raw water tank. A dedicated pump skid consisting of an electrical pump, jockey pump, and diesel pump supplies water to a fire water reticulation system that services the concentrator. The raw water tank level always maintains a minimum level of water for use by the fire water system.

Potable Water

Potable water is sourced from an existing pipeline connected to the local town supply system and stored in a tank for distribution to the concentrator site.

Gland Seal Water

Gland seal water is sourced from the raw water tank and pumped to various users throughout the concentrator.

Air

Plant air compressors supply air at 750 kPa to various users throughout the concentrator. An air dryer allows instrument air to be provided as required.

The concentrate and tailings filters have dedicated compressors to service the air-drying requirements.

Flotation air blowers provide lower pressure air at 55 kPa to the flotation cells.

17.5 Post Commissioning Improvements

Following commissioning of the plant, ADT committed to adding a further stage of flotation into each of the cleaner circuits, using a Jameson (pneumatic) flotation cell in each case, acting as a first cleaning stage, producing final grade concentrate. As of the time of the QP site visit, the cells had been installed and pumping and piping was being installed.

For a number of reasons, the plant has not yet achieved its design production rate; anecdotal evidence suggests that the plant is operating at no greater than 70% of its design. While a lack of available feed ore has been a significant contributor, the tailings filter is understood to represent an impediment to the plant achieving capacity. While ADT has implemented a modification to add additional plates to the existing filter, DPM is committed to installing a duplicate tailings filter, in order to eliminate this potential bottleneck.

17.6 QP Comments on Item 17

The available historical production data (see Table 6-5) shows that the plant has not achieved its design production rate (approximately 200 kt per quarter). While the monthly reports issued by ADT list the tonnes processed, they do not show operating hours, and so it has not been possible to assess whether the plant has been achieving its design instantaneous capacity when it has been running – a lack of available ore is understood to have resulted in a significant shortfall in operating time for the plant to date.

Regarding the metallurgical performance, the results (both grade and recovery) for Ag are in line with, if not slightly ahead of, the expected performance based on the regression equations developed from the testwork (see Table 13-6). However, the results for Pb and Zn (both grade and recovery) to date have fallen short of the expected performance.

Overall, the plant appears to have been built in accord with the design as described in the DFS report, which itself was soundly based on the testwork. Noting that the tailings filter is understood to be undersized as built, the QP notes that only a very limited amount of testwork was undertaken on thickening and filtration, for both concentrate and tailings (see Item 13.6).

While the design capacity of the plant is 800 ktpa, the QP notes that the mine production rate, and hence plant feed rate, in DPM's LoMP is 850 ktpa. Although the plant – noting that the operation in still in its ramp up phase – has not yet demonstrated its ability to meet its design capacity, it seems reasonable to expect that a plant with a design capacity of 800 ktpa should be capable of processing 850 ktpa.

ITEM 18. PROJECT INFRASTRUCTURE

18.1 Introduction

The Vareš Mine started operations in 2024 and is in the process of ramping up to target production. The following Items provide a summary of the recently constructed infrastructure.

18.2 Site Layout and Access

The overall site plan is illustrated in Figure 18-1, which shows the locations of geography of the Vareš Mine as follows:

- Rupice Site where the mine and associated surface infrastructure is located close to the village of Borovica Gomja;
- The Veovaca Processing Plant, which is located at Tisovci;
- The 25 km access road connecting the mine to the VPP, which is used for transporting of run of mine material to the plant for processing and backhaul in the same trucks of tailings to the backfill plant at Rupice;
- The proposed rail loading area for concentrate.

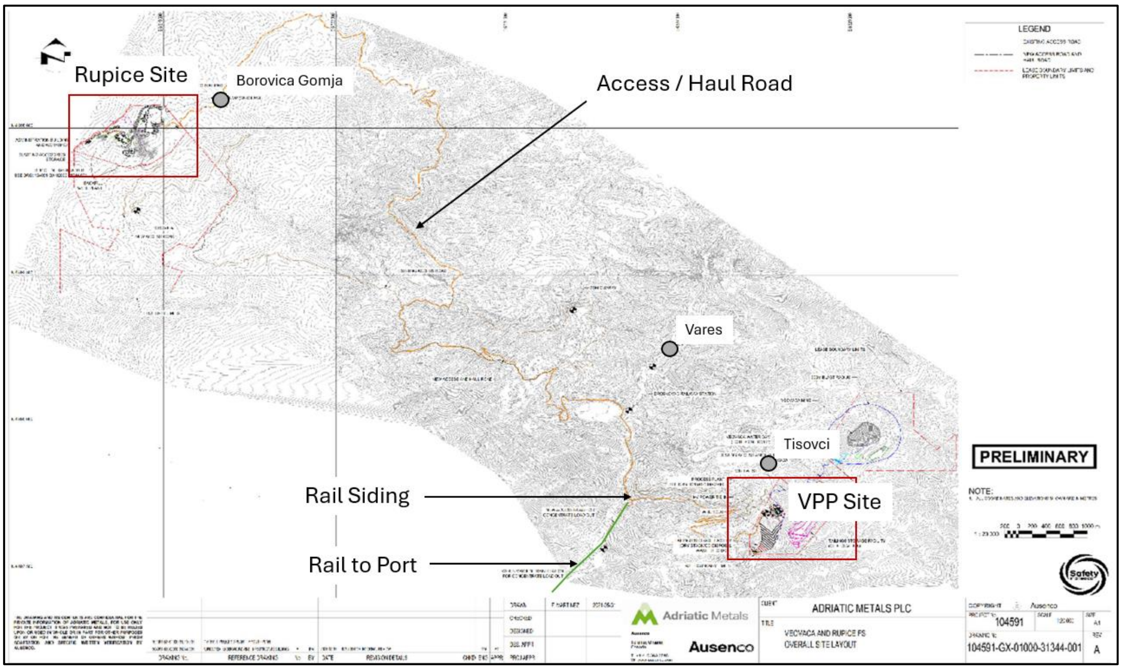


Figure 18-1: Overall site plan for the Vareš Mine

Figure 18-2 presents a more detailed view of the Rupice Mine site with the major installations and buildings and usage status as of October 2024. The Rupice site can be accessed via the main access road which intersects the national road R444 south of Vareš or the R444A near Borovica.

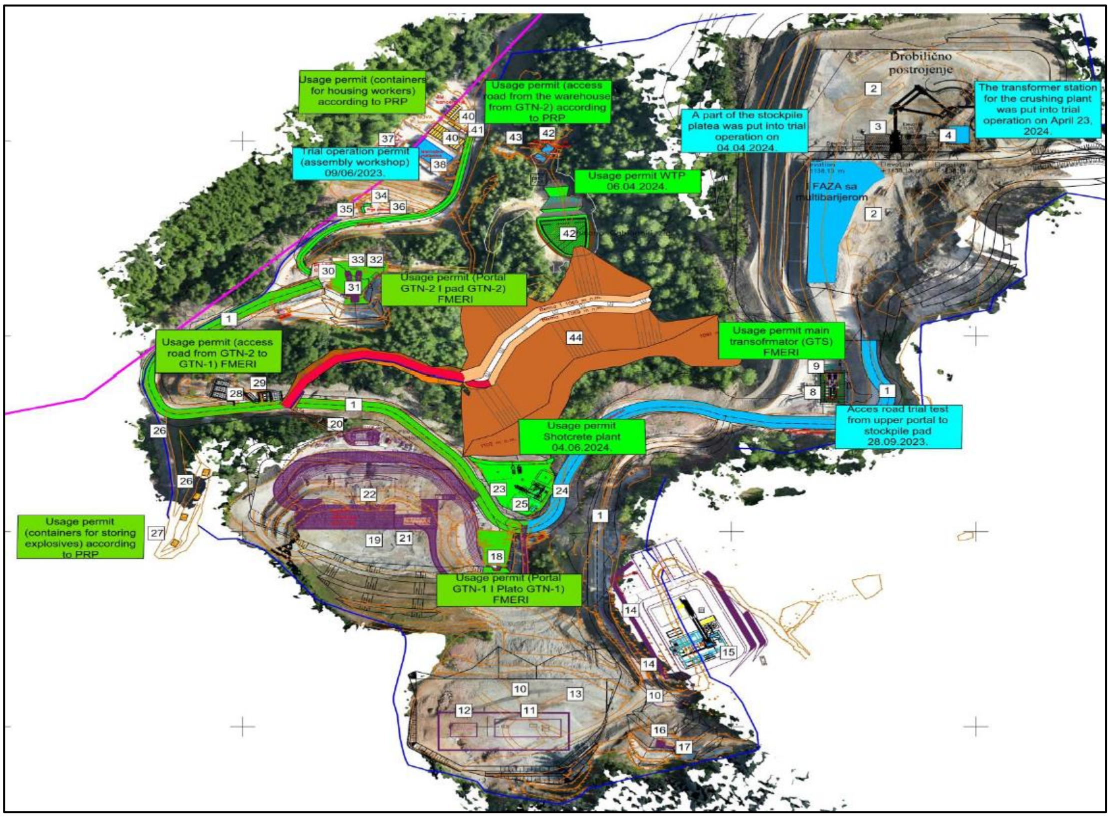


Figure 18-2: A site plan of the Rupice site, October 2024 (sourced from the ADT monthly report October 2024)

Figure 18-3 presents a more detailed view of the VPP with the major installations and buildings and usage status as of October 2024. The VPP is located on the site of a former processing plant at the southern side of the village of Tisovci. It is accessed from the R444 south of Vareš.

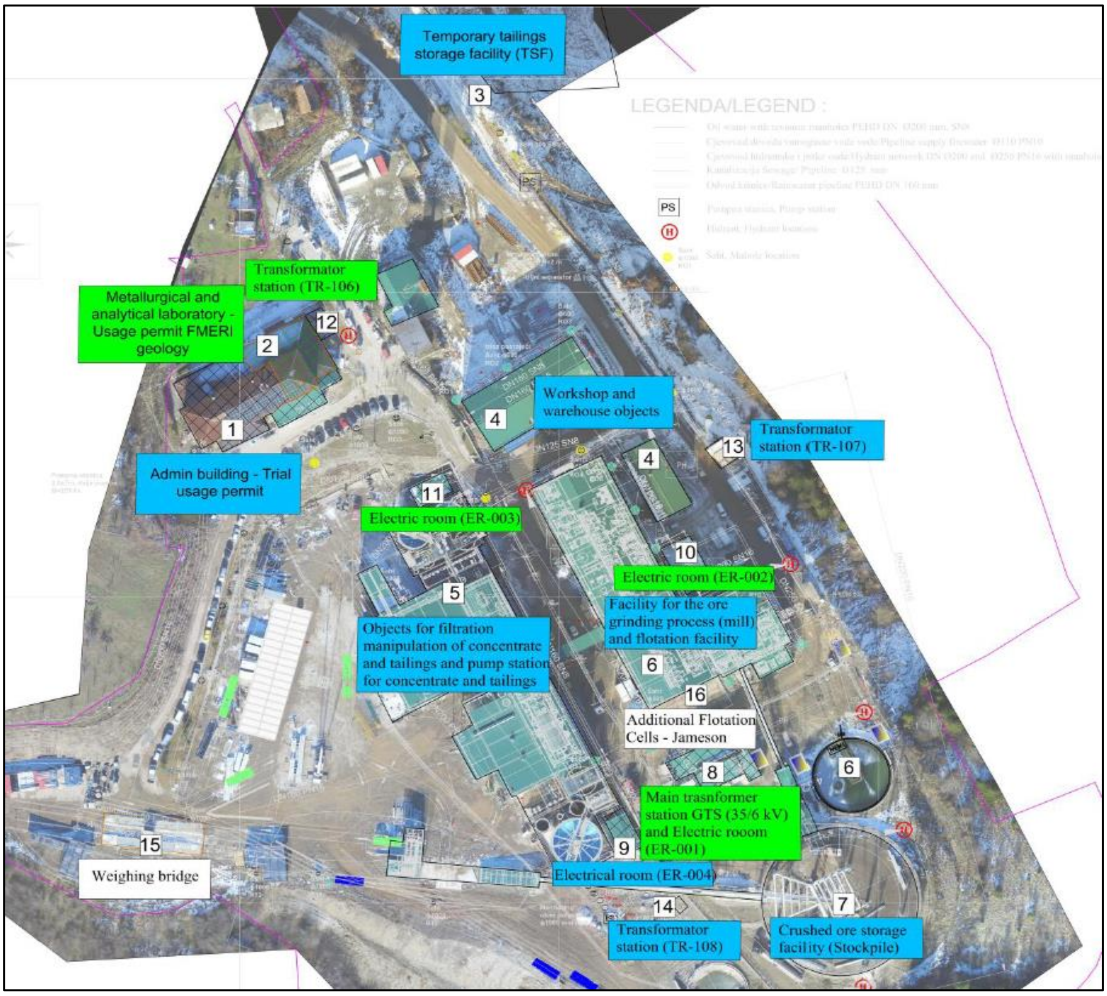


Figure 18-3: A site plan of the VPP showing key installations (sourced from the ADT monthly report October 2024)

18.3 Construction Status

According to the most recent monthly report received (February 2025), the following areas were still under construction:

- TSF Veovaca;
- Backfill plant at Rupice;
- Water Supply (Rupice) and pipeline;
- Emulsion storage (Rupice);
- Emergency Spares still to be purchased;
- Selected work on the access road to Rupice and VPP (EUR 4.5M or which EUR 0.7M is attributed to “LOT 2 Landslide Rehabilitation Project”; and
- Some support vehicles for the Rupice area (ambulance and firefighting truck).

The exact details, current construction status at time of issue of this Technical Report, and criticality of the infrastructure to achieving full production are unconfirmed.

18.4 Tailings Management

18.4.1 Introduction

The filtered tailings resulting from ore processing is either sent to backfill (for stabilisation and restoration of the mine voids) or for storage at surface in a Tailings Storage Facility (TSF). This Technical Report Item discusses the TSF, backfill is covered in Item 16.6.

The project TSFs comprise:

- The Temporary TSF - located directly adjacent to the processing site and has been used to store tailings in the short term whilst the Veovaca TSF is constructed and permitted.
- The Veovaca TSF - the main site of future above-ground tailings storage which is located in the historic Veovaca II Open Pit mine void which is approximately 2km to the north-east of the processing site.
- The Valley TSF – The valley directly below and to the south of the processing site was the original planned location of future above-ground tailings storage. However, owing to permitting and regulatory challenges related to forestry this site was suspended prior to construction and the TSF project was relocated to the historic Veovaca II Open Pit mine void. This site is not discussed further within this Technical Report.

18.4.2 Temporary Tailings Storage Facility

During the site visit of 25 March 2025, an inspection of the Temporary TSF was undertaken with the Managing Director and Chief Executive Officer (CEO) of ADT, together with other colleagues in the Due Diligence team.

The Temporary TSF is located directly adjacent to the processing site and has been used to store tailings in the short term whilst the Veovaca TSF is constructed and permitted. The Temporary TSF design, construction and operational history were not documented in the data provided for review.

Key observations from inspection are summarised in the following bullet points and summary photographs which follow them:

- There is an active slope failure occurring (Figure 18-4). There is credible risk that the failure will continue to develop further and could put safety of people at risk, particularly anyone working on the facility or in the area immediately downstream of it.
- The slope failure development timing, size, extent and downstream impacted area cannot be predicted with any degree of accuracy.
- The Temporary TSF is overlooked by homes, gardens, farms and the public road behind the facility crest (Figure 18-4 and Figure 18-5). The current facility configuration/condition/state is easily observed from these locations.
- In observed conditions either a shallow tailings slump or a translational slide along a critical weak interface in the underlying lining system are both credible.
- Vertical and lateral displacement of the tailings is dragging downwards against the HDPE geomembrane liner resulting in significant tension within it (Figure 18-6). Liner failure is credible, either by exceeding its capacity for tensile strain or by shearing during a translational slide along the critical interface.

- Heavy rainfall as had anecdotally occurred recently (including during the site inspection visit) is a normal/predictable/expected condition for this location. It is likely that the rainfall infiltrated and weakened the tailings, so part of the specific failure mode/mechanism. But an appropriate safe design would either allow for this or ensure that it did not occur such that slope performance and safety are always maintained. Normal/predictable/expected rainfall is therefore not the cause of this ongoing failure, which is instead attributed to deficiencies in site selection, design, operational management and tailings placement.
- The QP notes that ADT / DPM require addressing and understanding the impacts of any further placement of tailings in the Temporary TSF to manage this high risk. The QP would expect ADT / DPM to consider isolating the area to prevent access, and initiating an investigation to substantiate the cause and determine a corrective action plan. The QP has had no further update on the actions taken since the QP's site visit by ADT.

Figure 18-4: Annotated photographs of the Temporary TSF showing location and extent of active slope instability failure (SRK photograph, 25 March 2025)

Figure 18-5: Annotated photographs of the Temporary TSF showing condition at the crest of the facility (SRK photograph, 25 March 2025)

Figure 18-6: Annotated photograph of the Temporary TSF showing side slope HDPE liner under tension (SRK photograph, 25 March 2025)

18.4.3 Veovaca Tailings Storage Facility

Introduction and Design Basis Summary

This summary outlines the design, rationale, and operational considerations for the Tailings Storage Facility (TSF) at Veovaca II Open Pit, associated with the Vareš Project.

The information is primarily based on the Wardell Armstrong LLP (WA) design report titled 'Vareš Silver Project TSF Design 5.1 Mt – Relocation' (November 2024) and supplementary details from Zagrebinspekt d.o.o translated report 'Supplementary Mining Project of Temporary Flotation Tailings Disposal Site at Veovača II' (August 2024), which the WA report supersedes.

The WA 5.1 Mt design report (November 2024) builds on earlier studies, including the Prefeasibility Study (2020), Value Engineering Study (2021), Siting Study (2021), Basis of Design (2021), DFS Design (2021) and DSF TSF Design 3.6 Mt report (2022).

WA was initially appointed by ADT in 2020 to develop the Definitive Feasibility Study (DFS) for the TSF. The DFS concept for the TSF (The Valley TSF) was later revised due to changes in project parameters, discussions with landownership, and ecological and permitting reasons. This ultimately resulted in the Veovaca II Open Pit being proposed as the new location of the TSF.

The EU Mine Waste Directive and Best Available Techniques Reference Document for the Management of Waste from Extractive Industries (MTWR BREF) and the Global Industry Standard on Tailings Management (GISTM) standards were used for the design of the TSF.

The TSF will be constructed within the Veovaca II Open Pit, a former mining site active between 1983 and 1987. Although designed by WA as a permanent facility, the TSF is considered temporary for future exploitation of the underlying Mineral Reserve and potential tailings reprocessing. Nevertheless, because of uncertainties over future activities, WA has designed the TSF as though it were permanent/in-perpetuity.

Tailings deposited within the TSF will be filtered to form a stack of filter cake, with most of the tailings produced by the project used as underground backfill.

DPM project schedule shows the following:

- Total processed ore of 9.5 Mt.
- Dry tailings despatched to pastefill of 4.2 Mt.
- Dry tailings despatched to Veovaca TSF of 3.8 Mt.

During the site walkover carried out by the QP on the 25 and 26 of March 2025, TSF construction works had commenced at the site, and a permit to begin operation in it was expected imminently by site personnel. This includes construction of the starter embankment, downstream contact water pond and associated drainage pipe through the starter embankment, and installation of the basal liner system within the near vicinity of the starter embankment.

The design basis from the 5.1 Mt WA TSF design report is summarised in the following sub-sections.

Tailings Storage Facility Overview

The TSF is designed as a fully lined, dry stack facility. It will be developed in two phases to accommodate up to 5.1 Mt of filtered tailings that are not required for backfill in the underground mine. However, it is important to note that the mine is not expected to produce this volume of tailings during its Life of Mine (LoM).

A summary of the WA design concept is included as follows:

- Fully lined facility with nine maximum 10 m high lifts (but maximum tailings slope height of 50 m above the starter dam.
- Progressive closure with capping layers to prevent water infiltration.
- Contact water managed via drainage systems and a sump at the toe of the facility.
- Non-contact water diverted around the TSF through perimeter drains.
- Culvert beneath the facility for the Mala River diversion stream (to extend through the starter embankment and discharged downstream).
- Underdrainage system below the liner to collect groundwater seepages and eliminate phreatic surface build-up (to feed into the underlying culvert system).
- Capping layer above the tailings prior to closure with an impervious HDPE liner and associated drainage layer and engineered soil, followed by a final topsoil layer at the surface.

Location and Site Characteristics

The TSF is situated within the Veovaca II open pit, located northeast of the processing plant. The site, which was formerly part of the Mala River Valley, features a wide, open bowl-like structure created through the excavation of soil and rock during previous mining activities. This topography provides a suitable foundation for the TSF.

WA provide a summary of the geology, hydrogeology/hydrology, and climatic conditions at the open pit site, which is outlined as follows:

- Geology: Mineralisation occurs in Triassic conglomeratic sediments forming the northern pit face,
- Hydrogeology: Groundwater is ‘shallow’ at the pit base and increases in depth around the perimeter of the pit,
- Hydrology: A central ‘open swale’ channel runs through the centre of the pit to manage surface water (Mala River diversion),
- Climate: Humid continental climate with average annual precipitation of 1,088 mm and 48 snow days per year. Temperature ranges between -20°C (min recorded in winter) to +30°C (max recorded in summer).

WA provide a summary of the pre-TSF-construction condition of the site:

- A flat-bottomed pit with benches and weathered rock near the surface.
- Crushed waste rock forming the working surface for the former mining operation.
- Scattered trees concentrated on slopes and spoil heaps.
- A central swale channel, assumed to divert the Mala River, running through the centre of the pit (stagnant at the time of the WA walkover).

- Public road that follows the crest of the eastern bench and crosses the centre of the northern face (this road is to remain with tailings deposition below the level of this road).
- Settlements located downstream of the TSF.

Figure 18-7 includes a reference photograph of the at Veovača II Open Pit mine void prior to TSF development within it.

Figure 18-7: Site photograph prior to construction activities at the Veovaca II Open Pit site (facing WSW) - Sourced from Wardell Armstrong 'Vareš Silver Project TSF Design 5.1 Mt – Relocation' report (November 2024)

Geological and Geotechnical Conditions

The site is predominantly underlain by fresh limestone, which was exposed during the exploitation of Veovaca II. Groundwater levels around the ridge of the open pit fluctuate by approximately ±3 meters, while fluctuations within the pit itself are minimal. Groundwater levels in the pit are considered shallow, which is an important factor in the design and operation of the TSF.

No TSF-specific ground investigations were conducted for the TSF at the open pit site. Instead, WA used data from 87 historic exploration boreholes drilled between 1952 and 2019.

Limited geotechnical data was available within the above drilling records. Therefore, WA cross-referenced material descriptions from the exploration programme with site investigation data derived from the previously proposed Valley TSF development site (south of the processing plant).

A summary of the geotechnical properties of the sampled bedrock from the previously proposed TSF site is included in Table 18-1. 19 rock samples from the previously proposed TSF site were scheduled for characterisation and strength tests by an accredited in-country laboratory (results summarised in Table 18-1). Laboratory testing results for the superficial soils were disregarded due to the bedrock exposure at the Veovaca II site.

Table 18-1: Summary of laboratory testing and derived parameters from the previously proposed Valley TSF site

Strata	UCS (MPa)	UCS from PLT (MPa)	Density (kg/m^3)	Modulus of Elasticity	Poisson's Ratio
Weathered Limestone	10.9 – 108.5 (52)	38.76 – 93.51 (60)	2662 – 2728 (2695)	19.9 – 45.1 (30.8)	0.4 – 0.5 (0.46)
Fresh Limestone	5.2 – 120.7 (46)	34.38 – 113.60 (66)	2628 – 2779 (2705)	28.9 – 90.6 (59.8)	0.4 – 0.5 (0.45)
Note: Average values presented below value ranges					

Seismic Conditions

WA identified the Operating Base Earthquake (OBE) as having a Peak Ground Acceleration (PGA) of 0.128g and the Maximum Credible Earthquake (MCE) as having a PGA of 0.216g. This information is derived from the site-specific seismic hazard assessment.

Hydrogeological Conditions

WA noted that no hydrogeological specific investigation was undertaken to characterise the groundwater regime at the Veovaca II open Pit site. Instead, a historical data review was carried out to make assumptions regarding the rock properties and characteristics.

WA concluded from the data review that groundwater levels fluctuate by +/-3.0 m within the ridge around the pit, with minor fluctuations within the pit itself. Any surface accumulation of water due to higher groundwater levels is thought to have been dewatered by the central swale that crosses the site.

WA notes that seepage can appear within the southern area of the Veovaca II site which emerge from 'fissure-crack' type features with insignificant yields (1.0 – 3.0 l/min).

A report used in WA's hydrogeological data review indicates that permeability ranges from high (>1x10^{-5} m/s) in fractured rocks (barites, siderites, limestones, sandstones, breccias) to impermeable (<1x10^{-7} m/s) in clayey-sandy sediments.

Hydrological Conditions

Monthly flow monitoring of the Mala River was carried out between 2021 and 2023 at a single location (PPV-3 – downstream of the proposed TSF at the Veovaca II site). The monitoring concluded an average annual flow of 155.5 l/s (Table 18-2).

Table 18-2: WA summary of the hydrological characteristics of the Mala River

Basic Indicators (2021 – 2023)		
Average Annual Flow	Q_{sr} =	155.50 l/s
Maximum Daily Flow	Q_{max} =	841.20 l/s
Minimum Daily Flow	Q_{min} =	0.10 l/s
Specific Discharge (Modulus of discharge-Mo)	Q =	41.24 l/s

Geochemical analysis was also carried out on stream water samples which indicated alkaline, low sulphate conditions with barium and low level, but discernible, concentrations of thallium (typical chemistry for the area).

Tailings Testwork

WA provides a summary of tailings laboratory geochemical and geotechnical testing that was carried out as part of the *'TSF Design 3.6 Mt'* report (2022) and assumed that no further tailings material testing has been completed to date or that the tailings composition has not since changed:

- Geochemistry - Geochemical analysis carried out on the tailings indicated that the material is reactive to atmospheric conditions and prone to generating acid from the leaching of metals and sulphate.
- Geotechnical - Geotechnical analysis carried out on tailings showed filtered tailings moisture contents between 8.7-9.3%, Maximum Dry Density (MDD) of 2.46-2.51 t/m^3, permeability (at 95% MDD) of 4.0 x10^{-8} to 8.1 x10^{-9} m/s, and angle of shearing resistance of 33–36°.
- Interface shear strength testing was also carried out as part of the previous testing programme. A summary is provided in Table 18-3.

Table 18-3: Summary of interface testing

Interface	Angle of Friction (°)	Cohesion (kPa)
Drainage Layer/HDPE Liner	25.0	8.6
	29.8	4.3
Tailings/HDPE Liner	42.9	18.9
	37.2	30.8

Tailings Acid Generation Potential

The tailings have been classified as potentially acid-forming, with the potential to leach metals and sulphides if exposed to atmospheric conditions. To mitigate this risk, sealing the tailings during each construction phase will restrict water ingress, thereby minimizing the potential for acid generation and reducing environmental impacts.

Tailings Transportation

Filtered tailings will be transported to the TSF impoundment area using mine trucks along a newly constructed haul road. The design of this haul road is not being undertaken by WA.

Design Standards and Risk Classification

The Tailings Storage Facility (TSF) has been designed to meet the requirements of a Low-Risk Classification facility, as outlined in The Global Industry Standard on Tailings Management.

The design incorporates sufficient Factors of Safety (FoS) to account for both the assessed operating base earthquake and the maximum credible earthquake scenarios.

Additionally, drainage measures have been implemented to handle storm events during the operational phase and post-closure, ensuring the facility remains stable and secure under varying conditions.

Capacity and Phased Development

The TSF has been designed to store 5.1 Mt of tailings at a dry density of 2 t/m³ (i.e. total TSF storage void is 2.55 Mm³):

- Phase 1 (permitted) comprises three lifts for a total of 1.57 Mt (0.79 Mm³; Figure 18-9).
- Phase 2 (to be permitted) comprises an additional six lifts for an additional total of 3.53 Mt (1.77 Mm³; Figure 18-10).

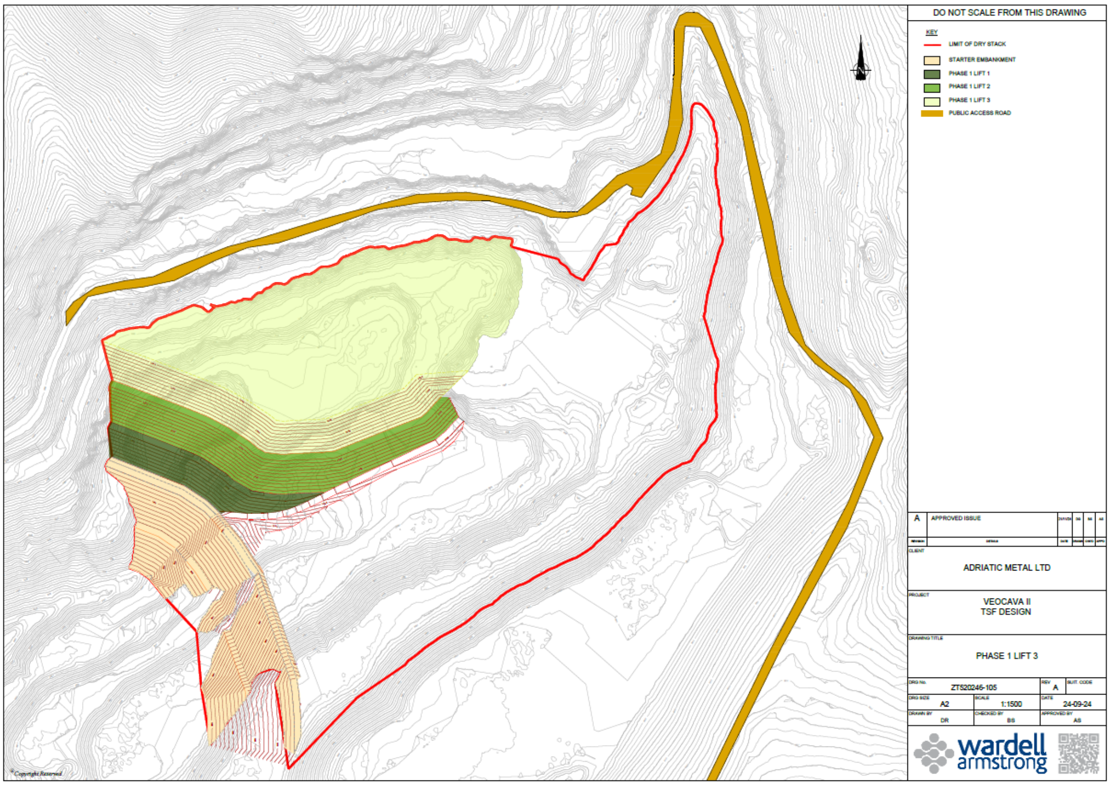


Figure 18-8: Veovaca TSF plan at end of Phase 1 Raise 3 - Sourced from Wardell Armstrong *'Vares Silver Project TSF Design 5.1 Mt – Relocation'* report (November 2024)

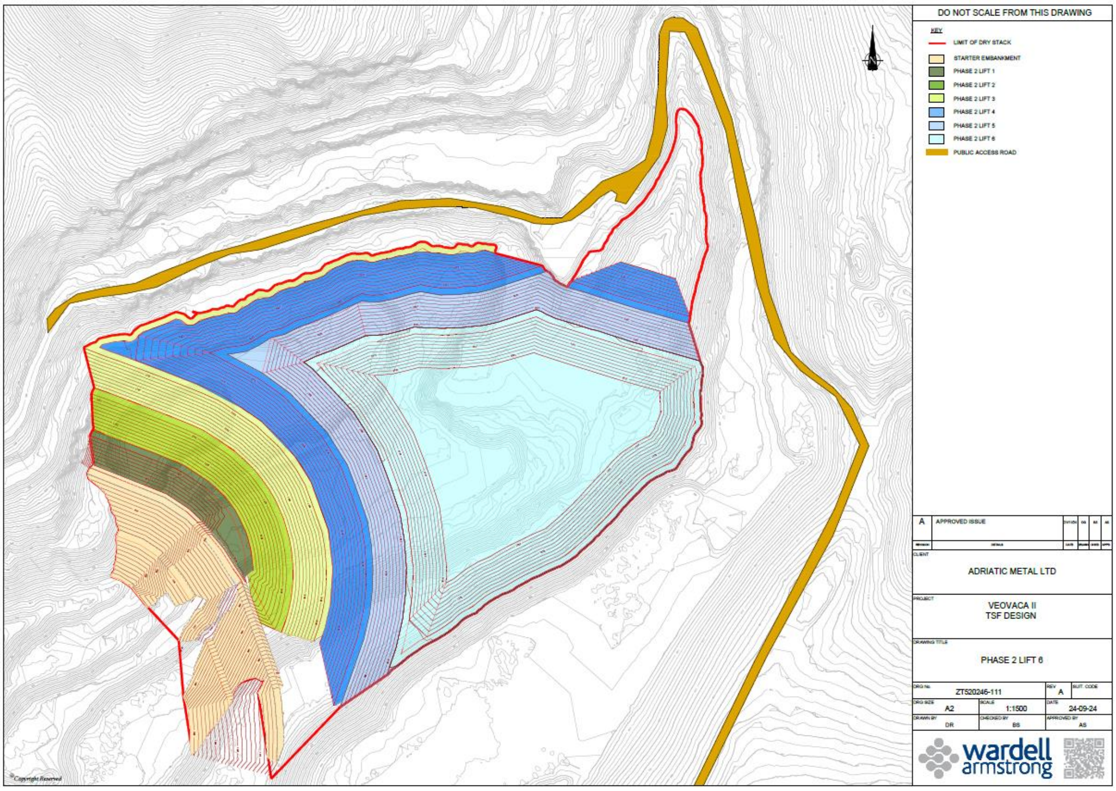


Figure 18-9: Veovaca TSF plan at end of Phase 2 Raise 6 - Sourced from Wardell Armstrong *'Vares Silver Project TSF Design 5.1 Mt – Relocation'* report (November 2024)

Starter Embankment and Base Lining

A 10-meter-high starter embankment will be constructed at the southwest end of the open pit to provide initial confinement for the tailings (Figure 18-11). The base of the storage area will be lined with a geosynthetic underdrainage layer (Secudrain), which will be graded towards a central drainage pipe running beneath the embankment (Figure 18-12 and Figure 18-13). This design ensures effective drainage and minimizes water accumulation beneath the tailings.

Tailings Placement and Final Capping

Tailings will be deposited in 10-meter lifts across the open pit, with an overall slope of 1 vertical (V) to 2.5 horizontal (H). The facility will be capped with a 2 mm HDPE liner, followed by a rock cap made from site-won material graded at a slope of 1 vertical (V) to 3 horizontal (H). A soil cap will then be placed above the rock layer to prevent erosion. Both the rock and soil caps will meet the specified strength requirements. Additionally, an organic-rich soil layer will be applied to the surface to encourage re-vegetation and restore the site's ecological balance.

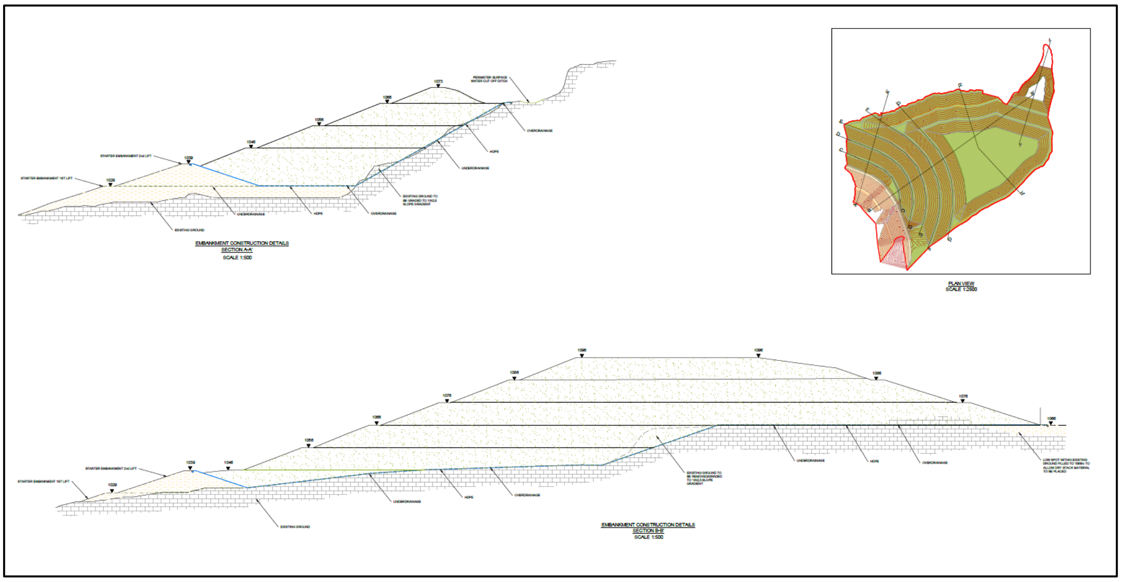


Figure 18-10: Veovaca TSF design plan and cross sections - Sourced from Wardell Armstrong *'Vares Silver Project TSF Design 5.1 Mt – Relocation'* report (November 2024)

Liner System and Water Management

The design of the basal lining system includes a 2.0 mm thick double textured HDPE liner and a Secudrain drainage geotextile (flow rate of >1.0 x10^{-1} m/s - both above and below the HDPE liner).

Above the underdrainage layer, a 2 mm thick HDPE liner is installed to seal the tailings from the underlying subsoil. A geosynthetic drainage layer (Secudrain) is placed over the HDPE liner to capture tailings bleed water effectively. The bleed water is directed towards a central drain and discharged into a contact water sump located downstream of the starter embankment.

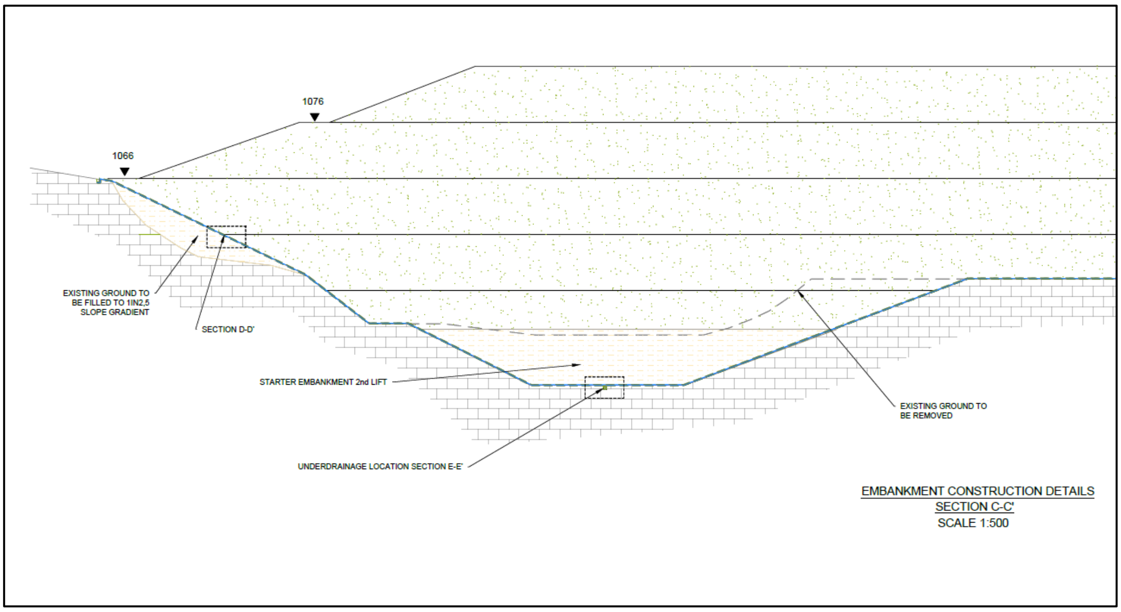


Figure 18-11: Veovaca TSF design side slope subgrade and liner configuration - Sourced from Wardell Armstrong *'Vares Silver Project TSF Design 5.1 Mt – Relocation'* report (November 2024)

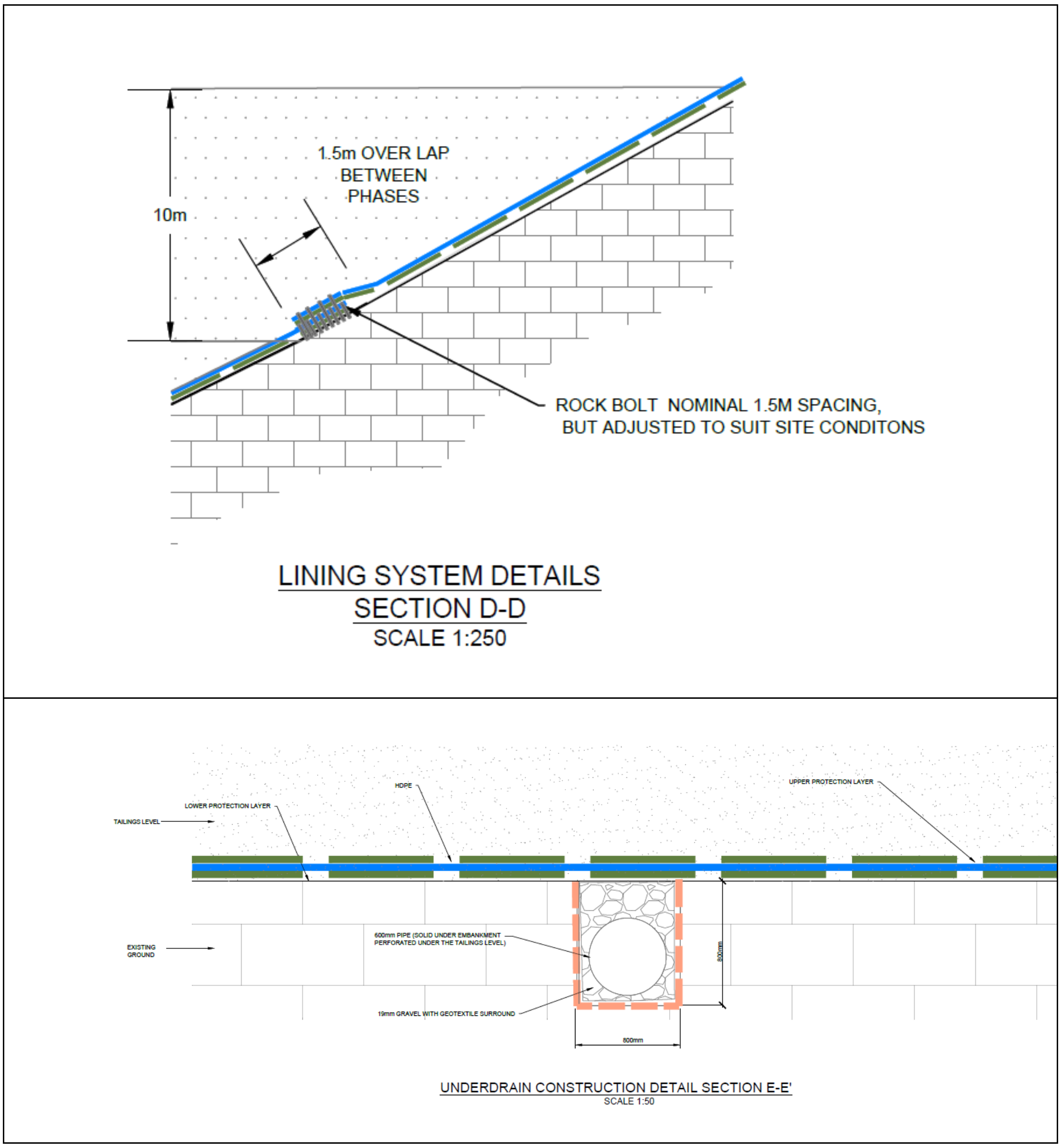


Figure 18-12: Veovaca TSF lining system and underdrain detail - Sourced from Wardell Armstrong *'Vares Silver Project TSF Design 5.1 Mt – Relocation'* report (November 2024)

Contact and Non-Contact Surface Water Management

WA incorporated weather station data obtained from Sarajevo from 2017 – 2020 in the design of the non-contact drainage system.

A 1 in 200-year 24-hour storm event was considered in the design for operational non-contact water systems, while a 1 in 10,000-year 24-hour storm event was used to inform the design of post-closure water management features.

To prevent surface water from entering the impoundment area, perimeter drainage ditches are constructed in phases. These ditches effectively divert water away from the tailings stack. A culvert is installed along the centerline of the facility to collect and channel clean surface water from beneath the stack (Figure 18-14).

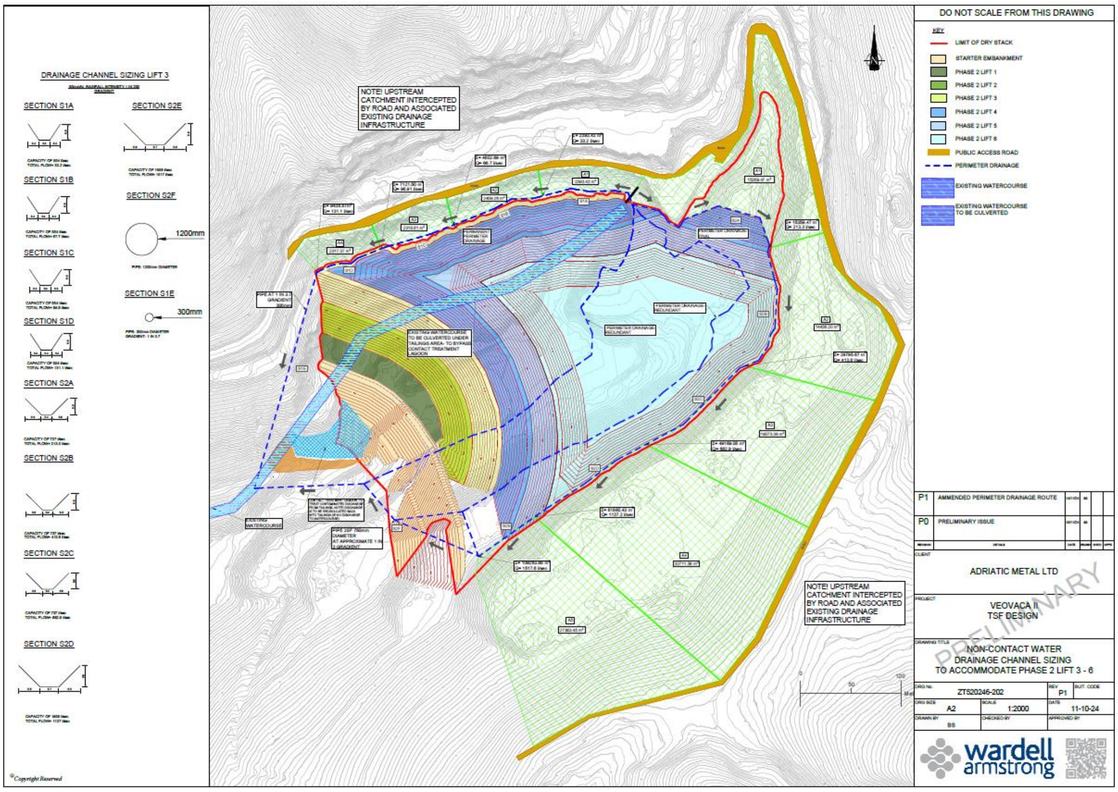


Figure 18-13: **Veovaca TSF non-contact surface water management plan at end of Phase 2 Raise 6 - Sourced from Wardell Armstrong *'Vares Silver Project TSF Design 5.1 Mt – Relocation'* report (November 2024)**

Contact water generated within the impoundment area is managed through a network of sumps and pipes located on the stack. This water is directed to a contact water collection pond situated beyond the toe of the TSF embankment (Figure 18-13 and Figure 18-14). From there, the collected contact water is pumped back to the process plant for recirculation, minimizing water wastage and ensuring efficient resource use.

The runoff analysis carried out by WA indicated that 0.40 m diameter pipes will be sufficient to collect and manage the runoff from the active stacking areas. However, a minimum of 0.60 m diameter is recommended for maintenance requirements.

WA also carried out seepage analysis which indicated that a single 0.25 m diameter pipe is sufficient to carry the bleed water from the over drainage system to discharge into the contact water sump.

Monitoring and Environmental Controls

Comprehensive monitoring systems are implemented for the TSF to ensure environmental and structural integrity.

Surface and groundwater quality are monitored both upstream and downstream of the facility, alongside assessments of dust and noise levels.

Settlement and movement monitoring are also conducted for the embankments to detect any potential structural issues. These measures help maintain compliance with environmental standards and ensure the long-term stability of the TSF.

Stability and Seepage Analysis

WA conducted comprehensive stability and seepage analyses for the proposed Tailings Storage Facility (TSF), focusing on both construction phases (including individual lifts) and the final Life of Mine (LoM) configuration.

Using Finite Element (FE) methods, saturated/unsaturated transient seepage analyses were performed during operation and closure, with results integrated into subsequent slope stability assessments. The slope stability analysis employed 2D Limit Equilibrium (LE) methods to derive Factors of Safety (FoS) for static, extreme rainfall, and pseudo-static conditions, targeting thresholds of >1.5, >1.2, and >1.0, respectively. While the seepage analysis incorporated an impervious HDPE layer and Secudrain drainage layer at subgrade level, these layers were excluded from the slope stability assessment, as they are not intended to provide structural stability. The analyses demonstrated that all FoS values exceeded the required thresholds under various conditions, including seismic events and extreme rainfall scenarios (example output plot included in Figure 18-15).

WA also investigated the sensitivity of tailings properties by varying the friction angle while keeping other parameters constant. This sensitivity analysis was prompted by laboratory testing results, which indicated that the derived friction angle might not be achievable in the field due to differences in compaction methods. Despite these variations, the sensitivity analysis confirmed that all FoS values remained above the required thresholds, ensuring the stability of the TSF under realistic field conditions. These findings provide confidence in the robustness of the TSF design and its ability to withstand operational and environmental challenges.

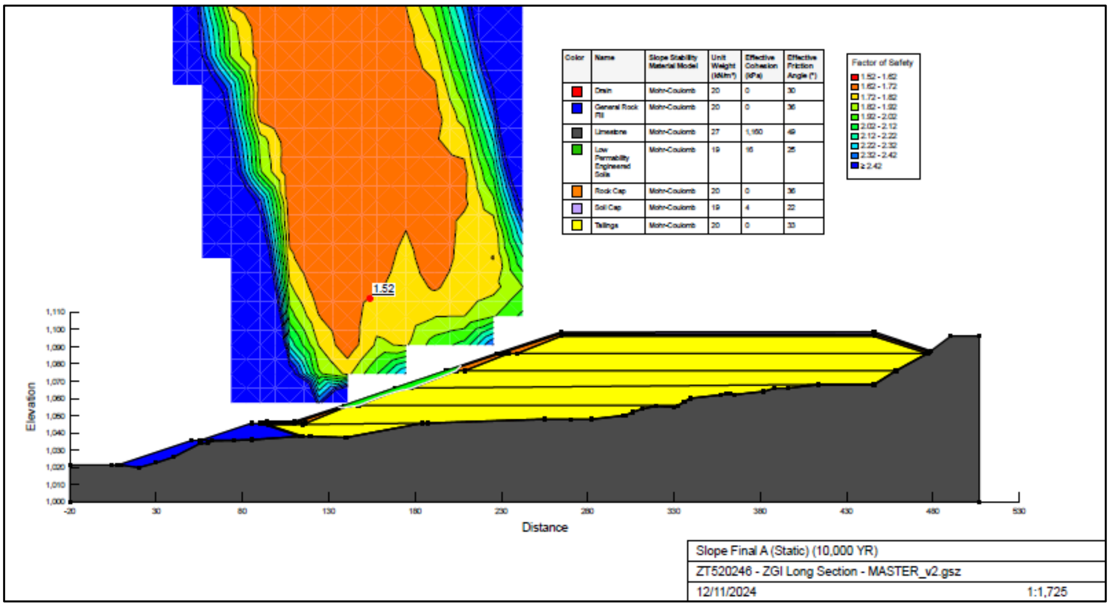


Figure 18-14: Veovaca TSF example limit equilibrium analysis output plot for Phase 2 Raise 6 - Sourced from Wardell Armstrong *'Vares Silver Project TSF Design 5.1 Mt – Relocation'* report (November 2024)

TSF Operation

- Facility is to be operated 24-hours, 7 days a week, with lighting provided by moveable floodlighting,
- Personnel requirements are based on two shifts and include a dozer operator (x2), a grader operator (x2), and a supervisor (x1) (monitoring and inspection personnel excluded from the TSF labour),
- Plant requirements for the TSF include a dozer (x1), a grader (x1), a water bowser (x1) for dust suppression, and an excavator (x1).
- WA assumed that the installation of the liner and geosynthetic drainage layers is undertaken by contractors.

Monitoring

- Piezometers are used both upstream and downstream of the facility to monitor groundwater seepage and water quality (assessed against baseline),
- The water quality of the culvert is monitored via an access chamber located on the platform,
- Settlement monitors are installed on the starter embankment to allow routine settlement monitoring,
- Dust monitoring is also routinely undertaken to confirm the dust suppression measures are operating as required.

TSF Closure and Rehabilitation

- Depending on the monitoring results, 3-5 years of continuous monitoring is carried out post-closure (WA anticipates that flow from the over drainage have ceased within this timeframe),
- Overdrainage discharge pipe is to be sealed following this monitoring period and all contact water infrastructure removed to prevent water accumulation within the sump area,
- Underdrainage and the culvert system remain post-closure.

Recommendations

Recommendations are detailed in Item 26.

18.4.4 QP Comments on Temporary TSF

Based upon the observed condition of the Temporary TSF (Item 18.4.2), the QP recommends that further placement of tailings in the Temporary TSF should stop, the area should be isolated to prevent access, and an investigation should be initiated to substantiate the cause and determine a corrective action plan.

18.4.5 QP Comments on Veovaca TSF

The design of the Veovaca TSF has advanced to the level of a PFS. Whilst the selected location and design are broadly reasonable, and can accommodate the project tailings storage capacity requirements, there are technical risks which will require attention to ensure safety and capacity are both realised. These risks are summarised as follows:

Slope stability failure of the filter cake tailings slope - resulting from saturated/out-of-specification/weak/sensitive/contractive tailings placed in the bowl behind the starter dam:

- There is a topographic bowl in the historic profile of the mine void located directly behind the starter dam (Figure 18-15 and Figure 18-16).
- The bowl; is over 10 m deep; has steeply inclined side slopes; has no access ramp; is lined, but the liner and overlying geocomposite drainage layer are in poor condition (Figure 18-16); includes a sump and drainage pipe through the starter dam to the contact water pond that is considered unlikely suitable to adequately drain the bowl and toe of the tailings slope.
- Owing to the structure, shape and location of the bowl, it is unlikely that tailings placed within will be appropriately compacted to ensure that density, state and strength specifications are met.
- Additionally, it is likely that the tailings in the bowl and above it will not drain efficiently and will remain saturated/partially saturated. The bowl is located in a critical area of the TSF cross section for shear stress.
- Tailings placed within the bowl will form the foundation at the toe of the filter cake tailings slope that will be raised above it.
- Without adequate compaction and drainage, there is risk that the tailings within the bowl will not be adequately compacted resulting in saturated/out-of-specification/weak/sensitive/contractive tailings placed in the bowl behind the starter dam. In turn, this could result in unacceptable slope stability FOS and/or deformations which could result in slope stability failure.
- In an extreme scenario, it could result in flow liquefaction if more generally (including areas outside of the bowl) the filtered tailings are not placed in accordance with required compaction specifications and are saturated/partially saturated.
- This risk is demonstrated by the results of additional limit equilibrium analysis undertaken for purposes of this Technical Report that were undertaken using the design shear strength parameters but with shear strength of the bowl tailings reduced.
- The analysis demonstrates FOS are reduced to less than 1.3 if the tailings in the bowl are modelled with a vertical strength ratio (undrained strength as a proportion of vertical effective stress) of 0.25 (Figure 18-17) and to below unity with an effective strength ratio of 0.1 (Figure 18-18). If an undrained response is triggered in weak/saturated/sensitive tailings behind the starter dam, the slope stability FOS are unacceptable.
- Whilst these results are only presented for indicative purposes, they serve to effectively demonstrate the risk of slope instability if bowl tailings are not effectively compacted and behave more like slurry tailings if an undrained response is triggered (by whatever means).
- From discussion with site personnel during the visit, the QP understands that the bowl will be used for storage of tailings in the short-term during continuation of the commissioning/implementation period. During this time, it is likely that filter performance will be variable and that higher moisture content/out-of-specification tailings will be produced episodically.

– The QP notes that prior to raising the tailings slope, DPM requires undertaking study work to ensure the bowl area is remediated. This may include; 1) development of a temporary tailings stacking area in the base of the mine void; 2) excavation of tailings from the bowl and re-placement of them in the temporary stacking area; 3) placement and compaction of engineered fill in the bowl; 4) re-establishing the basal liner over the filled bowl; 5) engineering of additional drains to facilitate transfer of contact water to the downstream seepage pond; 6) continued further development of the TSF in line with the broad PFS plan.

Figure 18-15: Photograph of the Veovaca TSF showing a general view of the TSF development area including the lined topographic bowl behind the starter dam (SRK photograph, 25 March 2025, looking south)

Figure 18-16: Photograph of the Veovaca TSF showing the lined topographic bowl behind the starter dam. While material is the over-liner drainage geocomposite (SRK photograph, 25 March 2025, looking north)

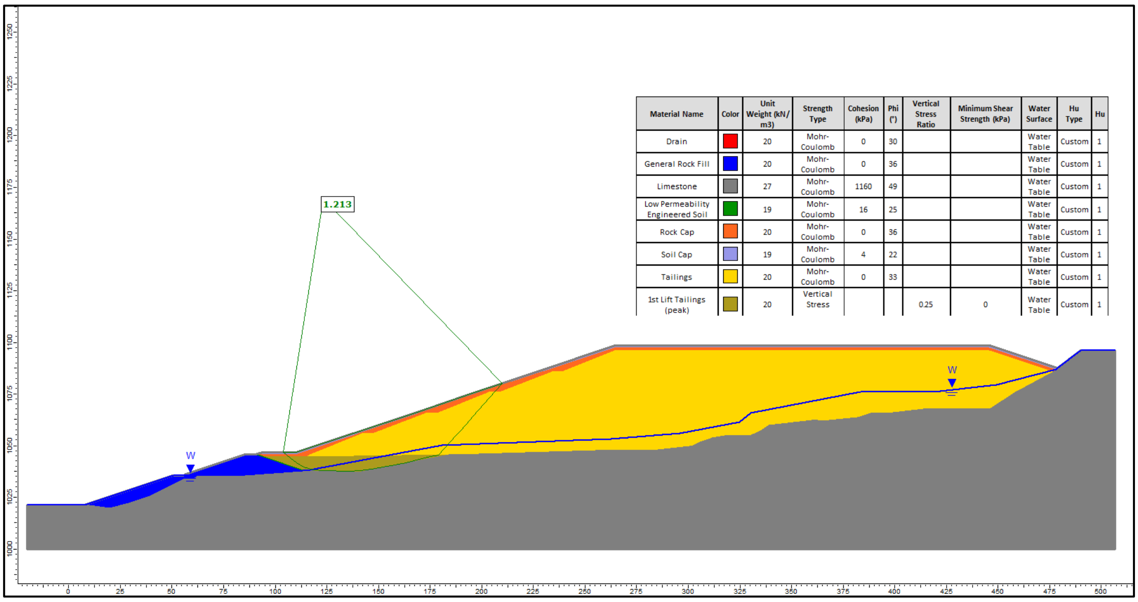


Figure 18-17: Result of indicative limit equilibrium slope stability analysis undertaken by SRK (tailings behind the starter dam modelled with a vertical effective stress ratio of 0.25)

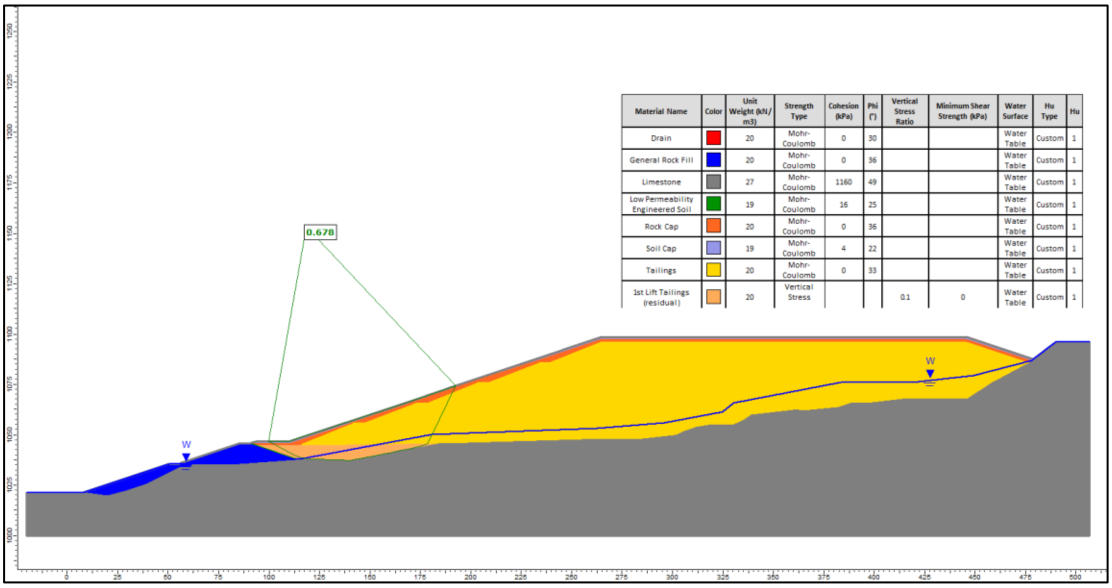


Figure 18-18: Result of indicative limit equilibrium slope stability analysis undertaken by SRK (tailings behind the starter dam modelled with a vertical effective stress ratio of 0.1)

Slope stability failure of the filter cake tailings slope and/or overtopping of the lined starter dam - resulting from inadequate contact water drainage provision in the toe/starter dam area:

- Aligned with the risks associated with the topographic bowl behind the starter dam is the inadequate drainage provision in its base, which is the only route for contact water to exit the TSF and enter the downstream clarification pond (Figure 18-19).
- By observation, it is considered highly unlikely that the small diameter single pipe in the sump at the base of the bowl is sufficient to effectively ensure free drainage under normal and storm flow conditions. Instead, it is likely that the sump is blinded by low permeability tailings above it and the pipe is impaired resulting in saturation of tailings in the bowl and in the tailings placed above it.
- The recommendations made in the previously to place engineered fill and line over the bowl facilitates management of tailings contact water at the planar basal liner/starter dam interface where an upstream open ditch and series of sumps with piped off-takes to the clarification pond could be established.
- By leaving a gap between starter dam upstream slope and the toe of the filtered tailings slope, there is potential access if necessary to clean out both the trench and sumps to ensure continuity of drainage in all circumstances. This contrasts with the existing design where the single sump and pipe are not accessible once tailings are placed in the bowl.
- The QP also recommends that as part of contact water re-design, the design sizing/justification for the downstream contact water management pond should be reappraised and confirmed sufficient for all required normal and storm flows.

Figure 18-19: Photograph showing a general view of the TSF contact water management pond downstream of the starter dam (SRK photograph, 25 March 2025, looking south)

Side slope lining system integrity failure - resulting from tension in the HDPE geomembrane induced by settlement and consolidation of tailings:

- The TSF is to be developed in a historic mine void. The design requires the base and side slopes of the mine void to be cleared and scaled, then lined with a composite lining system including Geosynthetic Clay Liner (GCL) overlain by HDPE geomembrane.
- The side slopes of the mine void comprise a bench and berm profile with steeply inclined faces (Figure 18-20). Effective lining of the existing topographic geometry is a significant challenge requiring careful sub-grade preparation (including placement of fill; clearing; scaling; and some excavation), and specialist lining services (potentially including welding of vertical HDPE seams via roped access).
- During operation of the TSF, there is risk that the steep inclination and complex geometry of the side slopes will limit the effectiveness of tailings compaction in the area adjacent to the liner for fear of damaging the geosynthetics.
- Without effective tailings compaction, some significant consolidation settlement of tailings is expected to occur which could result in down drag against the liner (on the long/steep side slopes) which could in-turn induce significant tension within it.
- Whilst HDPE can accommodate significant tension strain without increase in hydraulic conductivity, there have been cases of tearing and/or anchor-trench failure resulting from down-drag and interface shearing.
- The QP recommends that measures are undertaken to minimise potential for lining system failures to occur.
- These may include; 1) developing specific placement and compaction requirements/specifications for the side slope interface zone; 2) design of yielding anchor trenches with additional liner released progressively if tension is induced; and, 3) use of a sacrificial low shear strength interface above the liner such that shearing occurs down it without inducing tension in the primary liner.

- All of these techniques are successfully adopted in landfill engineering where magnitude of post deposition waste settlement is even higher than can be anticipated for consolidation of filter cake tailings.

Figure 18-20: Photograph of the Veovaca TSF showing a general view of the TSF development area including the steeply inclined mine void side slopes that will require lining in Phase 1 and Phase 2 (SRK photograph, 25 March 2025, looking north)

Storage capacity is insufficient - resulting from out-of-specification tailings placed at lower density and/or necessitating reduction in tailings slope inclination for safety:

- As described in the preceding text, there are a number of risks associated with placement of saturated/out-of-specification/weak/sensitive/contractive tailings. This may result from variability in filter plant performance, from rainfall during transport and placement, and from poor placement/compaction (including that which may occur because of topographical constraints in the old mine void, as previously discussed).
- Whilst the TSF is designed to accommodate 5.1 Mt of filter cake (in the two phases of development) and whilst this exceeds the tailings tonnes in the current LoM, it is reliant upon the design compacted dry density being achieved.
- If the challenges for production and placement highlighted previously mean that this is not possible, and if a reduction in slope inclination is required for adequate safety factors, then there is risk that there will be insufficient capacity in the lined Phase 1 and Phase 2 footprint for LoM tailings production.
- This risk can be effectively mitigated by following the recommendations made for each of the preceding risks and by developing a robust tipping, placement and compaction procedure (sometimes referred to as ‘tipping rules’).
- These tipping rules should define equipment and placement/compaction specifications including QA/QC testing requirements to demonstrate that the require densities are achieved.

- As part of the tipping rules, there may be separate provisions provided for different zones of the tailings waste mass. The outer slope shell tailings may have a tighter specification than the inner non-structural zone to ensure slope stability is demonstrated. This may mean that at certain times of year/seasons the tailings are predominantly placed in the non-structural zone away from the slope shell (rain; snow-melt; winter etc). As previously discussed, there may be different compaction provisions and equipment specified for the zone adjacent to the side slope lining system.

Failure of the non-contact surface water management culvert which is to be developed below the tailings – caused by normal and live loads during TSF operations:

- Failure of culverts below TSFs has been the cause of several known incidents elsewhere at other projects.
- The risk is that the roof of the culvert fails either due to design loads being exceeded, or due to degradation of the culvert condition post installation and during TSF operation. This in-turn results in tailings flow into the culvert and out to the downstream environment.
- If a culvert solution is necessary for this case, then it should be over-engineered with appropriate contingency factors to account for risks and should be designed to allow inspection access for remote camera equipment.

18.5 Water Management

18.5.1 Hydrological Characterisation

The climate and hydrological setting are described in Item 5.3.

Two dedicated meteorological stations have been established; one at the Rupice mine site and another at the processing plant location. These stations continuously monitor temperature, humidity, precipitation, wind direction and speed, and solar radiation (insolation). Baseline surface water flow monitoring has been undertaken since 2018 at five locations along the Borovički and Vrući streams at the Rupice mine site as well as at seven locations along the Mala and Trstionica rivers at the process plant and TSF. Water levels are recorded using automated loggers.

Baseline surface water quality sampling has been undertaken since 2020 at the same locations as those monitored for flow. Samples are analysed for major irons, metals, nutrients, hydrocarbons, and key physiochemical parameters. Results for the Vrući Potok show elevated suspended solids, along with exceedances of several metals, nitrate and total cyanide. The Borovički Stream also shows minor exceedances of some metals.

At the processing plant and TSF area, surface water is sampled at various locations along the Mala River. Results indicate impacts on surface water quality associated with historical mining activities, including exceedances of assessment criteria for various metals as well as nitrate and total cyanide.

18.5.2 Water Balance

A provisional Excel-based site wide water balance model was constructed for the mine site to represent average conditions. The water balance considers off-site water provision and groundwater inflows in the underground mine against mine water requirements but does not incorporate the wider aspects of a site wide water balance such as run-off, ponds and other water storage facilities or evaporation losses.

18.5.3 Water Supply

The make-up water demand required at the Rupice mine site for drilling, dust suppression, backfill and potable and ancillary demands is estimated to be approximately 5.5 L/s, up to a peak of 7.6 L/s.

The mine site sources potable water from the Bukovica spring source, provided by the local water company. A new water supply pipeline was constructed which discharges into a small water holding reservoir up slope from the mine site, with approximately 6 hours storage. Water lines run from the Borovički Stream and Vrući Potak are for use as non-potable water, such as backfill, dust suppression, drilling, wash down, etc.

The average steady state water demand at the Veovača processing site is estimated at 5 L/s for processing make-up water, and 0.3 L/s for potable water. This will be met entirely with supply provision from the local water provider. In the DFS, inflows to the Veovača pit were also planned to be captured for dust suppression, although this is now no longer possible since the TSF location was moved. The processing plant and TSF area are expected to be zero discharge, meaning that ore entrainment and evaporation are the only material water outflows.

18.5.4 Surface Water Management

Surface water management infrastructure defined as part of the DFS includes:

- Catch drains and diversion drains for the capture and management of all run-off from the site footprint; and
- Settlement ponds for the removal of suspended sediment in run-off from site facilities.

Run-off estimation and channel sizing for the mine site has been undertaken using simple empirical assumptions. Storm water management around stockpiles was designed to accommodate a 1 in 25 year, 24-hour storm event of 70 mm, whilst other (permanent) site infrastructure, with the exception of the TSF which is considered separately, was designed to a 1 in 100 year, 24-hour event of 100 mm. Sedimentation ponds have been designed to retain a design runoff volume but are not designed for a specific particle size removal. Average annual rainfall has been used to size storage ponds as well as other water retention infrastructure.

Runoff from the ore stockpiles, waste rock dump (WRD) and paste plant is expected to be poor quality and require treatment to achieve compliance for pH, suspended solids, metals, sulphate, conductivity and ammoniacal nitrogen. It will be treated as "contact water" and diverted to a sediment pond and will be sent, together with mine dewatering water, to a large pond which discharges to a high-density Sludge (HDD) water treatment plant (WTP) with a current maximum capacity of 950 m^3/day. A sludge waste is produced from the WTP which requires offsite disposal by a waste contractor in a specialist facility. The WTP was sized for the expected metals flux from the RoM and WRD over the life of the mine at the time of the DFS. The WTP has been operating near its maximum capacity throughout commissioning and operations and has been observed to be a constraint to dewatering operations at times. From the WTP, water is either discharged downstream into the Vrući Potok or reused as low-grade waters.

Run-off from the rest of the site is treated as "non contact" water and diverted directly to the Vrući Potok with no settlement or treatment.

The more stringent of either the Bosnian wastewater discharge standards or IFC effluent standards has been adopted as the site discharge criteria. At the mine site this is applied at the point of discharge of treated "contact" water back into the Vrući Potok, downstream of the site. The processing plant and TSF sites are designed to be "zero-discharge", specifically this applies to the discharge of "contact" water only. It should be noted that the QP has not reviewed water quality sampling results for effluent downstream of the water treatment plant against adopted water quality criteria.

18.5.5 QP Comments on Surface Water Management

The WTP was sized for the expected metals flux from the RoM and WRD over the life of the mine at the time of the DFS.

The current site wide water balance is limited in its scope and ability to accurately predict future water supply and requirements. This places the mine at increased risk, under certain climatic conditions, of water shortage and/or water surplus that may exceed the current water supply and treatment infrastructure capacity. This could result in the cost assumptions for water supply and/or treatment used in the current reserve estimation being underestimated.

The WTP has been operating near its maximum capacity throughout commissioning and operations and has been observed to be a constraint to dewatering operations at times. The risk of underestimating water treatment costs might be compounded if additional water treatment is required to manage higher than currently predicted groundwater inflows to the underground mine (see Section 16.2.3).

Surface run-off from disturbed areas of the mine site that does not come into contact with the ore stockpiles, waste dumps or paste backfill plant is considered 'non-contact' and is diverted and discharged from the site without treatment. Best-practice is to divert runoff from any disturbed ground associated with the project to a suitably designed sediment pond. The current surface water management approach could lead to poor downstream water quality with regards to suspended solids. Additional costs are likely to be required to increase the capacity and scope of sediment management infrastructure at the mine site.

DPM has indicated that it intends considering all site water as contact water, however this is yet to be developed and incorporated into an update water management plan.

18.6 On-Site Infrastructure (Surface)

18.6.1 Site Security and Access Control

The VPP site, Rupice mine site, and rail loading facility have perimeter demarcation and access control points. The access roads consist of sections of public road and thus are uncontrolled.

18.6.2 Camp and Accommodation

There are limited accommodation facilities on site as many personnel live or reside locally. There is a fully serviced accommodation facility called Veovača Lodge with 38 fully furnished rooms.

18.6.3 Internal Roads

Internal roads are constructed and understood to be of unbound aggregate pavement.

18.6.4 Administration Office and Auxiliary Facilities

A large administrative building at the plant site has been refurbished and is being used as the administrative facility and main country office for the Vareš Mine. Rupice has its own administration building. Weighbridges are installed at both sites. The mine owns and operates a fleet of support vehicles for operations and maintenance. A bus service will facilitate employee transport to work. Communications, data and security systems are operational and were observed on site.

18.6.5 Mine and Process Plant Surface Support Buildings

The mine, crushing plant and VPP are operational, and the QP understands that with the exception of those parts of the mine which are still under construction, support infrastructure, services and utilities, as described in the DFS have been constructed and commissioned; however, a full validation of as built versus planned in the DFS hasn't been undertaken as part of this review.

18.6.6 Fuel Storage

Fuel storage facilities have been constructed at the Rupice and VPP sites, which are operational.

18.6.7 Waste Management Facilities

Sewage

Sewage collected at the site will be treated by a sewage treatment plant located on the west of the mine pad. Waste from bathrooms will be collected, treated, and regularly trucked off site. The sewage treatment plant will be a 14 m (long) by 4 m (wide) single story building part of vendor package.

Solid and Liquid Wastes (non-process)

All waste was disposed of through authorized waste management companies and is reported in the following categories (e.g. Monthly Report April 2024):

- General waste;
- Large/bulky waste;

- Wastewater and mud;
- Used oils and oiled waste;
- Absorbers, filtrated materials, or lubricants;
- Metal waste.

18.7 Power and Electrical

18.7.1 Power Demand

For the Rupice site, peak electrical demand was estimated in the DFS at 6.5 MW with an average load of 5.75 MW and the main consumers being the underground mine, the backfill plant, and the crushing plant. At the VPP, peak demand was estimated to be 8.3 MW with an average load of 7.6 MW. Detailed load-lists and load calculations haven't been supplied for review.

18.7.2 Power Supply Strategy

As part of the construction phase, a new 35kV buried line was constructed from the Vareš Majdan substation to the Rupice site terminating at the 35 kV incomer switchgear at the Rupice 35/10 kV main substation. The substation consists of one 13.3 MVA 35/10 kV transformer.

An existing 35 kV overhead distribution already line ran to the VPP site and as part of the project, the line was upgraded by the utility company (JP Elecktroprivreda BiH) and a new 35/6kV Vareš Processing Plant main substation was constructed. The substation consists of two 13.3 MVA 35/6 kV transformers.

18.7.3 Power Infrastructure and Distribution

Rupice

At the Rupice site, according to the single line diagram ("SLD") presented in the FS, power is distributed at 10kV to the following 10/0.4kV consumer substations:

- Ventilation Fans, Paste Plant, Potable Water Treatment, and Underground Mine;
- Surface Infrastructure;
- Crushing Area;
- Mine Facilities; and
- Explosives Storage.

VPP

According to the FS, from 6 kV switchgear, the voltage will be stepped down to 400 V via step-down transformers feeding the MCCs that provide power to the facilities although larger variable speed drives (VSDs) will have 6 kV input, fed directly from the by main 6 kV switchgear. However, feedback from the site visit suggested the SLD may have been modified during detailed design from that presented in the FS.

18.7.4 Emergency Power

The FS notes emergency power at the VPP to be a single 1500 kW diesel generator and one 200 kW diesel generator on stand-by. The VPP stand-by generators have been sized for essential loads based on power to tank agitators, flotation cells, etc. The SLD for the Rupice site shows two 150kW standby diesel generator at the crushing area ns the Mine Facilities only.

18.7.5 Renewable Energy

ADT recently announced the installation of a rooftop mounted solar plant to provide energy to support infrastructure buildings. This is likely to displace around 25% of consumption from buildings such as the administration block, workshops and warehouse etc.

18.8 Off-Site Infrastructure

18.8.1 Haul Road / RoM Haulage

Construction

A new haul road (24.5 km) has been constructed to transport material from the Rupice Underground Mine to the VPP and dewatered tailings back to the Rupice site for backfill. The haul road is comprised of the following (a route is shown in Figure 18-21):

- 15.5 km of new haul road
- 9.0 km upgrade of existing public road

Haul road construction was split into five construction lots (“LOT”); the QP was not issued with the details of each LOT. The road is mostly un-bound gravel pavement (road width isn’t confirmed) and is essentially complete. The latest monthly report provided (February 2025) indicates construction works are on-going on the second phase of LOT2 and LOT3. Sections of the road are shared public and mine usage. The alignment passes through a number of sections of high relief and challenging terrain resulting in a requirement for cut and fill earthworks and a requirement for edge protection.

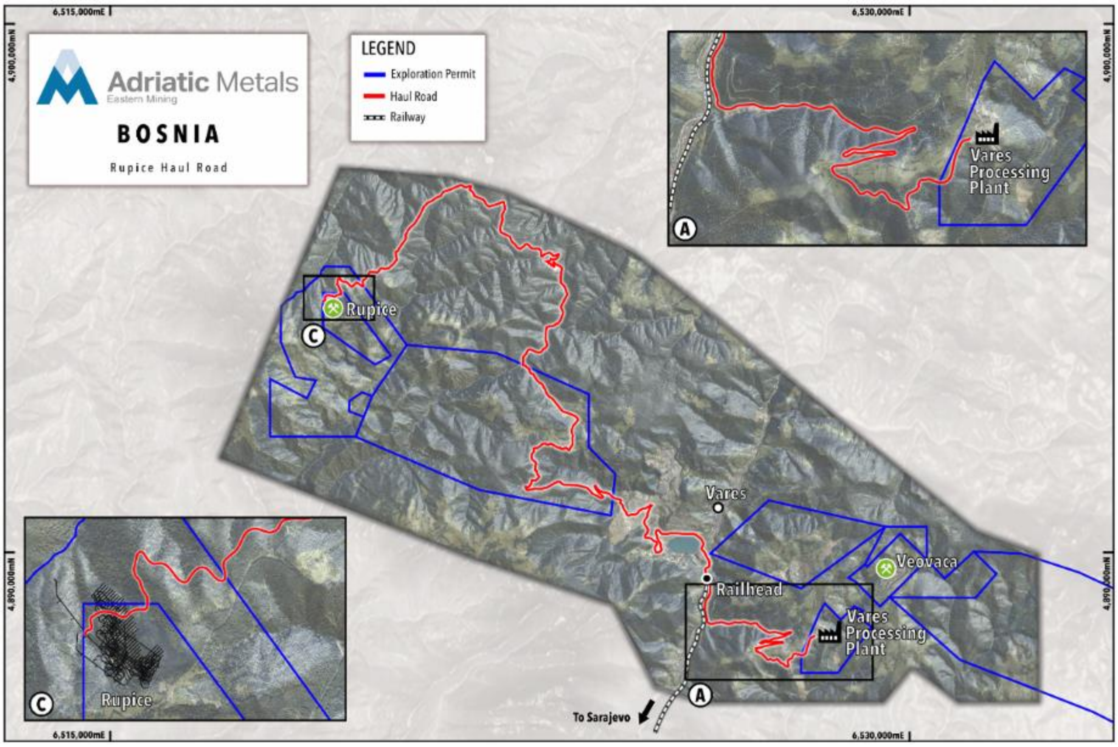


Figure 18-21: Route of the haul and access road (taken from www.adriaticmetals.com)

Haulage Operation

The haulage agreement with Almy Transport is in place and was concluded April 2023. Almy operates the haulage with 15 haul trucks (rigid 8x4 trucks) carrying around 25 t per truck of crushed run of mine from Rupice to the VPP and filtered tailings as a backhaul. The QP understands that all trucks are new units equipped with fatigue system and GPS tracking. At the anticipated production rate, this results in around 200 passes per day (including each way).

Performance

Since completion, the haul road has suffered a series of earthwork slope failures, which has interrupted haulage operations and necessitated emergency maintenance to be undertaken, and future repair works are envisaged.

The current operators have clarified that the budgeted costs only apply to "ongoing maintenance work". Any major roadworks such as landslides, significant repairs, and replacements (e.g., replacing the road base material on LOT 3, asphalt replacement, etc.) are classified as reconstruction or construction costs.

18.8.2 Concentrate Logistics System Overview

Proposed outbound logistics for concentrate products comprises the following system:

- Loading of concentrate to lined containers at the VPP;
- Road haulage of containers from the VPP to Droskovac rail siding (6 km). Containers are loaded to road trucks using a reach stacker;
- Rail siding development (capital project);
- Railing from Droskovac to Podlugovi using diesel locomotive rail haulage (25 km);

- Railing from Podlugovi to Ploce Port (located in Croatia) on mainline rail which is an electrified rail system (214 km);
- Unloading, storage, handling and ship-loading at Ploce Port.
- Sea freight

The DFS baseline is product transported in containers from mine through to customer.

Information below has been obtained from a third-party review report, monthly reports and ADT website.

18.8.3 Rail Load-out

The monthly reports indicate the reach stackers and road trucks have been purchased. Container loading at the VPP is straight forward with material discharging from the concentrate filter presses onto a small bunker stockpile for reclaim by front end loader (FEL) into hoppers conveying material directly into containers. Containers are pre-lined and need to be the reinforced type to accommodate load on the side walls.

From the monthly reports, the QP understands that ADT has refurbished the former site of the Droskovac Railway Station (which was previously used for iron ore and coal operations) including refurbishment of the sidings, erection of security fences and lighting, concrete pads for container storage and site offices, as was planned in the DFS. The external review stated the intention was for a third party to operate the siding. The finalised specification of the hardstanding and loading platform and its capacity for containers needs to be confirmed and this will impact the days of storage at the site.

The Railways Federation Bosnia and Herzegovina (“Railways FBiH”) owns the rail infrastructure in Vareš.

Areas of concern highlighted in the external third party review report are as follows, and the QP has not been able to verify during this review whether ADT has rectified or modified the approach as a result:

- Traffic management around the concentrate shed;
- Specification of container handling equipment and ability to operate in the planned shed and / or redesign of the hoppers;
- Container storage at the site and potential plans to blend; and
- Container management and differentiating of containers.

18.8.4 Rail

The Railways Federation Bosnia and Herzegovina (“Railways FBiH”) owns and operates the railway line. A maximum of 900 wet metric tonnes of concentrate, stored in containers (i.e. 36 containers, each containing 25 t of concentrate), can be transported by rail with each rail movement.

Having been last used in 2020, the 25 km of rail from Droskovac to Podlugovi needed refurbishment; however, there is no detail as to the scope of this work or how it was completed.

The QP understands that recently, rains have disrupted concentrate transport. The QP has not been provided with details or an exact location of the issue; however, anecdotally the QP understands that rains caused instability on a section of the railway line, and this has halted rail transport. The current status is unclear.

From Podlugovi the concentrate is transported on national railways which are electrified. Concerns regarding capacity at peak production rate have been highlighted by a third-party review.

18.8.5 Port

The Ploce Port is where containers are loaded to ocean going vessels for sea freight to smelters in Europe or China. It appears that a full train can be unloaded using the port's mobile equipment and containers stored at the 60,000 TEUs/annum container berth. At peak volumes around 16,528 TEUs are required (loaded and empty) taking utilisation to around 25% of total port capacity.

18.9 QP Comments on Item 18

18.9.1 Tailings Management

See Items 18.4.4 and 18.4.5.

18.9.2 Water Management

See Items 18.5.5.

18.9.3 Site Infrastructure and Logistics

Availability of Data and Review

For site and general project infrastructure information was drawn from three principal sources:

- The DFS report (only) was used to obtain descriptions of proposed infrastructure; however no engineering documentation has been provided and therefore, as-built infrastructure has not been verified against the proposals in the FS and some descriptions may therefore not be reflective of actual constructed infrastructure.
- Selected monthly reports from the construction period and subsequent operations provide an overview of construction progress and some issues subsequently experienced.
- Observations and notes from a site visit undertaken by the QP in Q1 2025. A tailings engineering visited the site; however there was no dedicated site visit for infrastructure engineer.

Haul Road Design Deficiencies and Required Maintenance / Upgrade

The haul road is critical to ensure the delivery of crushed ore to the VPP, the return of tailings for backfill purposes and movement of supplies and personnel to support the operation.

Based on the reports from the site visit and interactions with the operations, it would appear:

- The haul road has suffered from multiple earthwork slope failures and thus far, the operations team has only instigated interim corrective measures.

- Clearly, the level of survey and design work for haul road earthworks and drainage, along with an appreciation of the geotechnical risks and hazards, needed further development prior to construction.
- Unless the road is upgraded, further failures are almost inevitable and until there is a better understanding of the causes and modes of failure, there is a potential for *significant* disruption and additional survey, design review (including a geohazards review) and redesign (e.g. slope stability, slope drainage) is necessary.
- Dundee is looking to upgrade the road, and the required works could be costly, especially if slope stabilisation measures are required. This cost is likely to be concentrated into the first 1-5 years and once a better understanding of the common areas of failure, efforts can be focused.
- The transport of the proposed tonnages looks achievable with the fleet identified in the relevant monthly report.
- Within the stated capital cost budget (as per the February Monthly report) the current operators have EUR 0.615 million reserved for “repair or landslides” and this is in addition to the EUR 2.3 million for finishing the construction scope. In the QP’s opinion, once adequate investigations and studies have been done, the total cost could be substantially more.

Along with the geotechnical / ground stability risk, other risks include:

- Shared public and mine usage increasing the risk collisions with mine traffic;
- Pavement width: A third party review previously noted that the planned width of 5m to be very tight (which the QP agrees with) and advised the road to be widened. It is unclear if the final design incorporated a wider road; and
- Given the terrain and alignment, edge protection must be in place on embankment or sidelong ground; the scope of edge protection installed cannot be confirmed.

Rail, Railway Loading, Port and Concentrate Transport

The QP has not been given access to the documents noted in other external technical review under Item 12.1 of that report.

We don’t have adequate detail as to the status of the rail load-out and rail operations to provide comment.

Clearly, there is the potential for interruption to concentrate transport on the railway line. The mitigation for this would be to truck the containers to a location further downstream during times of disruption; however, this would increase the transport costs (e.g. the rail siding to port transport cost may increase 40-50% if at short notice, trucks were used to transport concentrate to Podlugovi where storage and loading would be required)

Based on a third-party review comments, there is potentially an issue of capacity on the main electrified rail for transport of concentrate at peak production rates, but this needs further analysis to confirm.

Power Supply & Distribution

The QP has not been able to verify that sufficient stand-by power exists for the Rupice site to ensure critical underground infrastructure remains energised during a grid interruption (e.g. water pumps, emergency facilities). Additional stand-by generators may need to be mobilised.

The QP has not been able to verify that the VPP electrical distribution "as-built" is reflective of that proposed in the FS and that major electrical consumers (e.g. ball mill) are fed directly at 6kV. If required, modifications to the electrical distribution may be needed and this is an aspect that has also been noted by DPM.

A concern has been raised regarding the underground electrical distribution design. The design presented in the FS is not reflective of the likely change (expansion) in mine layout or increase in water pumping requirements, thus additional electrical distribution costs may be needed over time.

Rupice Site Earthworks and Drainage

During the site visit, deficiencies in earthwork drainage systems were noted (significant ponding on platforms, poorly formed drainage ditches). While not "critical" to production, this will impact operations on a day-to-day basis and should be rectified. Comments regarding current under-sizing of the water treatment plant are included under Item 18.9.2.

On-going Construction Work

Some construction work is still on-going. The exact details, current construction status at time of issue of this Technical Report, and criticality of the infrastructure to achieving full production isn't confirmed.

ITEM 19. MARKET STUDIES AND CONTRACTS

19.1 Introduction

Prior to the start-up of the mine, ADT engaged the services of Bluequest Resources AG ("BQR") to assist with the marketing of the silver- lead concentrate and zinc concentrate. Off-take agreements were secured for 100% of silver-lead concentrate and over 90% of zinc concentrate production for the first 2-3 years of operations. Concentrate deliveries have already commenced, with further sales agreements recently established. Accordingly, ADT has provided evidence it can produce saleable products in the current market.

19.2 Sales Contracts

19.2.1 Zinc Concentrates

Concentrate sales are in place for over 90% of mine production over the first three years of production, with three customers. The customers are well-known smelting and trading companies. Contracted terms are representative of the general market for long-term concentrate sales with smelters and traders. Based on DPM's understanding of the zinc concentrates market, it is expected that the existing contracts can be extended at the same, or better, terms and conditions.

19.2.2 Silver-lead Concentrates

Concentrate sales are in place for 100% of mine production over the next two years with three customers. The customers are well-known smelting and trading companies. Contract terms are representative of the general market for long-term concentrate sales with smelters and traders. Based on DPM's understanding of the silver-lead concentrates market, it is expected that the existing contracts can be extended at the same, or better, terms and conditions.

19.3 Concentrate Markets

19.3.1 Zinc Concentrates

Due to the content of mercury in the zinc concentrate, the material will mainly be sold to smelters in the European market. Fortunately, there are several options, all with the ability to process concentrates with elevated mercury levels.

Traders operate several blending facilities in Europe and Asia which could be used to blend the Vareš concentrates to a suitable grade for delivery to China (max. 600 ppm Hg), in the unlikely event that European smelters are unable to purchase them.

19.3.2 Silver-lead Concentrates

There is a shortage of lead concentrates in the market currently, especially for those with high silver, resulting in a low level of treatment charges that is expected to remain for the foreseeable future. This is supported by the fact that ADT was able to secure a USD 25 million prepayment agreement from one of its customers, coupled with extended offtake agreements for approximately 100kt of zinc and silver-lead concentrates into 2027, with increased payabilities and lower treatment charges compared to existing offtakes.

19.4 Commodity Price Projections

Price projections used in DPM's financial model are taken from presented in Table 22-1. DPM has sourced these from the Bloomberg analyst consensus metal price forecasts. The QP has cross referenced independent consensus market forecast prices to which it subscribes, and finds the costs in Table 22-1 to align with these, other than the antimony prices, for which the QP has no information. Antimony accounts for 0.1% of revenue, so its price forecast is not material.

Table 19-1: Commodity Prices

Commodity	Unit	2025	2026	2027	2028	2029-LTP
Zinc	(USD/t)	2,806	2,771	2,766	2,780	2,661
Lead	(USD/t)	2,076	2,059	2,082	2,050	2,064
Copper	(USD/t)	8,818	9,811	10,119	10,362	9,348
Gold	(USD/oz)	2,300	2,621	2,490	2,363	2,212
Silver	(USD/oz)	27.00	31.87	30.76	29.08	27.69
Antimony	(USD/t)	2,300	2,300	2,300	2,300	2,300

ITEM 20. ENVIRONMENTAL STUDIES, PERMITTING, AND SOCIAL OR COMMUNITY IMPACT

20.1 Introduction

The environmental, social and governance (ESG) input has been prepared based on a desktop review of information made available to the QPs and a site visit by an SRK ESG specialist. The site visit included visiting the mine and processing facilities, and discussions with the General Manager of Sustainability and Business Optimisation (Section 2.3).

Key documents informing ESG commentary include:

- Vareš and Rupice Feasibility Study Report (Ausenco, September 2021);
- Vareš Polymetallic Mine ESIA (WAI, February 2022) and supporting environmental and social management plans (as updated);
- Permit Register 2013-2023 (ADT, 2023);
- Vareš Silver Operation corporate presentation (ADT, March 2025);
- Annual Report for the Year Ended 31 December 2024 (ADT, March 2025);
- 2024 Rupice Mineral Resource and Reserves Update (ADT, March 2025);
- Vareš Operation Monthly reports (ADT, 2024 and 2025); and
- Operations Update (ADT, March 2025).

Background information on environmental permitting requirements, the status of environmental approvals and compliance is covered in Item 4.

20.2 Environmental and social management

20.2.1 Status of assessments and studies

Several environmental and social assessments have been completed for the mine. Two environmental impact assessment (EIA) processes were undertaken by local consultants to support the in-country permitting process. Tuzla Mining Institute conducted an EIA process for the Rupice Mine and Enova consultants conducted an EIA process for the Vareš Processing Plant (VPP). These assessments were conducted in accordance with Bosnian requirements and reports submitted to the Ministry for Environment and Tourism. Ms Harris did not receive these reports, or subsequent environmental permits, but understands that environmental permits were granted in 2020 (VPP) and 2021 (Rupice) (ADT, 2023).

A subsequent ESIA process was conducted by WAI to facilitate project financing. This assessment, completed in 2022, was reported to have been conducted in accordance with the Equator Principles, International Finance Corporation (IFC) Performance Standards and European Bank for Reconstruction and Development (EBRD) Environmental and Social Policy and associated Performance Requirements. The process included seasonal baseline data collection, and qualitative and quantitative assessment of impacts relating to greenhouse gas and climate change, soils and contaminated land, air quality, noise and vibration, hydrology and hydrogeology, geochemistry, social, archaeology, landscape and visual, biodiversity, ecosystem services and land use.

After completion of the 2022 ESIA, and following the constitutional court decision in 2024 (Item 4.5), the Veovaca TSF was introduced to the project description. This facility was not included in the previous assessments as a preferred or alternative location for tailings storage. A separate local EIA process was conducted for this facility in 2024, in accordance with Bosnian requirements, to obtain environmental approvals for this facility. Ms Harris was not provided with this assessment and is also not aware of additional impact assessments being conducted for this facility to align with international financing requirements.

As part of the project financing process, the operator has an Environmental and Social Action Plan (ESAP) that aims to ensure conformance with EBRD Environmental and Social Policy and associated Performance Requirements. Ms Harris was not provided with a copy of the current ESAP or reports from independent environmental and social monitoring of the plan that has occurred since the finding was provided. Ms Harris therefore cannot comment on the status of conformance with the ESAP. While the original project documentation was prepared to align with the Performance Requirements, it is not clear whether this level of conformance has been extended through recent changes to the project design and retained during project implementation.

20.2.2 Management systems

Operationally, environmental and social issues are managed by the Sustainability and Business Optimisation business unit, which consists of nine teams including health and safety, emergency response, security, environment, stakeholder management, and communications among others. The operation has implemented an integrated management system including environmental and social elements, which is managed through an online platform (INX). The system includes policies, legal and other obligations, risk registers, management plans, incidents, inspections and other documents.

A suite of 18 environmental and social management plans were originally prepared as part of the 2022 ESIA. These plans are being updated to reflect the current stage of operation, and to satisfy requirements of regulatory permits, as well as measures included in the 2022 ESIA.

The operation has an annual monitoring programme aligned with permits and management plan requirements. Ms Harris did not receive a copy of this programme but understands from monthly reports that monitoring is conducted for groundwater and surface water (monthly or quarterly depending on location), noise (bi-annually), air quality (quarterly), biodiversity (seasonally) and waste management (monthly). Monitoring data and regulatory reports were not shared with Ms Harris as part of the review. Therefore, the status of permit compliance and operational effectiveness of management measures could not be confirmed.

20.2.3 Local content

Some 85% of the workforce represented by Bosnian nationals and procurement from local sources represents 74% of total procurement expenditure (Vareš corporate presentation, ADT March 2025). The proportion of local content attributable to the communities closest to the mine is not provided in the data reviewed.

The Adriatic Foundation was established in 2021 as a charity to support local communities, funding initiatives selected by the local community representatives in education and training, healthcare, and sustainability. In 2024, USD 100,000 was donated by ADT to the Foundation.

20.2.4 Stakeholder engagement

The operation has a recently updated stakeholder engagement plan, including stakeholder mapping, communication activities, key issues, monitoring and evaluation. The communication plan includes extensive engagement through several communication channels, including newsletters, meetings, local Information Centres, community bulletin boards, radio and online media. A Public Liaison Committee was established in 2020 with representatives from local communities most affected by the operation, key institutions, non-governmental organisations, utilities companies, business owners and municipal authorities. The group has a total of 30 voluntary members and meets quarterly.

Grievances are managed through a grievance mechanism that is reportedly aligned with UN Guiding Principles on Business and Human Rights. In 2024, 13 grievances were raised, of which 10 have been closed. Five grievances have been raised between January and March 2025, of which one has been closed. The remaining open grievances mostly relate to property damage from the haul road, noise and concerns about impacts from Veovaca TSF.

During discussions, ADT indicated it has broad support for the operation but recognises the need for continued efforts to improve relations, specifically with communities around the VPP and Veovaca TSF, along the haul road, and with stakeholders in the adjacent Kakanj municipality. The most common concerns raised by stakeholders relate to the potential for community health impacts, particularly dust from vehicle movements near VPP, environmental impacts specifically on water courses, air quality and biodiversity, and requests for local employment and procurement.

Insufficient historical engagement with communities around the Veovaca TSF has resulted in disagreements about use of a public road for transport of tailings whilst construction of a dedicated access road is being completed. Intense efforts have been required by the operator to negotiate a short-term agreement with these communities to maintain road use for two months (to June 2025).

Following historically limited engagement with stakeholders in Kakanj Municipality, ADT has been seeking to establish constructive relationships through actively enhancing engagement activities, including the opening of an information centre in 2025, employment of local workers and increased active coordination with local authorities. Future concession agreements and exploration licences to the west of the existing concession area will require approval by the Kakanj Municipality.

In 2022, stakeholders in Kakanj Municipality raised a complaint against the operation that is being actively investigated by the Independent Project Accountability Mechanism (IPAM), an arm of the European Bank of Reconstruction and Development (EBRD). The same complaint was raised with Secretariat of the Bern Convention (discussed in Item 4.5.2). The complaint was raised by residents of the Trstionica and Boriva Nature Park and includes concerns relating to impacts on natural resources (forest removal, landslides), water resources (surface water quality) and adequacy of community engagement. An assessment was completed in 2022 and a compliance review is expected to be completed in July 2025.

20.3 ESG Factors

This Item presents ESG factors that could be Modifying Factors when reporting Ore Reserves and may influence the determination of economic extraction. The concept of double materiality is applied, with potential ESG impacts from the operation considered equally to impacts posed by the ESG setting to the operation. For this assessment, potentially material is assumed to be factors that could:

- Stop or affect the continuation of operations, or obtaining and maintaining of approvals;
- Pose major concern to stakeholders and/or could affect the social licence to operate (this includes local communities, potential business stakeholders and non-governmental or community organisations);
- Lead to mis-alignment with corporate strategies or policies; and/or
- Result in the need for additional studies or costs that could affect the proposed design and/or operation and thus the value of the assets (e.g., design changes, operational management requirements, cash flow restrictions, rehabilitation/closure demands).

The potential for materiality has been identified on the basis of:

- Experience of ESG reviewer;
- Understanding of the location; proposed operation; regulatory and governance structure; socio-political situation; environmental and social setting; described in Items 4, 5 and 20 of this Technical Report; and
- Understanding of potential investors' expectations on ESG disclosure.

20.3.1 Permitting and approvals

Due to the lack of information provided during the preparation of this Technical Report, including the outcome of any parallel legal due diligence, it has not been possible to confirm:

- whether surface rights are secured and conditions of rights-holding are being met;
- if existing infrastructure has all the required permits and the operation is in compliance with any conditions of approval in these permits;
- the status of permit applications still required for construction of time-critical project components, such as the Veovaca TSF access road and return water pipeline, and the paste backfill plant;
- if the VPP environmental permit renewal has been issued; and
- if the current permit conditions and approved project documentation are aligned with the updated LoM plan and whether amendments to permits will be required to address changes introduced by the new plan.

Additional permitting matters relating to waste facilities are presented in Item 20.3.5.

A delay to obtaining required rights, permits, or altered permit conditions, could interrupt operations or affect the duration of the ramp up schedule. Any compliance-related issues may also result in a fine being issued, permits being revoked or future renewals or permits requests being declined.

On-going legal proceedings (if any) would also pose a threat to mineral rights, surface rights and environmental approvals.

20.3.2 Management controls

Due to the absence of monitoring data and regulatory reports being provided to SRK, the status of compliance and effectiveness of management controls at Rupice Mine and VPP cannot be confirmed. In addition to the regulatory risks on non-compliance described above, if management controls are insufficient, additional capital expenditure may be required to upgrade operational infrastructure and / or address any actual impacts.

Without the EIA for the Veovaca TSF, it is not possible to confirm whether baseline data collection is sufficient, particularly upgradient of the facility, and impacts from the tailings facility on people and the environment have been appropriately assessed. In particular, the sufficiency of assessment and measures to control surface water and groundwater impacts downgradient of the facility during operations and post-closure are unclear. If management controls incorporated into the facility design prove inadequate to control impacts, this may result in the need for additional remedial actions with associated costs.

20.3.3 Community relations

While ADT reported broad support for the operation, issues raised by certain stakeholder groups could escalate and result in interruptions to operations, the maintenance and acquisition of licences and permits, and reputational damage. The status of community relations could be affected by:

- Perceptions regarding impacts from the mine on the Bukovica water supply source and discharge water quality from Rupice Mine affecting surface watercourses (Vruci Potok), and thus downstream receptors in Kakanj Municipality, resulting in reputational issues.
- Continued complaints about noise and dust along the haul roads from VPP to Rupice Mine and to Veovaca TSF, resulting in deterioration of relationships and reputational damage;
- Failure to meet the conditions of the community agreement to use the public access road to Veovaca TSF, resulting in interruptions to tailings haulage until the dedicated access road can be completed;
- Active slope failure of the Temporary TSF (Item 18.4.2) resulting in community concern and reputational damage;
- Potential traffic incidents with mine-related vehicles on the publicly accessible haul road, resulting in blockage of the access road and reputational impacts.
- Perceptions around insufficient local benefits from the operation, with regards to employment and procurement opportunities.

Continued engagement efforts, through the existing communication channels such as the Public Liaison Committee and other forums, and enhanced efforts with certain stakeholder groups will be required to minimise risks from community relations. However, it will remain an ongoing challenge, with any single of these individual threats potentially leading to a loss of social licence.

20.3.4 Water stewardship

In addition to the findings from the water management review (Item 18.5), the key water stewardship issues that may represent modifying factors from an ESG perspective are as follows:

Impacts on water supply sources

The mining concession directly abuts the catchment divide with the Bukovica River catchment, which is an important water supply source for communities in the Kakanj Municipality. Risks from the mine to the water supply source have been highlighted in permit conditions (Item 4.4), previous audits and are the subject of third-party complaints. Several hydrogeological studies have been conducted to confirm the impact from the mine on the Bukovica water supply source. These studies have concluded a low probability of connection, however, there are weaknesses in the studies that limit confidence in the findings. Until future studies and additional appropriate hydrogeological test work confirm more confidently the lack of connection, there remains a reputational risk and a threat to maintaining regulatory approvals.

Rupice discharge water quality

Management of water quality, particularly suspended solids, in runoff from the mine site is a risk in terms of potential downstream impacts for the Vruci Potok catchment. Discharge quality has been the focus of a significant number of regulatory environmental inspections and stakeholder complaints. In 2024, 6 water quality incidents were recorded (elevated sediment and foam in Vruci Potok), one of which resulted in a penalty fine from water inspection authorities (October monthly report, ADT 2024).

The site discharges ‘contact’ water and ‘non-contact’ water. ‘Contact’ water is collected and treated prior to discharge in the Vruci Potok. Surface run-off from disturbed areas of the site that does not come into contact with the ore stockpiles, waste dumps or paste backfill plant is considered ‘non-contact’ and is diverted and discharged from the site without treatment. The QP suggests this surface water management approach could lead to poor downstream water quality in the Vruci Potok, especially with regards to suspended solids. Best-practice is to consider diverting runoff from any disturbed ground associated within the operation to a suitably designed sediment pond, with additional water quality treatment as required.

DPM has indicated that it intends considering all site water as contact water, however this is yet to be developed and incorporated into an update water management plan.

Additional costs are likely to be required to increase capacities of surface water infrastructure to improve management of surface run off and reduce suspended sediments in site discharge. Costs may also be required to manage ‘non-contact’ water if elevated sediment remains an issue with downstream users.

Impacts on downstream receptors

Topography at both the Rupice Mine site and Veovača processing plant/TSF area is steep with key water receptors, such as water supply abstractions, local communities and sensitive habitats, located downstream from the mine and processing sites. This, together with a potentially locally high permeability underlying groundwater system, creates a high risk of mining activities impacting on downstream water users. Little data have been provided in terms of how potential downstream water impacts have been assessed at the Veovača TSF. Monitoring data have been unavailable to confirm the current impacts occurring in downstream watercourses from any of the mine infrastructure. As previously stated, if management controls are insufficient, additional capital expenditure may be required to upgrade water management infrastructure on site to reduce the source of potential impacts.

Modified baseline

Both the mine site and the processing plant catchments have been significantly impacted by other catchment activities such as forestry and historical mining. These pre-existing legacy and current catchment impacts present a risk that:

- Historical and on-going impacts from other catchment users might be wrongly assigned to impacts from the operation; or
- Potential impacts from the operation in addition to impacts from other catchment users (current or historical) results in cumulative impacts that are unacceptable despite these impacts not reaching impact thresholds when considered in isolation.

These risks may contribute to a deterioration of stakeholder relations and require additional studies to define the responsibilities for impacts and remediation.

20.3.5 Waste management

Regulatory mine waste management plans prepared as part of the permitting process were not available as part of the QP's review, therefore alignment between permitted and operational practices has not been confirmed.

To enable the LoM plan to be implemented, permits remain outstanding for:

- 600,000 t of waste rock storage at Rupice, of which a proportion will be potentially acid generating; and
- Phase 2 Veovaca TSF (required from approximately Year 5).

Permitting for these facilities should be completed as a priority.

A review of the waste management strategy in the context of the revised LoM plan is also required to estimate expected volumes of non-acid-generating (NAG) or potentially acid generating (PAG) material, to confirm appropriate locations with appropriate environmental controls for each type. Should additional waste facilities take longer to identify, design and permit than anticipated, there may be a delay to the overall schedule. It's also unclear whether costs for additional waste rock facilities have been included in the financial model.

The change to waste capacities at Rupice Mine may also affect the management of the 'Red Rock' waste rock dump located close to the mine site. Ms Harris was verbally informed that this facility contains NAG waste generated from construction of the Run of Mine pad and development waste from underground. The dump was planned as a temporary facility with a plan to relocate the waste back to the mine site during operation, however, with the current surplus of mine waste this may no longer be viable. There is a risk unplanned costs will be incurred from hauling the waste to an alternative location, or rehabilitating the waste facility at its current location.

Additional costs may also arise from relocation of the Temporary TSF to Veovaca TSF for final storage. As part of the agreement negotiated with communities surrounding the VPP in March 2025, it has been agreed that relocation of the temporary TSF will be carried out within a period of 36 months, beginning in May 2025.

20.3.6 Climate change

Decarbonisation

Bosnia and Herzegovina is committed to collaborate with the EU in achieving net-zero emissions across the continent by 2050. To support this goal, Bosnia and Herzegovina is preparing to introduce a carbon pricing and trading system, including a carbon tax by January 2026. This system is primarily in response to the EU Carbon Border Adjustment Mechanism (CBAM) that will impose taxes on the import of certain goods (including iron, steel, cement and electricity) from countries without similar carbon pricing systems. The tax will be at or above the EU Emissions Trading Scheme allowance price. It is unclear whether the Bosnian carbon pricing and trading scheme will apply directly to the operation. As a minimum, the introduction of the carbon tax is expected to lead to an increase in electricity prices, and as costs are passed onto consumers, result in likely increases to operating costs for the mine.

The 2022 ESIA (WAI, 2022) estimates LoM Scope 1 and Scope 2 emissions to reach 575,000 tCO2, with the use of electricity by the process plant being the largest contributor. The peak annual emissions were predicted to be 66,000 tCO2 once the mine reached full production. In 2024, the operation emitted approximately 12,000 tCO2 (Scope 1 and Scope 2 emissions). This estimate accounted for emissions avoided through the 32kW solar infrastructure, which is now operational, providing power to both processing and administrative facilities. The operation's emissions profile is expected to rise for 2025 and beyond as concentrate production continues to ramp up.

Neither ADT nor DPM has set clear carbon reduction targets for the operation or developed a decarbonisation strategy. In the medium and long term, capital expenditure is likely to be required to implement carbon reduction projects however the magnitude of capital costs will remain undefined until a decarbonisation strategy is prepared. There is a risk both short-term costs (impacts from carbon tax) and medium/long-term capital requirements could impact financial performance.

Climate adaptation

Based on the expected future climate change scenarios (briefly described in Item 5.3), a physical climate risk assessment conducted by ADT identified flooding and wildfire as the highest climate-related risks (ADT, March 2025). Forest fires have not yet caused damage to mine infrastructure but are considered in emergency response plans. Storms and subsequent flooding in October 2024 resulted in damage to certain sections of the railway line to Ploče used by the operation and necessitated trucking of concentrate by road until the railway was repaired.

It does not appear that climate change considerations have been included in the design of surface water management infrastructure. Changes or upgrades may be required to provide additional capacity to manage extreme events and could result in additional capital expenditure.

ADT has also stated in the 2024 Annual Report (ADT, March 2025) that future climate change risks could impact the closure provision (Item 20.3.7) both in terms of the nature of decommissioning and rehabilitation required to deal with more extreme events.

20.3.7 Closure and rehabilitation

According to the 'Law on the Mining Industry' of the Federation of Bosnia and Herzegovina (Law 01-02-224/10, April 2010), exploitation permit holders have an obligation to remediate and reclaim the area impacted from mining. The operator must submit a closure plan at the end of operations to obtain a permit for suspension, and implement activities to eliminate dangers to health and safety of people and property, and potential causes of environmental pollution. The responsible authority will issue a closure certificate to confirm sufficient works have been completed.

The Decree on Financial and Other Guarantees to Cover the Costs of Risk of Possible Damage, Cleaning and Post-Closure Procedures ("Official Gazette of the Federation of BiH", No. 39/06) addresses the coverage of the costs of the risk of possible damage, rehabilitation and procedures after the closure of 'landfills'. Financial guarantee can be in the form of a surety bond, letter of credit or insurance policy. The amount of the financial guarantee must be proportionate to the costs estimated within the landfill closure plan and include 30 years of post-closure aftercare and monitoring. The requirement for, and status of, a guarantee by the operator under this legislation is not clear from the available information.

The operation has a Conceptual Mine Rehabilitation and Closure Plan, last updated in October 2024 to include the Veovaca TSF location. Closure-specific stakeholder engagement has not yet been conducted to inform the closure vision, but the assumed vision is to return the Rupice area to forested land and to remove mine-related infrastructure from VPP and prepare the site for future re-use. Key assumptions included in the plan include no waste rock remaining on surface at closure, no extensive water management or treatment will be required at Rupice, VPP or for the TSF, and post-closure monitoring will be required for 5-years.

For waste rock, the current LoM plan will result in over 100,000 t of waste rock remaining on surface at closure. This will be an addition to the currently planned closure activities and costs.

Regarding water management, the plan states that groundwater recharge volumes and quality will be assessed through a hydrogeological study conducted during operations with provision made in future closure plan updates for final containment or treatment, if required. These provisions could be material depending on the nature of management and treatment activities required. In particular, the study and treatment requirements will need to include geochemical testing of backfill and modelling of contaminant transport in groundwater during and following rebound through the backfilled voids.

The need for post-closure water management and treatment for Veovaca TSF is also unspecified. The proposed 5-year post-closure monitoring timeframe is short compared with potential legal aftercare obligations extending to 30 years for the TSF.

20.4 Conclusion

The operation has been subject to several environmental and social assessments during project development. The EIA reports prepared to inform regulatory permitting processes were not provided for review. While the original project financing documentation (2022 ESIA) reports to be aligned with good international industry practice (defined as IFC Performance Standards and EBRD Performance Requirements), it is not clear whether this level of rigour has been extended through more recent changes to the project design, permitting and retained during the implementation phase.

Although the operator reports it has the necessary approvals, insufficient information has been provided for this review to confirm the status of permitting and compliance with approval conditions. Risks remain with regards to maintaining approvals and obtaining outstanding permissions for waste rock and tailings storage to support the LoM plan.

Based on a review of ESG Factors that could be Modifying Factors when reporting Ore Reserves and which may influence the determination of economic extraction, several issues have been identified that have the potential to interrupt operations, delay the ramp up schedule or result in additional capital or operating costs. These factors relate to permitting, environmental and social management, stakeholder engagement, and operational water and waste management, climate change and closure. These are presented as qualitative risks rather than adjustments to the LoM plan or financial model.

ITEM 21. CAPITAL AND OPERATING COSTS

21.1 Capital Cost Estimates

Basis of Estimate

DPM has revised the capital costs estimated by ADT during the course of the QPs' review. The mine being mostly constructed, has derisked much of the unknowns associated with the start-up capital. The initial and sustaining capital costs are presented in Table 21-4.

Exploration

The USD 5 million exploration budget described in Item 9.2 is not included in the financial model, as it is not a required spend to support the Mineral Reserves. Any resulting positive results will be presented in future economic assessment.

Drilling

Expenditure for infill and geotechnical drilling has been included, amounting to USD 12 million from H2 2025 and extending a further 8 years, including associated studies to interpret data and revise mine design and planning accordingly.

Mining

The mining capital primarily consists of capitalised underground development, mining infrastructure, purchase of additional mining equipment to ramp up to full production, and replacement thereof during the life of the mine. DPM reports its capital cost estimate is based on unit estimates taken from benchmarking analysis from an analogue operation in the Balkans region. The breakdown is presented in Table 21-1.

Table 21-1 Mining Capital Estimate (USD million)

Item	Description	Initial	Sustaining	Total
Mine Development	Capex development,19,050m	16.0	54.5	70.5
Underground Facilities	Infrastructure	4.1	0.0	4.1
Ventilation Infrastructure	Raises, raisebored	1.6	3.8	5.4
Dewatering Infrastructure	Pumpstations x3	0.0	0.4	0.4
Electrical Infrastructure	Follows capex development	4.4	14.9	19.3
Communications System	Follows capex development	0.4	1.1	1.5
Safety Infrastructure	Escapeways and Refuge Bays	0.1	0.2	0.3
Backfill Infrastructure	Reticulation pipework	0.5	1.7	2.2
Compressed Air	Compressors x 3	0.2	0.1	0.3
Service Water	Pressure reducers x 6	0.0	0.0	0.0
Equipment Purchases	Mobile equipment	15.2	24.6	39.8
Total		**42.5**	**101.4**	**143.9**

Physical details of each item and the build-up of costs have not been available for review, so it is unclear which items are intended to be completed by in-house or contractor resources. Apart from the Mine Development, which is confirmed as being in accordance with the provided design files, no plans for other excavations are included in the mine plan design file provided.

Overall, the mining capital estimate appears plausible though the weighting of the development costs should be supported by a build-up analysis to demonstrate that the known difficult conditions at Rupice have been captured in the rate (USD 3,700/m). Given the PFS level of confidence of the known design, the QP considers the contingency of 7.5% to account for items not specifically identified at this time.

Process Plant

The process plant construction is overall complete, with a few areas identified since commissioning that require additional plant components. This includes an additional tailings filter, an upgrade to the concentrate filter, an upgrade to the thickener, and an upgrade to the plant automation.

The backfill plant remains to be constructed. The QP has been informed that equipment has been purchased, however, construction is yet to be executed. It is estimated that the plant all in cost will amount to USD 12 million. The QP does not have clear up to date information on the status of the construction, and an outstanding cost of USD 4 million. This figure is an estimate only.

RoM and Filtered Tails Haulage

Stabilisation of the 25 km haul road: the QP has highlighted this as an area of risk to uninterrupted operations of mining and processing. DPM and SRK have included USD 3 million for additional construction, including replacing road base material, asphalt replacement, rectification of the slope failure(s). The USD 3 million is an allowance only at this stage and there is a high likelihood that more work is required. This allowance also assumes the construction work planned for 2025 as part of the on-going construction work to finalise the road is completed prior to acquisition.

Access road to Veovaca TSF: Construction had commenced at the time of SRK's site visit and it is assumed that this access road and associated return water pipeline will have been completed by the time of the completion of DPM's acquisition of the asset.

Tailings

Costs are presented for the WA design for storage of 5.1 Mt of tailings at the Veovaca TSF (which is more tonnage/capacity than is required by the DPM project LoM). Capital cost totals USD 3.0 million and sustaining capital totals USD 12.2 million, including a 30% contingency which is appropriate for a PFS-level design. Closure cost for the TSF is USD 3.9 million.

Water Management Facilities

Additional capital cost has been included to allow for the upgrade the WTP capacity to reflect the higher loading from a larger above-ground WRD than was assumed in the DFS. An allowance of USD 5 million has been made, for water treatment, storage and general related infrastructure across the site, to deal with contact water and non-contact water, which DPM plans to treat in the same manner.

Power

An allowance has been made for minor modification to the power supply system, amounting to USD 2 million of initial capital in 2025 and 2026.

Indirect Costs

No additional indirect costs are required due to the near completion status of the mine and the nature of capital costs being relatively minor in value and engineering requirements other than that provided by the current mine engineering office.

Contingency

A contingency of 7.5% has been applied to all capital costs, initial and sustaining. Despite numerous designs for the capital items not meeting FS at present, there is good knowledge of costs from other mines in the Balkans region. Further, the mine being in early-stage operation results in more DFS assumptions having been derisked and unknowns having been identified. The QPs consider the contingency rate to be reasonable.

Closure Costs

The DFS closure plan included a LoM closure cost estimate of USD 5.9 million for physical closure activities, USD 12.5 million for social closure, including redundancy payments and USD 0.6 million for post-closure monitoring. This results in a total closure liability of USD 19 million. It is not clear if this includes sufficient earthworks for the capping of the Veovaca TSF. The asset retirement obligation disclosed in the 2024 annual report (ADT, March 2025) was USD 5.4 million. The similarity between the 2024 ARO and LoM cost also indicates an under-estimation of the LoM cost, as the Veovaca TSF was not in operation at the end of 2024 and will add to the reclamation liability once this commences. DPM has provided an increased allowance for closure in the financial model of USD 24 million.

The QP was not provided with the detailed breakdown of the ADT or DPM closure cost estimates. However, in the QP's opinion, there is a risk the costs are under-estimated. This is due to uncertainty about whether closure costs for Veovaca TSF have been included, uncertainties and optimistic assumptions regarding waste rock volumes on surface at closure, post-closure water management and the short duration of proposed monitoring requirements.

Other

ADT had carried over USD 6.2 million from 2024, due to be spent up till June 2025, with the majority spent in May and June 2025. The QP assumes that this expenditure will be spent prior to completion of DPM's purchase and taken into account in the transaction.

21.2 Operating Cost Estimates

Basis of Estimate

The operating costs are partly based on DPM's revised costs (notably mining) and ADT existing costs (processing and G&A). The consolidated operating costs are presented in Table 21-4.

Mining

DPM's estimate of mining operating cost was prepared by scaling the characteristics of a known Balkans analogue, and adjusted to reflect identified characteristics at the Rupice underground mine. Adjustments for LHOS, include for production rate, poorer ground conditions, higher cement content in pastefill due to stoping sequence creating more exposures, all driving costs.

Adjustment for MCAF, compared with LHOS, has considered the lower productivity, lower ore yield, resulting in a higher cost per unit activity, and a reduced backfill cost due to lower cement content.

Cost of producing filter cake for paste backfill and haulage thereof is included in the process plant operating cost.

The QP notes that operations have not yet reached a steady state rate equivalent to the targeted production level and until that occurs, there is a reasonable likelyhood that the operation will encounter further disruptive, as yet unknown, conditions. The adjusted costs shown in Table 21-2 are based on DPM's assessment of known conditions, and are at a PFS level of confidence. With further significant changes to be experienced in the future (pastefill operations, MCAF mining), a further contingency should be added to the adjusted costs for the risk of currently unknown conditions. The contingency of 7.5% is appropriate, considering that DPM's adjustments are based on somewhat, but not fully, derisked conditions.

Table 21-2: Mining Unit Operating Cost

Mining	LHOS (USD/t)	MC&F (USD/t)
Mining		
Fuel	3.75	5.6
Power	6.79	10.2
Development materials and consumables (e.g. ground support)	4.92	7.4
Stope drilling (consumables/maintenance)	5.60	8.4
Stope blasting (consumables/maintenance)	1.91	2.9
Mucking (consumables/maintenance)	1.29	1.9
Haulage (consumables/maintenance)	1.22	1.2
Backfill	5.76	5.2
Mobile maintenance (UG workshop)	0.19	0.2
Dewatering (40 l/s)	0.30	0.3
Mine safety	1.60	2.1
Logistics	0.99	1.1
Mine labour (staff & hourly)	12.78	19.2
Other	1.57	1.6
Total	**48.7**	**67.2**

The QP notes that in the financial model unit costs of USD 50/t for LHOS and USD 70/t for MC&F have been included. This is before the additional contingency of 7.5% (described ahead in this Item).

Process Plant and Tailings Disposal

The processing unit cost is based on ADT's actual and forecast figures. DPM has revised these to reflect higher anticipated reagents and consumables, a higher haulage along the 25 km haul road. Some duplication of costs resulting from DPM's newly estimated mining unit costs have been removed, notably the cost of backfilling in the underground mine. The freight costs have been modelled as part of the concentrate payment terms (supported by sale contracts), and laboratory and assay costs have been included in general and administration costs. Some minor unknowns remain, including the revised energy use once plant upgrades have been introduced, and the cost of filtering of tailings, however, these costs are deemed to be comfortably covered by the contingency of 7.5% (described ahead in this Item). The QP finds the processing unit cost to be reasonable and well supported.

The QP finds the tailings costs seem reasonable for this type and style of facility, in this location and local-cost base. Limited associated information validates the costs, deemed to remain at a PFS level of accuracy. The unit cost is based on the technical risks (in the preceding report Items), and account for re-working of out-of-specification tailings and/or additional equipment and compactive effort required in critical zones of the TSF, specifically including the downstream tailings slope shell and in the areas adjacent to the side-slope lining system. The tailings hauled to the Veovaca TSF and disposal thereof results in a unit cost of USD 2.73/t tailings, or USD 1.45/t run of mine ore (53% of tailings are stored in the Veovaca TSF, and 47% returned to the mine via the paste backfill plant).

Table 21-3: Processing Unit Operating Cost

Processing	Unit (USD/t)
Variable Costs	
Plant Reagents & Consumables	8.16
Plant Maintenance	1.17
Plant Power	6.54
Ore and tailings hauling (to paste plant)	4.34
Tailings disposal	1.45
Backfilling - included in Mining	-
Concentrate freight - in con payment terms	-
Fixed Costs	
Labour (Processing)	4.35
Laboratory and Assays – included in G&A	-
Total	**26.01**

Water Management

The QP notes that the operating cost associated with an upgrade the surface water management is to be assessed. However, this is not expected to be a relative material cost.

Surface Infrastructure and RoM Haulage

Using the costs to date as the basis, a maintenance budget allowance has been developed by DPM beyond that already assigned for snow clearance and de-icing. This budget results in an average monthly cost estimated at BAM 50,000 to BAM 60,000 (e.g. USD 30,000 to USD 35,000) per annum, which is included in the forecast operating costs.

The cost for the ore haulage and backhaul of filtered tailings to the past backfill plant is estimated to be USD 3.00/t, which seems reasonable and aligns with that predicted in the DFS.

General and Administration

The general and administration costs are deemed to be in the correct order of magnitude. These will be better understood once the identified capital projects are executed and the ramp-up to full production is achieved. The cost may then reduce somewhat.

The financial model does not include provision for impacts from the forthcoming carbon tax, or capital requirements for decarbonisation activities or infrastructure upgrades for resilience to future climate scenarios. There is also a risk that costs may also arise due to a need for additional environmental controls to manage impacts from the operation, but no specific provision has been made at this stage.

Contingency

A contingency of 7.5% has been applied to all operating costs. Despite the mine design and mine plan being at PFS at present, there is good knowledge of costs from other mines in the Balkans region. Further, the mine being in early-stage operation results in more DFS assumptions having been derisked and unknowns having been identified. The QPs consider the contingency rate to be reasonable.

Table 21-4: Summary of Capital and Operating Costs

Year	Unit	Total	P2025*	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040
Capital Costs																		
Initial Capital																		
Mine Development	(USDm)	**16**	5.4	10.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Mine Infrastructure	(USDm)	**11**	2.9	8.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Mine Equipment	(USDm)	**15**	12.4	2.7	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Backfill Plant	(USDm)	**4**	2.0	2.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Surface water	(USDm)	**5**	2.5	2.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Electrical distribution	(USDm)	**2**	1.0	1.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Main haul road	(USDm)	**2**	1.2	1.2	-	-	-	-	-	-	-	-	-	-	-	-	-	-
One Tailings filter	(USDm)	**5**	5.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Upgrade concentrate filter	(USDm)	**2**	1.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Upgrade thickener	(USDm)	**1**	0.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Upgrade Automation	(USDm)	**2**	1.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Resource / Geotech Drilling	(USDm)	**3**	0.8	2.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-
TSF initial capital	(USDm)	**3**	1.5	1.5	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Contingency	(USDm)	**5**	2.9	2.4	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Total initial capital	(USDm)	**76**	41.1	34.9	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Sustaining																		
Process sustaining	(USDm)	**10**	0.3	0.4	0.8	0.8	0.9	0.8	0.9	0.9	0.9	0.9	0.9	0.6	0.5	0.2	0.1	-
Mine Development	(USDm)	**54**	-	-	10.7	9.1	11.0	8.7	7.5	4.8	2.8	-	-	-	-	-	-	-
Mine Infrastructure	(USDm)	**22**	-	-	4.6	3.3	4.4	3.6	2.8	1.8	1.1	0.2	0.2	0.2	0.1	0.0	-	-
Mine Equipment	(USDm)	**25**	-	-	-	0.3	3.2	7.0	3.9	4.3	1.2	3.3	1.2	0.2	-	-	-	-
TSF	(USDm)	**12**	-	-	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	0.8	0.6	0.3	0.0	-
Main haul road	(USDm)	**1**	-	-	1.2	-	-	-	-	-	-	-	-	-	-	-	-	-
Resource / Geotech Drilling	(USDm)	**8**	-	-	2.0	2.0	1.0	1.0	1.0	0.6	0.6	-	-	-	-	-	-	-
Exploration drilling	(USDm)	**-**	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Contingency	(USDm)	**10**	0.0	0.0	1.5	1.3	1.6	1.7	1.3	1.0	0.6	0.4	0.3	0.1	0.1	0.0	0.0	-
Total sustaining capital	(USDm)	**143**	0.3	0.4	22.0	17.9	23.2	24.0	18.5	14.5	8.4	5.9	3.6	1.9	1.3	0.5	0.1	-
Closure	(USDm)	**24**	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	24.0
Total Capital Costs	(USDm)	**243**	**41.3**	**35.3**	**22.0**	**17.9**	**23.2**	**24.0**	**18.5**	**14.5**	**8.4**	**5.9**	**3.6**	**1.9**	**1.3**	**0.5**	**0.1**	**24.0**

* P2025: partial year, 9 months starting 1 April.

Table 21-4 Continued

Operating Costs		Total	P2025*	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040
Mining	(USDm)	**570**	3.9	20.8	47.9	49.2	48.7	50.8	45.6	48.1	50.4	55.4	56.6	40.2	30.9	15.1	5.9	-
Processing+TSF	(USDm)	**246**	2.0	10.5	22.1	22.1	22.0	22.1	22.0	22.1	22.1	22.1	22.1	16.1	12.0	4.8	1.9	-
G&A	(USDm)	**142**	1.1	6.1	12.7	12.7	12.7	12.8	12.7	12.8	12.8	12.8	12.8	9.3	6.9	2.8	1.1	-
Contingency	(USDm)	**72**	0.5	2.8	6.2	6.3	6.2	6.4	6.0	6.2	6.4	6.8	6.9	5.0	3.7	1.7	0.7	-
Royalties	(USDm)	**21**	0.2	0.9	1.9	1.9	1.8	1.9	1.8	1.9	1.9	1.9	1.9	1.3	1.0	0.4	0.2	-
Total	(USDm)	**1,050**	7.8	41.1	90.8	92.1	91.5	94.0	88.1	91.0	93.5	98.9	100.2	71.9	54.6	24.8	9.8	-
Unit Operating Costs	(USD/t ore)	**111**	101	101	107	108	108	111	104	107	110	116	118	119	118	134	132	-

* P2025: partial year, 9 months starting 1 April.

ITEM 22. ECONOMIC ANALYSIS

22.1 Cautionary Statement

The results of the economic analysis represent forward-looking information that are subject to several known and unknown risks, uncertainties, and other factors that may cause actual results to differ materially from those presented here. Forward-looking information includes Mineral Resource and Mineral Reserve estimates; commodity prices and exchange rate; smelter terms; the proposed mine production plan; projected recovery rates; use of a process method, infrastructure construction costs and schedule; mine capital and operating costs; and assumptions that Project environmental approval and permitting will be forthcoming from local, state, and federal authorities.

22.2 Financial Model Methodology

Financial analysis of the Vareš Mine was carried out using a discounted cash flow (DCF) approach. This method of evaluation requires projecting yearly cash inflows, on 1 April 2025 money terms, through estimation of revenues, operating costs, capital costs, and taxes. The resulting net annual cash flows are discounted back to the date of valuation and totalled to determine the net present value (NPV) of the Mineral Asset at selected discount rates.

22.3 Financial Model Parameters

The economic evaluation is undertaken on a 100% ownership basis, reflecting DPM full ownership of the Mineral Asset.

The cash flow model start date is 1 April 2025. The NPV was discounted back to this date, using a mid-year discounting approach. The cash flow model is in real money terms, dated 1 April 2025, i.e. no inflation was included, and the base date of the costs is 1 April 2025.

Technical input parameters are presented in Table 22-6.

Revenue is derived from the sale of a silver-lead concentrate with a copper stream, and a zinc concentrate The concentrates are assumed to be sold in the year they are produced, with working capital costs applied according to existing contracts.

22.4 Metal Prices and Commercial Terms

Metal prices are presented in Item 19.4. The payabilities forecast by DPM, based on contracts and DPM's market knowledge, are presented in Table 22-1.

Table 22-1: Metal Payabilities (for the first 10 years)

Year	Total	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034
Zn	**75.3%**	76.7%	76.4%	75.6%	75.3%	75.8%	75.2%	74.9%	75.7%	74.9%	75.2%
Pb	**87.1%**	88.1%	86.9%	86.7%	87.1%	86.4%	87.4%	88.0%	87.9%	87.4%	86.4%
Cu	**20.4%**	20.7%	20.4%	20.2%	20.4%	20.2%	20.5%	20.9%	20.7%	20.6%	19.9%
Au	**74.2%**	83.7%	78.7%	77.6%	76.9%	78.2%	75.1%	75.7%	74.3%	70.8%	66.0%
Ag	**90.0%**	90.8%	90.1%	90.0%	90.1%	90.2%	90.3%	90.5%	90.2%	90.1%	89.4%
Sb	**11.6%**	5.7%	16.9%	20.5%	18.1%	23.1%	11.2%	11.0%	6.6%	-	-

22.5 Royalties

The application mining royalty in Bosnia is BAM 3.9/t RoM. The Bosnian mark is pegged to the EUR. DPM has applied the long-term analyst forecast USD:EUR foreign exchange rate (1.0933 at the time of calculation) resulting in USD 2.18/t RoM. There will be volatility in this, which is not deemed to have a material impact on the Mineral Asset economics.

22.6 Capital and Operating Costs

The capital and operating costs are presented in Item 21.

22.7 Corporate Tax Regime

The Corporate Income Tax (CIT) has been calculated using the current rate of 10%.

Capital costs are amortised in accordance with Bosnian tax and accounting regulations.

Tax losses are calculated and amortised considering the 5-year carry forward rule and 25% limitation based on annually generated taxable profits.

No opening balance reflecting undepreciated sunk costs has been included for deduction against concentrate sales revenue for the purposes of calculating CIT. This presents a small upside. Sunk costs, or tax losses, consist of capitalised investments, including pre-production costs, preparation and mine development costs.

For modelling purposes, closure costs are not amortised or expensed until the final years of the mine, during the closure phase.

The impact of value added tax is not modelled, as assumed to be 100% recoverable, mostly within the year affected.

22.8 Reclamation and Closure Costs

A closure cost of USD 24 million has been allowed for. See Item 21.1

22.9 Financing

The Vareš Mine is in production whereby the majority of the startup capital has been sunk. The remaining capital requirements is modelled as being paid by operating profit (post tax) or 100% equity financed. No debt or debt repayments are included within the financial model.

22.10 Inflation

The financial model is a real money terms model, assuming a date of 1 April 2025. No escalation or inflation are accounted for.

22.11 Working Capital

Working capital is the capital required to fund operations prior to receiving revenue from the finished product. It is defined as the current assets minus the current liabilities. The financial model estimates working capital by subtracting 30 days of direct operating costs from 30 days of revenue. Over the mine life, working capital nets to zero.

22.12 Sunk Costs

DPM has not included any sunk costs as opening value for the tax calculation, due to this value not having been verified at the time of the Report. This presents a small upside in the payable tax calculation.

22.13 Salvage Value

No salvage value is included within the financial model, reflecting recognised practice.

22.14 Financial Model Results

The revenue is detailed in Table 22-2, showing gross and net smelter revenue for the sale of zinc and lead concentrates. Table 22-3 shows a summary of net smelter revenue by commodity.

Table 22-2: Sales Revenue by Concentrate

Concentrate Sales Revenue	Zinc	Lead
	(USD million)	(USD million)
Gross Revenue		
Zn	1,176	6
Pb	-	684
Cu	-	100
Au	162	394
Ag	240	1,344
Sb	-	4
Total	**1,578**	**2,532**
Selling Costs		
Hg Penalty	-7	-8
As Penalty	-	-2
Sb Penalty	-	-15
Treatment Costs	-168	-61
Refining Costs	-	-50
Transport Costs	-37	-48
Other Selling Costs	-5	-13
Total	**-217**	**-197**
Net Revenue - Zinc Concentrate		
Zn	1,014	6
Pb	-	630
Cu	-	92
Au	140	364
Ag	207	1,240
Sb	-	4
Total	**1,361**	**2,335**

Table 22-3: Net Smelter Revenue Summary by Commodity

Commodity	USD million
Zn	1,019
Pb	630
Cu	92
Au	504
Ag	1,446
Sb	4
Total	**3,696**

The QP notes that DPM selected a 5% discount factor as being most appropriate for the economic assessment. Whereas no WACC has been calculated, the QP comments that this is reasonable reflecting the areas of high confidence, notably the marketability of the precious metals and contracts in place for the base metals, the work to date having derisked the project to a significant extent (FS unknowns mostly uncovered at present), most of the start-up capital has been sunk, therefore low technical and economic risk, and DPM having demonstrated its ability to operate in the region.

The summarised key technical and economic inputs and resulting economic indicators are presented in Table 22-4, Table 22-5 and Figure 22-1, with details provided in Table 22-6 and Table 22-7.

Table 22-4: Key Inputs and Financial Indicators

Description	Unit	Value
Macroeconomic Parameters		
Long term metal prices		
Gold	(USD/oz)	2,212
Silver	(USD/oz)	27.69
Zinc	(USD/lb)	1.21
Lead	(USD/lb)	0.94
Copper	(USD/lb)	4.24
Discount rate	(%)	5.0
Production		
Mineral reserve	(Mt)	9.5
Annual throughput	(ktpa)	850
Average grade processed (LoM average) (1)	(g/t Au Eq)	9.15
Gold equivalent recovery (LoM average)	(%)	85.4
Gold equivalent payability (LoM average)	(%)	76.2
Gold equivalent payable production (LoM)	(Moz Au Eq.)	1.8
LoM Operating Costs	**(USDm)**	(USD/t ore)
Mining	570	60
Processing + TSF	246	26
G&A	142	15
Contingency	72	8
Royalties	21	2
Total cash cost (2)	**1,050**	**111**
Offsite Cost (3)	414	
LoM All-in Sustaining Cost (co-prod) (2)	(USD/oz Au Eq.)	901
Capital Cost Estimate		
Initial Capital	(USDm)	76
Sustaining Capital (LOM)	(USDm)	143
Closure Costs	(USDm)	24
Project Economics		
Cash flow (post-tax)	(USDm)	2,071
NPV (after-tax, 5% discount)	(USDm)	1,585

Note:

(1) A Au equivalent grade is reported to align with DPM’s standard reporting format. The QP notes the Au contributes to 14% to the net revenue, whereas other metals contribute in the amounts of, Ag 39%, Zn 28%, Pb 17%, and Cu 2%. The reported grade was calculated from the Mineral Reserve metal grades presented in Table 1-2. The QP further notes that the commodity prices are detailed in Table 19-1, the metal recoveries in Table 22-6, and the metal payabilities in Table 22-1.

(2) Cash cost and cash cost per tonne of ore processed; all-in sustaining costs and all-in sustaining cost per gold equivalent ounce on a co-product basis are non-GAAP financial measures or ratios and have no standardised meaning under IFRS Accounting Standards (IFRS) and may not be comparable to similar measures used by other issuers. Refer to the “Non-GAAP Financial Measures” in Item 2.8 of this Report for more information, including a detailed description of each of these measures.

(3) Offsite costs include concentrate sales costs, including freight, treatment and refining charges.

Table 22-5: Post-Tax Net Present Value at Different Discount Rates

Post-tax	Unit	Value
NPV @ 5%	(USD million)	1,585
NPV @ 8%	(USD million)	1,372
NPV @ 10%	(USD million)	1,253

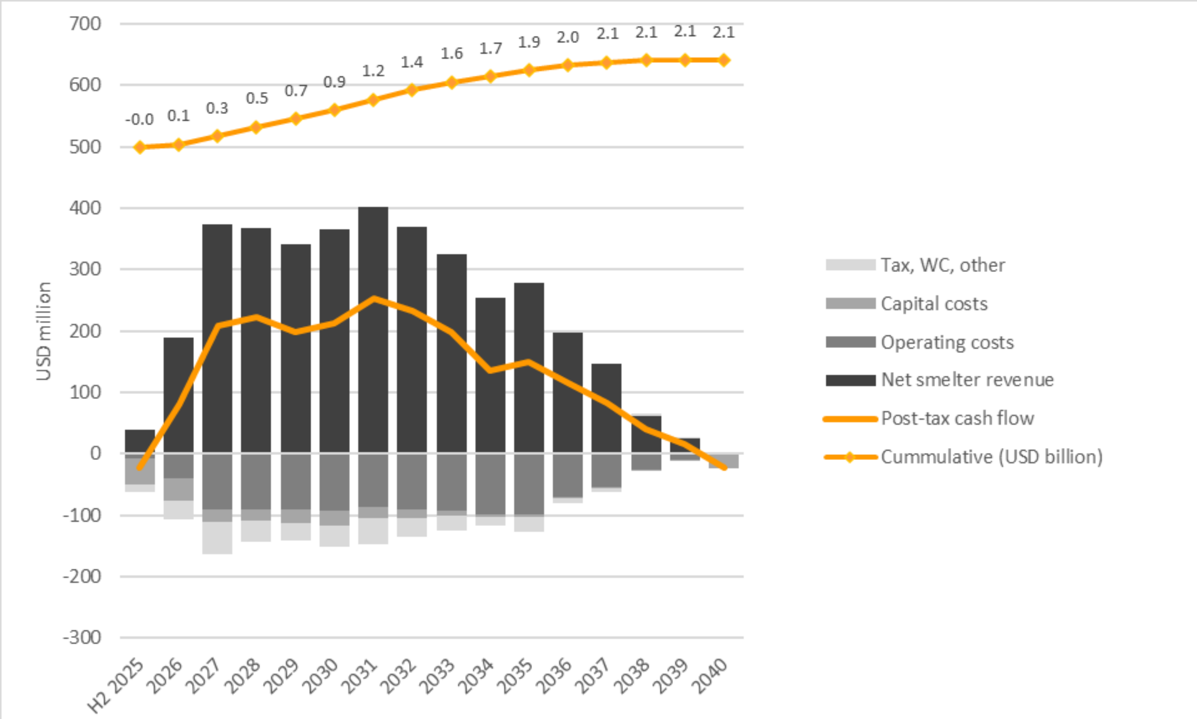


Figure 22-1: Undiscounted Post-Tax Cash Flow (excluding financing)

Table 22-6: Vareš Mine Production (Mining and Processing)

Year	Unit	Total	P2025*	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039
Ore Tonnage	(kt)	**9,459**	77	405	850	850	851	850	851	850	851	851	851	602	462	185	74
Ore Grade																	
Zn	(%)	**6.80**	7.34	7.15	6.83	6.80	6.25	7.30	8.05	7.69	6.52	5.90	6.29	6.27	6.69	6.10	6.41
Pb	(%)	**4.34**	4.39	4.08	4.05	4.35	3.82	4.64	5.27	5.12	4.67	3.74	4.07	3.98	4.11	3.92	4.07
Cu	(%)	**0.57**	0.64	0.58	0.54	0.60	0.53	0.64	0.84	0.74	0.67	0.38	0.45	0.44	0.41	0.43	0.41
Au	(g/t)	**1.72**	3.16	2.19	2.04	2.03	2.06	1.90	2.11	1.92	1.50	1.12	1.31	1.18	1.07	1.25	1.18
Ag	(g/t)	**228**	271	230	238	247	254	263	281	244	235	177	182	187	169	201	207
Sb	(%)	**0.18**	0.15	0.21	0.28	0.22	0.27	0.19	0.22	0.19	0.15	0.12	0.13	0.14	0.10	0.10	0.09
Metal Recoveries																	
Zn	(%)	**90.8**	91.1	90.9	90.8	90.8	90.7	90.9	91.0	91.0	90.8	90.6	90.7	90.7	90.8	90.7	90.7
Pb	(%)	**92.6**	93.2	92.5	92.4	92.6	92.2	92.7	93.1	93.0	92.8	92.2	92.4	92.4	92.5	92.3	92.4
Cu	(%)	**94.8**	94.2	94.7	95.1	94.7	95.1	94.6	93.9	94.3	94.5	95.7	95.4	95.4	95.5	95.6	95.6
Au	(%)	**62.7**	70.6	65.6	64.3	63.9	64.1	63.4	64.4	63.4	61.1	58.1	59.6	58.7	57.8	59.1	58.5
Ag	(%)	**89.5**	90.5	89.7	89.6	89.7	89.8	89.9	90.1	89.7	89.6	88.7	88.7	88.9	88.6	89.0	89.1
Sb	(%)	**93.9**	93.0	94.3	95.2	94.4	94.9	93.8	94.3	93.8	93.1	92.2	92.5	92.8	91.9	91.6	91.3
Product																	
Zn Con	(kt)	**896**	7.8	40.2	80.8	80.3	73.8	86.3	94.4	90.7	77.2	70.1	74.6	54.0	43.0	15.8	6.7
Pb Con	(kt)	**781**	6.3	31.6	66.3	70.2	63.0	74.2	82.0	80.5	74.5	62.2	66.6	47.5	36.4	14.1	5.8
Recovered metal																	
Zn	(kt)	**584**	5.1	26.3	52.7	52.4	47.9	56.4	62.0	59.5	50.3	45.5	48.5	35.1	28.1	10.2	4.3
Pb	(kt)	**381**	3.1	15.3	31.8	34.2	29.8	36.6	41.5	40.5	36.8	29.3	31.9	22.7	17.6	6.7	2.8
Cu	(kt)	**51**	0.5	2.2	4.4	4.8	4.2	5.1	6.7	5.9	5.4	3.1	3.6	2.6	1.8	0.8	0.3
Au	(koz)	**327**	5.5	18.7	35.8	35.3	35.9	32.9	37.0	33.3	25.0	17.7	21.2	13.8	9.2	4.4	1.6
Ag	(Moz)	**62**	0.60	2.68	5.83	6.04	6.22	6.47	6.89	5.99	5.75	4.28	4.41	3.31	2.23	1.06	0.44
Sb	(t)	**16,357**	106	788	2,238	1,790	2,140	1,491	1,742	1,487	1,207	915	987	801	441	165	61
Au Eq	(koz)	**2,375**	24	100	213	224	219	239	267	244	216	167	181	130	95	40	16
Payable Metal																	
Zn	(kt)	**440**	3.9	20.1	39.9	39.4	36.4	42.4	46.4	45.0	37.7	34.2	36.4	26.3	21.0	7.7	3.2
Pb	(kt)	**331**	2.8	13.2	27.6	29.7	25.7	31.9	36.6	35.6	32.2	25.3	27.7	19.7	15.2	5.8	2.4
Cu	(kt)	**10**	0.1	0.5	0.9	1.0	0.9	1.1	1.4	1.2	1.1	0.6	0.7	0.5	0.4	0.2	0.1
Au	(koz)	**243**	4.6	14.8	27.8	27.1	28.0	24.7	28.0	24.7	17.7	11.7	14.7	9.2	5.8	3.0	1.1
Ag	(Moz)	**56**	0.5	2.4	5.2	5.4	5.6	5.8	6.2	5.4	5.2	3.8	3.9	3.0	2.0	1.0	0.4
Sb	(t)	**1,920**	6	133	458	325	494	167	191	100	-	-	-	42	3	-	-
Au Eq	(koz)	**1,811**	19	78	164	171	170	183	202	185	163	127	137	98	72	30	12

Table 22-7: Vareš Mine Cash Flow

Year	Unit	Total	P2025*	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040
Net Smelter Revenue	(USDm)	**3,696**	40	190	373	366	339	365	402	367	322	248	268	193	139	59	24	-
Operating Costs	(USDm)	**1,050**	8	41	91	92	92	94	88	91	93	99	100	72	55	25	10	-
Initial Capital	(USDm)	**76**	41	35	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Sustaining Capital	(USDm)	**167**	0	0	22	18	23	24	18	15	8	6	4	2	1	1	0	24
Tax, WC, other	(USDm)	**332**	14	31	51	34	27	35	42	31	25	12	23	8	6	-3	-1	-2
Post-tax cash flow	**(USDm)**	**2,071**	-23	82	209	222	197	211	253	230	195	132	141	111	78	37	16	-22

* P2025: partial year, 9 months starting 1 April.

22.15 Sensitivity Analysis

A sensitivity analysis was conducted on the post-tax NPV of the project using the following variables: metals prices, head grade, metal recoveries, operating cost, initial capital cost, and discount rate. Post-tax sensitivity results are shown in Table 22-7. The analysis revealed that the economic analysis is most sensitive to changes in revenues (metal prices, head grade, and metal recoveries) and less sensitive to changes in costs (operating cost and initial capital cost).

Table 22-8 Sensitivity Analysis

Metal prices (All)						
Change	(%)	(10%)	(5%)	–	5%	10%
Metal price (Ag Eq.)	(USD/oz)	24.9	26.3	27.7	29.1	30.5
Post-tax NPV(5%)	(USDm)	1,308	1,447	1,585	1,724	1,862
Milled grade						
Change	(%)	(10.0%)	(5.0%)	–	5.0%	10.0%
Ag Eq	(g/t)	660	697	733	770	807
Post-tax NPV(5%)	(USDm)	1,314	1,449	1,585	1,722	1,859
Metal recovered						
Change	(%)	(10.0%)	(5.0%)	–	5.0%	10.0%
Metal recovery	(%)	76.9%	81.2%	85.5%	89.7%	94.0%
Post-tax NPV(5%)	(USDm)	1,312	1,449	1,585	1,722	1,858
Operating costs						
Change	(%)	10%	5%	–	(5%)	(10%)
Operating costs	(USD/t)	120	114	109	103	98
Post-tax NPV(5%)	(USDm)	1,516	1,551	1,585	1,620	1,655
Initial capital						
Change	(%)	10%	5%	–	(5%)	(10%)
Initial capital	(USDm)	84	80	76	72	68
Post-tax NPV(5%)	(USDm)	1,578	1,581	1,585	1,589	1,593

ITEM 23. ADJACENT PROPERTIES

There are no adjacent properties, at operational, developmental or exploration stage deemed to be relevant to the Vareš Mine.

ITEM 24. OTHER RELEVANT DATA AND INFORMATION

24.1 Workforce Considerations

The Vareš Mine has been mostly constructed and operational, though not at full production. ADT has a current workforce, its current make-up (local versus expatriate) was not provided to the QP, and DPM plans to review this as part of its Integration Plan.

ITEM 25. INTERPRETATION AND CONCLUSIONS

The QPs note the following interpretations and conclusions in their respective areas of expertise, based on a review of the data available for the Technical Report.

25.1 Mineral Tenure, Surface Rights, Royalties and Agreements

The QPs understand the necessary mineral rights and mining approvals have been obtained for the operation and that DPM will hold a 100% interest in its concession agreements and licences.

Independent legal opinion was not available to confirm whether the concessions and licences are in good standing with the responsible authorities, and that the necessary surface rights are in place for the Vareš Mine.

A mining royalty is due to Bosnia of BAM 3.9/t RoM. Volatility in foreign exchange rates used in the financial model are not deemed to have a material impact on the Mineral Asset economics.

25.2 Drilling and Analytical Data

Data supporting the Mineral Resource comes from comprehensive diamond drilling coverage with a robust approach to sampling, assaying, density determination and logging. The ADT geology team has a comprehensive logging and sampling facility and associated equipment to provide meaningful input to the mine planning team and the processing team.

ADT provides a detailed assessment of the QAQC data which supports their drilling data collected since 2017; earlier historical data has been adopted with some confidence given that almost all of the historical drill sites have been found and resurveyed and some of the historical drillholes were twinned and the new data agreed well with the old data.

25.3 Geology and Mineral Resource

The geology of the deposit and the style of mineralisation are very well understood.

The block model used for Mineral Resource estimation and mine planning is fit for purpose in the QP's opinion. There are a few recommendations to consider regarding high grade blocks whose grade values exceed 100% - the QP has checked the impact and determined that overall the change to the average grades is negligible, however there is a risk that the highest grade stopes will be slightly overestimated.

There is an opportunity to implement density weighting in the grade estimation method, this has the possibility of correctly increasing metal in high grade stopes and will likely more than correct for the above adjustment.

The QP's main adjustment has been to the MRE reporting which now uses a cut-off value which reflects current operating costs and current net revenues using a net smelter return value; however this has resulted in a smaller proportion of the block model reporting to the Mineral Resource statement compared with previous MRE statements issued by ADT.

There is extensive exploration ground covering most of a 25 km stretch of the same fold belt that contains Rupice. A number of drill-ready targets have already been identified and ADT has a dedicated team currently following up on these.

The Rupice deposit itself is open to the northwest at depth, the model currently terminates at the concession boundary. ADT was considering applying for an exploration permit in the adjacent area to test this extension opportunity, however, the ground is in a different municipality which presents challenges as described in Item 20.2.4.

25.4 Mining Plan

The mining plan is the result of reasonable technical work undertaken to prepare mine development and stoping designs, and a mine life development and production schedule. Both design and schedule were prepared using a manual approach and with limited underlying data. The QP ran various checks to validate the mining inventory and the production schedule, including construction of a check schedule. The QP's verification review revealed a number of areas where the state of the contributing technical work is at PFS level which satisfies the standard required for the declaration of a Mineral Reserve.

Consequently, the QP considers DPM's work is sufficient to be used to estimate a Mineral Reserve for Rupice and that DPM's production plan is reasonably achievable.

Given the PFS level of certain parts of technical work, including the capital and operating cost estimation, and the state of operations not yet being fully commissioned or operating at steady-state, contingency allowances have been added to the financial model to compensate for some of the remaining level of uncertainty that remains in the mining operation.

Furthermore, gaps in the hydrogeological understanding also present a risk to mine production and project costs, if dewatering inflows exceed currently planned capacity, with limited controls currently in place e.g. cover drilling.

25.5 Metallurgical Testwork and Processing

The testwork with regard to comminution and flotation is of sufficient breadth and depth to inform a Feasibility Study level of project definition, leading into detailed design and construction. However other aspects, notably dewatering (thickening and filtration) testwork has been conducted on only one sample in each case (i.e. both concentrates and the flotation tailings) – this represents a risk to the robustness of the ensuing plant design and operation.

The available historical production data shows that the plant has not achieved its design production rate. While the monthly reports issued by ADT list the tonnes processed, they do not show operating hours, and so it has not been possible to assess whether the plant has been achieving its design instantaneous capacity when it has been running – a lack of available ore is understood to have resulted in a significant shortfall in operating time for the plant to date.

Regarding the metallurgical performance, the results (both grade and recovery) for Ag are in line with, if not slightly ahead of, the expected performance based on the regression equations developed from the testwork. However the results for Pb and Zn (both grade and recovery) to date have fallen short of the expected performance.

Overall, the plant appears to have been built in accord with the design as described in the DFS report, which itself was soundly based on the testwork. The fact that the tailings filter appears to be undersized as built is probably not unrelated to the fact that only a very limited amount of testwork was undertaken on thickening and filtration.

25.6 Tailings Management

The Temporary TSF, located adjacent to the processing site, has been used for short-term tailings storage but exhibits significant stability concerns, including active slope failure, tension in the HDPE liner, and risks to public safety and community relations. Immediate recommendations include halting further tailings placement, isolating the area, and initiating an investigation to address these deficiencies.

With regards to tailings storage and management for the LoM, while the Veovaca TSF design is at a PFS-study level, is broadly reasonable and meets storage capacity requirements, addressing the identified technical risks and implementing the recommended measures will be critical to ensuring the facility's long-term safety, stability, and environmental compliance.

Additional contingencies for capital costs, sustaining capital costs and operating costs are proposed to address costs associated with these requirements.

25.7 Surface Water Management

There is a weak understanding of the hydrogeology and its impact on the mine design and mine plan. The mine dewatering system is highly constrained by the water treatment plant capacity. The water treatment plant has been operating at/near its maximum capacity throughout commissioning and operations and has been observed to be a constraint to dewatering and mining operations at times.

A higher than predicted groundwater inflow rate would impact the production rates assumed in the life of mine plan. A sudden inrush event would pose a safety risk, could materially impact the mining production rates assumed in the life of mine plan, and require significant remediation measures.

Surface run-off from disturbed areas of the mine site that does not come into contact with the ore stockpiles, waste dumps or paste backfill plant is considered ‘non-contact’ and is diverted and discharged from the site without treatment. Best-practice is to divert runoff from any disturbed ground associated with the mine to a suitably designed sediment pond. DPM has indicated that it intends considering all site water as contact water. However, this is yet to be developed and incorporated into an update water management plan

Both higher groundwater in-flows and sudden inrush would have a cost impact. The expansion of the water treatment plant and sediment management infrastructure at the mine site will require additional capital, and an estimate is included the current economic analysis.

25.8 Infrastructure and Logistics

Current production confirms that sufficient surface infrastructure and facilities are in place to facilitate this production; however, already there are aspects that are proving to require further work to ensure full serviceability such as the earthworks which support the haul and haul road, the drainage systems at the Rupice site, some sections of the mainline railway, and the capacity of some aspects of the site electrical distribution systems. The data provided, and time frame allowed, for review had not been sufficient to fully understand these issues and DPM must plan to undertake investigations and enquires to identify requirements and be prepared to invest additional capital expenditure to correct any deficiencies.

The current site wide water balance is limited in its scope and ability to accurately predict future water supply and requirements. This places the project at increased risk, under certain climatic conditions, of water shortage that may exceed the current water supply capacity. The cost assumptions for water supply used in the current reserve estimation may therefore be underestimated.

The WTP was sized for the expected metals flux from the RoM and WRD over the life of the mine at the time of the DFS. However, more above ground waste storage is planned which will increase the metals flux beyond that which was assumed in the DFS. Furthermore, the WTP has already been operating near its maximum capacity throughout commissioning and operations and has been observed to be a constraint to dewatering operations at times. Additional WTP capacity is required beyond the plan outlined in the DFS, taking into account an increased flux from more above ground waste storage and informed by a more robust water balance, that incorporates aspects like climate change.

Surface run-off from disturbed areas of the mine site that does not come into contact with the ore stockpiles, waste dumps or paste backfill plant is considered ‘non-contact’ and is diverted and discharged from the site without treatment. The current surface water management approach could lead to poor downstream water quality with regards to suspended solids. Additional sediment management infrastructure is required at the mine site.

25.9 Environmental, Permitting and Social Considerations

The operation has been subject to several environmental and social assessments during project development. The EIA reports prepared to inform regulatory permitting processes were not provided for review. While the original project financing documentation (2022 ESIA) reports to be aligned with good international industry practice (defined as IFC Performance Standards and EBRD Performance Requirements), it is not clear whether this level of rigour has been extended through more recent changes to the project design, permitting and retained during the implementation phase.

Although the operator reports it has the necessary approvals, insufficient information has been provided for this review to confirm the status of permitting and compliance with approval conditions. Risks remain with regards to maintaining approvals and obtaining outstanding permissions for waste rock and tailings storage to support the LoM plan.

Based on a review of ESG Factors that could be Modifying Factors when reporting Ore Reserves and which may influence the determination of economic extraction, several issues have been identified that have the potential to interrupt operations, delay the ramp up schedule or result in additional capital or operating costs. These factors relate to permitting, environmental and social management, stakeholder engagement, and operational water and waste management, climate change and closure. These are presented as qualitative risks rather than adjustments to the LoM plan or financial model.

25.10 Markets and Contracts

ADT secured off-take agreements for 100% of silver-lead concentrate and over 90% of zinc concentrate production for the first 2-3 years of operations. Concentrate deliveries have already commenced, with further sales agreements recently established.

The customers are well-known smelting and trading companies. Terms are representative of the general market for long-term concentrate sales with smelters and traders. Based on DPM's understanding of the silver-lead concentrates market and the zinc concentrates market, it is expected that the contracts can be extended at the same, or better, terms and conditions.

Commodity price forecasts are based on Bloomberg's analyst consensus metal price forecast. The QP notes that the long-term price for gold is USD 2,200/oz, which is a step change increase that has taken place over the last six months. The QP notes that this aligns with an independent consensus market forecast source.

25.11 Cost Estimates

Initial capital costs amounting to USD 76 million and sustaining capital costs amounting to USD 143 million have been projected (excluding USD 24 million as a closure cost allowance), along with life of mine cash operating costs totalling USD 1,050 million.

25.12 Economic Analysis

The economic analysis undertaken results in a positive NPV of USD 1,596 million at a discount rate of 5%.

25.13 Mineral Resource and Mineral Reserve Estimates

The QP considers the Mineral Resource model to be robust despite making a few recommendations for improvement. However, the cut-off grade strategy used by ADT in previous reporting were modified by the QP to more closely reflect current technical-economical parameters.

The QP considers the Mineral Reserve to be supported by actual information and sufficient technical study to constitute PFS level of work.

25.14 Risks

Following the QP's review, risks perceived as high or medium are highlighted and presented in Table 25-1 and Table 25-2. The QP discusses the impact and/or mitigation plans to address these. No critical risks have been identified.

At the time of the Technical Report, DPM's development of the Integration Plan is ongoing. The QP is unable to assess the risk associated with the change of management from ADT to DPM. This is deemed to be a short-term impact, and presents as many opportunities as it does risks.

In addition to the risks that were identified, the QP highlights the limitations and restrictions in data provided, see Table 12-1 (Data Not Provided), and unknowns that may result.

Table 25-1: Perceived High Risks Associated with the Mineral Asset

High Risk	Mitigation
Permitting of paste backfill plant Risk: ▪ Permit not granted for the desired location (construction has commenced) Consequence: ▪ Change of location, impacting reticulation logistics, extended time delay, increase i operating costs, impact on NPV (low to moderate)	A plan to address a change in location will only take place once the permit is rejected. The time delay, including reapplication, remains the key consequence. Production can continue by adapting the schedule to extract more ore from primary ore stopes, for a limited period, resulting in a reduced rate. The risk of increased instability if exposure time are exceeded will be managed, eg, using cemented aggregate.
Water treatment and storage Risk: ▪ Delay in increasing capacity of water treatment plant and water lagoon Consequence: ▪ Reduced mining rate due to constrained mine dewatering ▪ Reduced mining rate resulting from delay until increasing water management capacity (storage and treatment), including permitting, construction, implementation	ADT has commenced addressing this issue, however SRK has no information in relation to this. DPM has identified this risk as a priority to be addressed.
Haul road (25 km surface haul road) Risk: ▪ Road in very poor condition at times, potential slope failure Consequence: ▪ Interrupted haulage and production for some days, and safety to personnel and vehicles	DPM has identified this risk as a priority requiring action, with plans to invest in the maintenance and improvement of the haul road in conjunction with the municipality.
Temporary TSF Risk: ▪ Complexity and time needed to remove the material from Temporary TSF to Veovaca TSF. The QP has not seen the remediation plan. Consequence: ▪ Safety to personnel and equipment ▪ Relationships with communities and authorities ▪ Reputation	DPM has identified this as a high priority action to move the tails to either Veovaca TSF or backfill paste plant commissioned

Table 25-2: Perceived Medium Risks Associated with the Mineral Asset

Medium Risk	Mitigation
Permitting of paste backfill plant Risk: ▪ Permit not granted at scheduled time Consequence: ▪ Delay to start-up of paste backfilling, delaying ramp up to 850 ktpa	N/A
Permitting of access road and return water pipeline to Veovaca TSF Risk: ▪ Permit not granted prior to expiry of community agreement Consequence: ▪ Interruption to haulage of tailings material between VPP and Veovaca TSF until permit is granted and facilities constructed	DPM recognises the permitting risks with plans to proactive in engaging with and developing a strong relationship with authorities.
Underground rock conditions Risk: ▪ Instability of development and stopes in poor ground conditions. Consequence: ▪ Loss of ore, reduced ore grade	Implement data collection, interpretation, analysis and monitoring programmes to predict and manage ground conditions.
Underground water Risk: ▪ Sudden inrush if mining connects with a karst system Consequence: ▪ Significant mine flooding, interruption to mining to an extended period, potential loss of some mining area. ▪ Potential risk to equipment and personnel. ▪ Revenue and cost impact. Potentially significant if WTP requires upgrading.	Immediate: Cover drilling during development Short to medium term: further hydrogeological characterisation of the deposit and surrounding areas to the full planned depth of mining
Sustaining target mining rate Risk: ▪ Unable to sustain target rate due to complex mining sequence or unexpected constraints. Consequence: ▪ Reduced production, increased costs for mitigation (low to medium likelihood, however significant impact)	Prepare detailed schedule to FS level to ensure flexibility that can cope with unexpected conditions.
Change of mining method Risk: ▪ Support systems (ventilation, pastefill, dewatering) inadequate for new methods, schedule Consequence: ▪ Increased costs	DPM to undertake targeted studies to collect and interpret geotechnical data, to inform the new mining method and schedule
Change of mining method Risk: ▪ Unfamiliarity with new methods, esp. MCAF Consequence: ▪ Higher costs, lower production, disrupted schedule, safety considerations with entry method	Prepare detailed implementation plan including training, benchmarking, site visits

Veovaca TSF Risk: ▪ Placement of out-of-specification tailings (saturated/ weak/ sensitive/ contractive) placed in the bowl behind the starter dam resulting in slope stability failure of the overlying filter cake tailings slope. Consequence: ▪ Costs to remediate; reputational damage	It is recommended that prior to raising the tailings slope the bowl area must be remediated. Follow the recommendations made to address the identified technical risk (Section 18).
Veovaca TSF Risk: ▪ Inadequate contact water drainage provision in the toe/starter dam area resulting in slope stability failure of the filter cake tailings slope and/or overtopping of the lined starter dam resulting from. Impact: ▪ Costs to remediate; reputational damage	Facilitate easier management of tailings contact water at the planar basal liner/starter dam interface where an upstream open ditch and series of sumps with piped off-takes to the clarification pond could be established. Follow the recommendations made to address the identified technical risks (Section 18).
Veovaca TSF Risk: ▪ Tension in the HDPE geomembrane induced by settlement and consolidation of tailings resulting in side slope lining system integrity failure. Impact: ▪ Contamination by contact water seepage to the ground; costs to remediate; reputational damage	It is recommended that measures are undertaken to minimise potential for lining system failures to occur. Follow the recommendations made to address the identified technical risks (Section 18)
Veovaca TSF Risk: ▪ Out-of-specification tailings placed at lower density and/or necessitating reduction in tailings slope inclination for safety. Impact: ▪ Storage capacity is insufficient; costs to develop additional tailings storage areas	Developing a robust tipping, placement and compaction procedure (sometimes referred to as ‘tipping rules’). Follow the recommendations made to address the identified technical risks (Section 18)
Waste rock management strategy Risk: ▪ Absence of design (design criteria, footprint, schedule) ▪ Permitting delay for additional waste rock storage ▪ Lack of design for PAG storage Consequence: ▪ Interruption to operations ▪ Insufficient environmental controls for storage of PAG material leading to potential environmental contamination	Develop a waste management strategy that aligns geochemical testwork of waste lithologies with revised LoM plan and confirm locations and appropriate methods of storage to prevent environmental contamination. Follow the recommendations made to address the identified technical risks
Stakeholder relations Risk: ▪ Escalation of stakeholder issues that results in deterioration of relationships Consequence: ▪ Interruptions to operations, the maintenance and acquisition of licences and permits, and reputational damage	Develop a stakeholder engagement plan for transition period and beyond, with consideration of specific stakeholder groups

25.15 Opportunities

Following SRK's review, the following opportunities are noted.

Opportunity Summary	
Production schedule	Some schedule-critical rate inputs could be conservative. Improving on these can de-risk the schedule.
Mineral Resource	Improve geological continuity in the up-dip portion of the Rupice Northwest zone by modelling as a fold, this may present a more coherent stoping target
Mineral Resource	Improve density estimation formula to include iron – this may add a little metal into the existing estimate
Mineral Resource	Incorporate density weighting in the grade estimation method, this will likely increase metal in the high grade stopes
Exploration	The primary opportunity is to extend the Rupice Northwest deposit where it is open at depth towards the northwest although this will require successful permitting in a new municipality
Exploration	Continue working on the many exploration areas on ADT ground along the belt; many of these are attractive targets in the QP's opinion

ITEM 26. RECOMMENDATIONS

In support of DPM progressing with its Integration Plan, the QPs makes a number of recommendations.

26.1 Mineral Resource and Exploration

Wireframing

The wireframing used for grade estimation domains is fit for purpose, however a more 3D approach is likely to fine-tune some of the geometry and improve continuity, particularly in Rupice Northwest up-dip area.

Consider simplifying the wireframing effort which currently aims to provide a set of domains for each metal to be estimated. A more comprehensive assessment of metal distribution may demonstrate that some metals are sufficiently well correlated to be able to share grade estimation domains; this would a reduce the number of domain wireframes required without compromising the integrity of the estimation.

Mineralogy and Density Estimation

Although this is not a significant concern in the orebody, core quality can bias the sample selection process in the surrounding waste rocks; generally speaking, whole-box weighing of core before cutting is a simple means by which to estimate density more robustly.

Given the high sulphur content in this orebody, density is as important to quantify and estimate as grade. The QP used the assay data to check the density values with some first-pass mass balance equations. If the merits of this approach were to be studied further, then the recommended next step would be to use the petrographic equipment on site to conventionally identify and quantify mineral species present in some 50-100 of the samples previously selected for density determinations. Further electron microprobe work would be necessary to confirm some of the element ratios in some of the minerals. This would allow more robust mass balances to be completed, possibly with assistance from machine learning, ultimately providing block by block estimates of mineralogical proportions from which density can be estimated very robustly and incorporating other attributes such as grain size and intergrowth, potentially the determination of different geometallurgical ore types.

The grade estimation method should be modified to incorporate density as an additional weighting factor; this approach is theoretically more correct and will likely add metal into the higher grade parts of the deposit.

Exploration

ADT has compiled historical data, generated new data, identified several attractive exploration areas and assembled a dedicated exploration team with a USD 5 million budget for 2025. In the QP's opinion the budget has been realistically built up and suitably apportioned to the key exploration targets.

the QP's recommendation is to undertake additional data analysis to determine which of the remote sensing methods are most successful at detecting this style of mineralisation at depth and then initiating a belt-wide air-flown remote sensing effort to achieve a complete and uniform coverage. This will be important in the medium term to ensure a complete assessment of the belt and to ensure well balanced prioritisation of work on current known targets and some potential new targets to take full advantage of the prospectivity on the concessions.

26.2 Geotechnics

The rock mass conditions at the mine have provided challenges with regards development advance, rock support and stoping performance and behaviour. Observations during the site visit indicated that the site team is very experienced and many of the geotechnical challenges are in the process of being overcome. The QP recommend that:

- Detailed assessment of the rock mass conditions by domains separating the deposit areas and also by depth is required to assess the expected rock quality and not combining all data for statistical averages;
- In order to manage the ground conditions going forward the operation will need to ensure that geotechnical and structural models are developed and regularly updated;
- Televiewer logging is recommended in some of the drilling to revise the understanding of fracturing and joint sets;
- The regular lidar drone scanning and 'rate-of-change' type assessment should be rigorously applied in all stopes, to increase performance knowledge; and
- The locations of the various mining methods are to be independently assessed for stope and support design. This optimises the technical assessment to improve stability and reduce dilution, as well as ensure worker safety in the entry MCAF method.

The impact of this work is of a technical nature rather than a significant cost. The revised mining costs already take geotechnical recommendations into account.

26.3 Hydrogeology

Before the mine progresses into new areas which have not been well characterised, additional hydrogeological characterisation (drilling and testwork) of the Rupice deposit and surrounding area is required in order to:

- More reliably define long-term mine inflows;
- Further investigate the risk of sudden groundwater inflows;
- Define long-term mine inflows and risk of sudden inrush; and
- Further investigate risk of drawdown impacts to the south and communities reliant on groundwater and spring flow for water supply in the Bukovica catchment.

New hydrogeological data should be used to inform:

- Updated conceptual and hydrogeological modelling of the mine to address the above three risks.
- An inrush risk assessment and hazard map, with additional inrush controls developed if required.

Implement cover drilling routines when developing into new areas, to help manage the risk of sudden inflows.

The impact of this work is of a technical nature rather than a significant cost.

26.4 Geochemistry

The mined material contains sulphides and could be partially classified as potentially acid-forming (PAG) if exposed to atmospheric conditions leading to leaching of metals and sulphides.

Existing characterisation and management of the PAG material in the Rupice Main area should be aligned for the revised LoM plan. Additional work is recommended to characterise the mined material from RNW to develop sufficient actions to determine quantities and inform waste management planning.

Based on the characterisation and quantification of the acid forming potential, sufficient location and storage facilities can be designed to prevent the acid generation and manage the run-off appropriately. This applies to all material storage locations sucks as RoM pad, ore and waste stockpiles as well as any temporary rock stockpiling locations for PAG material. Existing work and documentation regarding the current status of the geochemical characterisation and waste management practices are described in Section 20.2.1.

The outcome of such work will may have an impact on costs, however this can only be assessed upon progressed characterisation studies.

26.5 Mining

A number of items contributing to DPM’s mine plan are based on inputs at a PFS level of confidence. These should all be progressed to the FS level of confidence to ensure they are suitable for DPM’s mine plan and to de-risk the prospects of achieving the mine production schedule. These include:

- Mine plans to include a full mine development design containing all capital and operating tunnel development for increased detail to support the FS cost estimation and further work to refine the mining sequence and production strategy. Current development is horizontal. This should be modified to provide the appropriate drainage for water shedding.
- The mine production schedule is recommended to include a full equipment level of detail to enhance the accuracy and transparency of the mine plan as well as for further optimisation and de-risking of the mine production.
- The ventilation plan should be updated to FS level by combining both mining areas into a full 3D mine ventilation model to support the mine production schedule as well as cost estimation.
- Backfill plan should be progressed to the feasibility level by complementing the current information with optimisation of the backfill recipe, incorporating the mass balance of the mine site in greater detail to the LoM plan, and including a full paste backfill and underground reticulation engineering study for the RNW.
- Waste rock dump design and scheduling should be analysed in accordance with the changed mining sequence to bottom-to-top, as well as to de-risk the plan by further studying the effects of the backfill strategy on the required waste storage capacity underground and surface. PAG and NAG potential of the waste should be confirmed for the RNW area and appropriate waste management strategies developed.

The impact of this work is of a technical nature rather than a significant cost, as it can be undertaken by DPM mining engineers as part of mine planning work.

26.6 Process

The QP has no recommendations. The performance of the process plant will be better understood once steady state production is achieved.

26.7 Tailings Management – Temporary TSF

The immediate recommendations include halting further tailings placement, isolating the area, and initiating an investigation to address the deficiencies detailed in Item 18 of this Technical Report. The cost of this remediation has been included in the economic analysis.

26.8 Tailings Management – Veovaca TSF

Complete the recommendations made by WA for their TSF design, specifically including:

- Confirmation of HDPE liner and geosynthetic drainage layer properties (e.g. friction angle) through testing,
- Conduct additional tailings material testing to verify geotechnical properties over the mine life,
- Install sediment traps downstream to protect sensitive receptors.
- Develop a monitoring instrument plan with piezometers upstream and downstream.

Complete the recommendations made in this report to address the identified technical risks, specifically including:

- **Tailings slope foundation remediation/mitigation** - Prior to raising the tailings slope above it, the topographic bowl area behind the starter dam must be remediated. This may include; 1) development of a temporary tailings stacking area in the base of the mine void; 2) excavation of tailings from the bowl and re-placement of them in the temporary stacking area; 3) placement and compaction of engineered fill in the bowl; 4) re-establishing the basal liner over the filled bowl; 5) engineering of additional drains to facilitate transfer of contact water to the downstream seepage pond; 6) continued further development of the TSF in line with the broad PFS plan.
- **Contact water management reappraisal and redesign** - The recommendations made in the previous paragraphs to place engineered fill and line over the bowl will facilitate easier management of tailings contact water at the planar basal liner/starter dam interface where an upstream open ditch and series of sumps with piped off-takes to the clarification pond could be established. By leaving a gap between starter dam upstream slope and the toe of the filtered tailings slope there will be potential if necessary to access and clean out both the trench and sumps to ensure continuity of drainage in all circumstances. This contrasts with the existing design where the single sump and pipe will not be accessible once tailings are placed in the bowl. It is also recommended that as part of contact water re-design, the design sizing/justification for the downstream contact water management pond should be reappraised and confirmed sufficient for all required normal and storm flows.

- **Side slope lining system shearing/tension protection** - It is recommended that measures are undertaken to minimise potential for lining system failures to occur. These may include; 1) developing specific placement and compaction requirements/ specifications for the side slope interface zone; 2) design of yielding anchor trenches with additional liner released progressively if tension is induced; and, 3) use of a sacrificial low shear strength interface above the liner such that shearing occurs down it without inducing tension in the primary liner. All of these techniques are successfully adopted in landfill engineering where magnitude of post deposition waste settlement is even higher than can be anticipated for consolidation of filter cake tailings.
- **Tailings placement and compaction tipping rules** - develop a robust tailings haulage, tipping, placement and compaction procedure (sometimes referred to as ‘tipping rules’). These tipping rules should define equipment and placement/compaction specifications including QA/QC testing requirements to demonstrate that the require densities have been achieved. As part of the tipping rules there may be separate provisions provided for different zones of the tailings waste mass. The outer slope shell tailings may have a tighter specification than the inner non-structural zone to ensure slope stability is demonstrated. This may mean that at certain times of year/seasons the tailings are predominantly placed in the non-structural zone away from the slope shell (rain; snow-melt; winter etc). As previously discussed, there may be different compaction provisions and equipment specified for the zone adjacent to the side slope lining system.
- **Non-contact water culvert reappraisal/redesign/design confirmation** - If a culvert solution is necessary for conveyance of surface water, then it should be over-engineered with appropriate contingency factors to account for risks and should be designed to allow inspection access for remote camera equipment.

The cost of this work has been included in the economic analysis, however will be better understood once the studies and designs have been updated.

26.9 Water Management

Build a fit-for-purpose site-wide water balance calibrated site-wide water balance (SWWB) for the mine and processing and TSF areas, incorporating climate change and constructed and calibrated, and calibrate to current observations. This site-wide water balance can then be used to confirm water supply (and surplus discharge/treatment) requirements under various climatic and operational scenarios.

The impact of this work is of a technical nature rather than a significant cost.

26.10 Surface Infrastructure and Logistics

Haul Road – a full scope of works should be developed to investigate causes of failure and potential for future incidents, but this should include, but not be limited to, the following:

- Undertake a full visual survey of the road and understand the location and causes of all failures to confirm the high-risk road sections.
- Conduct a geohazard survey including terrain mapping and slope mapping.
- Conduct geotechnical analysis on slopes where failures have occurred (back analysis) and reanalyse all other cutting slopes, including downslope sections where road is supported on enablement fill causing loading to the slope.

- Re-appraise drainage design for all earthwork cuttings and embankments including later drainage along the road.

Logistics:

- Interact with Railways FBiH to understand the causes and scope of the rail interruptions and work with Railways FBiH to develop actions plans and risk mitigations.

Surface Infrastructure:

- Review the earthworks and drainage design, including basis of design and modelling, to improve drainage across the Rupice site.
- Expand the water treatment plant capacity.

The cost of this work has been included in the economic analysis, however will be better understood once the studies and designs have been updated.

26.11 Environment, Permitting and Social Considerations

To address the qualitative risks to Mineral Resources and Mineral Reserves, it is recommended that DPM:

- Completes a legal due diligence to confirm status of approvals, surface rights, legal liabilities and on-going legal proceedings or claims that could pose a threat to the maintenance of mineral rights, surface rights, permits and approvals for the operation, or result in material fines and penalties.
- Prepares a permitting strategy to align permits and conditions of approval with revised LoM plan, and timeline for obtaining permits required to implement the LoM plan (for example waste storage and Phase 2 Veovaca TSF).
- Considers conducting additional hydrogeological test work to increase confidence in the lack of connection between the mine and the Bukovica water supply source.
- Defines opportunities for soil erosion control and wastewater treatment to improve discharge water quality, particularly for suspended sediments.
- Develops a waste management strategy that aligns geochemical testwork of waste lithologies with revised LoM plan to define expected quantities of non acid-generating and potentially acid-generating lithologies and confirm locations and appropriate methods of storage to prevent environmental contamination.
- Develops a stakeholder engagement plan for transition period and beyond, with specific consideration of stakeholders at a municipality level and those located close to the haul road, VPP and Veovaca TSF.
- Conducts local content planning, increasing local employment and procurement, and skills analysis and training.
- Updates closure plan and conceptual cost estimate to align with revised LoM plan.
- Defines impact of impending Bosnian carbon tax on the operation, determines carbon reduction targets and develops a decarbonisation strategy with expected timeframes and capital requirements.

The impact of this work is of a legal and technical nature rather than a significant cost.

26.12 Capital and Operating Costs

The capital and operating costs associated with recommendation will be impacted, as part of normal running of the business.

ITEM 27. REFERENCES

The reference documents that SRK has had access to and reviewed include:

- “Vareš & Rupice Feasibility Study Report” prepared by Ausenco Engineering Canada Inc.(“Ausenco”) dated 23 September 2021 (the “DFS”);
- 2024 Mineral Resource Statement: “Rupice Polymetallic Deposit: Mineral Resource Update”, AMC Consultants, 7 November 2024;
- Rupice Ore Reserves (AMC Consultants Pty Ltd, 2023, December 2023);
- Rupice Polymetallic Deposit – December 2024 - Mineral Resource Update Technical Summary, 14 March 2025;
- “Structure and Mineralisation of the Base and Precious Metals Rupice Deposit”, Majoribanks, November 2018;
- Wardell Armstrong LLP (WA) design report titled “Vares Silver Project TSF Design 5.1 Mt – Relocation” (November 2024) and supplementary details from Zagrebinspekt d.o.o translated report “Supplementary Mining Project of Temporary Flotation Tailings Disposal Site at Veovača II” (August 2024), which the WA report supersedes.
- Vareš Polymetallic Mine ESIA (WAI, February 2022) and supporting environmental and social management plans (as updated);
- Permit Register 2013-2023 (ADT, 2023);
- Vareš Silver Operation corporate presentation (ADT, March 2025);
- Annual Report for the Year Ended 31 December 2024 (ADT, March 2025);
- 2024 Rupice Mineral Resource and Reserves Update (ADT, March 2025);
- Vareš Operation Monthly reports (ADT, 2024 and 2025);
- Operations Update (ADT, March 2025);
- “0401 Locked Cycle Test Summary 17.08.2020” – spreadsheet summarising LCT results from PFS testwork program;
- “Adriatic Metals Rupice, Bosnia Feasibility Study Metallurgical Testwork Report”, Wardell Armstrong International, June 2022;
- “Adriatic Metals Rupice, Preliminary Metallurgical Testwork Report for the Rupice Polymetallic Deposit”, Wardell Armstrong International, October 2019;
- “Rupice Polymetallic”, Petrolab Ltd, March 2019;
- “Adriatic Metals Plc Vareš Project Debottlenecking Scoping Study”, Ausenco Pty Ltd, October 2024;
- “Vareš IE Phase 3 DFS Due Diligence Technical Report”, Palaris Europe Limited Report, November 2021;
- “Plum site visit observations”, DPM internal memo, July 2024;
- “020201 Plum Mineral Reserves.01.07.2025.xlsx”, DPM, Mineral Reserves production schedule;
- “020201 Plum_ug_schedule.v001.14.04.2025.xlsx”, DPM, mine production schedule
- “020201 Plum Mobile Mining Equipment.17.04.2025.xlsx”, DPM, mine equipment schedule;

- "020201 Plum Mobile Mining Equipment.17.04.2025.xlsx", DPM, mine equipment schedule;
- "020201 Plum Mining OPEX breakdown_PN_nh rev 1.14.04.2025.xlsx", DPM, mining operating cost estimation;
- "020201 Plum Mining Capex.28.04.2025.xlsx", DPM, mining capital cost estimation;
- "DPM Plum Mine Design.duf", DPM, mine design project.

ITEM 28. DATE AND SIGNATURE

The date of signature of the Technical Report is 9 June 2025. On this date, the QPs signed their respective Certificates.

QUALIFIED PERSONS CERTIFICATES

Certificate of Martin Pittuck

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mpittuck@srk.co.uk

I, Martin Pittuck, do hereby certify that:

- I am Principal Consultant (Resource Geology), employed by SRK Consulting (UK) Ltd since 1996.
- This certificate applies to the technical report entitled "Amended and Restated NI 43-101 Technical Report on the Vareš Mine, Bosnia" with a report date of 9 June 2025 and an effective date of 1 April 2025 (the "Technical Report").
- I am a graduate with a Master of Science in Mineral Resources gained from Cardiff College, University of Wales in 1996 and I have practised my profession continuously since that time. Since graduating I have worked as a consultant at SRK on a wide range of mineral projects. I have undertaken many geological investigations, resource estimations, mine evaluation technical studies and due diligence reports.
- I am a member of the Institute of Materials Mining and Metallurgy (Membership Number 49186); I am a Fellow of the Geological Society and I am a Chartered Engineer;
- I have worked as a geologist for a total of over 30 years.
- I have read the definition of Qualified Person as set out in National Instrument 43-101 – Standards of Disclosure for Mineral Projects ("NI 43-101") and certify that, by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I am a Qualified Person for the purposes of NI 43-101.
- I am responsible for the preparation of Items 1.4 – 1.7, 1.9, 7 – 11, 14, 25.2, 25.3 and 26.1 of the Technical Report relating to geology and Mineral Resource estimation. as well as relevant parts in the Executive Summary, Reliance on Other Experts, Conclusions and Recommendations, Risks and Opportunities, References and Date and Signature of the Technical Report, and I accept professional responsibility for those sections of the Technical Report.
- I am independent (as defined by Section 1.5 of NI 43-101) of Dundee Precious Metals Inc and Adriatic Metals Plc. I have not had prior involvement with the property that is the subject of the Technical Report.
- I visited site on 25 to 26 March 2025.
- I have read NI 43-101 and Form 43-101F1 and the Technical Report has been prepared in compliance with that instrument and form.
- As of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed and to make the Technical Report not misleading.

Signed and dated on 9 June 2025 in Cardiff, United Kingdom.

Martin Pittuck

Certificate of Neil Marshall

SRK Consulting (UK) Ltd
5th Floor Churchill House, 17 Churchill Way, Cardiff CF10 2HH, Wales, United Kingdom
nmarshall@srk.co.uk

I, Neil Marshall, do hereby certify that:

- I am Principal Consultant (Mining Geotechnical Engineer), employed by SRK Consulting (UK) Ltd since 1998.
- This certificate applies to the technical report entitled "Amended and Restated NI 43-101 Technical Report on the Vareš Mine, Bosnia" dated 9 June 2025 (the "Technical Report").
- I am a graduate of the University of Portsmouth, UK, with an Honours degree (BSc) in Engineering Geology and Geotechnics in 1979 and an MSc (DIC) in Engineering Rock Mechanics from Imperial College, UK in 1982.
- I am Member of the Institute of Mining, Metallurgy and Materials (IOM^3) and a Chartered Engineer. My membership number is 50266.
- I have practiced my profession continuously since 1979. I have been employed by SRK Consulting since February 1998 during which time I have project managed numerous geotechnical investigation and analysis programmes for open pit and underground mining Feasibility Studies.
- I have read the definition of Qualified Person as set out in National Instrument 43-101 – Standards of Disclosure for Mineral Projects ("NI 43-101") and certify that, by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I am a Qualified Person for the purposes of NI 43-101.
- I am responsible for the preparation of Items 16.1 and 26.2 of the Technical Report relating to Geotechnical Considerations as well as relevant parts in the Executive Summary, Reliance on Other Experts, Conclusions and Recommendations, Risks and Opportunities, References and Date and Signature of the Technical Report, and I accept professional responsibility for those sections of the Technical Report.
- I am independent (as defined by Section 1.5 of NI 43-101) of Dundee Precious Metals Inc and Adriatic Metals Plc. I have not had prior involvement with the property that is the subject of the Technical Report.
- I have not visited the Vareš site however have relied upon Mr Di Giovinazzo's (named as an expert in the Technical Report) feedback and photos taken during his site visit.
- I have read NI 43-101 and Form 43-101F1 and the Technical Report has been prepared in compliance with that instrument and form.
- As of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed and to make the Technical Report not misleading.

Signed and dated on 9 June 2025 in Cardiff, United Kingdom.

Neil Marshall

Certificate of Peter Myers

SRK Consulting (UK) Ltd
5th Floor Churchill House, 17 Churchill Way, Cardiff CF10 2HH, Wales, United Kingdom
pmyers@srk.co.uk

I, Peter Myers, do hereby certify that:

- I am Principal Consultant (Mining Engineering), employed by SRK Consulting (UK) Ltd since September 2022.
- This certificate applies to the technical report entitled "Amended and Restated NI 43-101 Technical Report on the Vareš Mine, Bosnia" with a report date of 9 June 2025 and an effective date of 1 April 2025 (the "Technical Report").
- I am a professional mining engineer having graduated with a Bachelor of Engineering degree with Honours in 1980 from the University of Melbourne.
- I am a Fellow of The Australasian Institute of Mining and Metallurgy, Membership Number 105826.
- I have worked as a mining engineer for a total of 45 years, since graduation.
- I have read the definition of Qualified Person as set out in National Instrument 43-101 – Standards of Disclosure for Mineral Projects ("NI 43-101") and certify that, by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I am a Qualified Person for the purposes of NI 43-101.
- I am responsible for the preparation of Items 1.10, 16 other than 16.1, 16.2, 16.8.6 and 16.12.2 of the Technical Report relating to mining and Mineral Reserve estimation. as well as relevant parts in the Executive Summary, Reliance on Other Experts, Conclusions and Recommendations, Risks and Opportunities, References and Date and Signature of the Technical Report, and I accept professional responsibility for those sections of the Technical Report.
- I am independent (as defined by Section 1.5 of NI 43-101) of Dundee Precious Metals Inc and Adriatic Metals Plc. I have not had prior involvement with the property that is the subject of the Technical Report.
- I visited site on 25 to 26 March 2025.
- I have read NI 43-101 and Form 43-101F1 and the Technical Report has been prepared in compliance with that instrument and form.
- As of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed and to make the Technical Report not misleading.

Signed and dated on 9 June 2025 in Cardiff, United Kingdom.

Peter Myers

Certificate of John Willis

SRK Consulting (UK) Ltd
5th Floor Churchill House, 17 Churchill Way, Cardiff CF10 2HH, Wales, United Kingdom
jwillis@srk.co.uk

I, John Willis, do hereby certify that:

- I am a Principal Consultant (Mineral Processing), employed by SRK Consulting (UK) Ltd since 2008.
- This certificate applies to the technical report entitled "Amended and Restated NI 43-101 Technical Report on the Vareš Mine, Bosnia" with a report date of 9 June 2025 and an effective date of 1 April 2025 (the "Technical Report").
- I graduated with a BE in Metallurgical Engineering from the University of Queensland, Australia in 1985, and a PhD in Minerals Process Engineering from the same institution in 1994.
- I am Member and Chartered Professional of the Australasian Institute of Mining and Metallurgy (Membership Number 103635).
- I have worked as a Mineral Processing Engineer for more than 35 years since my graduation from University.
- I have prepared Items 1.8, 1.11, 13, 17, 25.5 and 26.6 of the Technical Report in the role of independent reviewer of the Project, and have contributed to relevant parts in the Executive Summary, Data Verification, Conclusions and Recommendations, Risks and Opportunities, References and Date and Signature of the Technical Report.
- I am independent (as defined by Section 1.5 of NI 43-101) of Dundee Precious Metals Inc and Adriatic Metals Plc. I have not had prior involvement with the property that is the subject of the Technical Report.
- I have not visited the Vareš site.
- I have read the definition of Qualified Person as set out in National Instrument 43-101 – Standards of Disclosure for Mineral Projects ("NI 43-101") and certify that, by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I am a Qualified Person for the purposes of NI 43-101.
- I have read NI 43-101 and Form 43-101F1 and the Technical Report has been prepared in compliance with that instrument and form.
- As of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed and to make the Technical Report not misleading.

Signed and dated on 9 June 2025 in Cardiff, United Kingdom.

John Willis

Certificate of James Bellin

SRK Consulting (UK) Ltd
5th Floor Churchill House, 17 Churchill Way, Cardiff CF10 2HH, Wales, United Kingdom
jbellin@srk.co.uk

I, James Bellin, do hereby certify that:

- I am Principal Consultant (Water), employed by SRK Consulting (UK) Ltd since 2017.
- This certificate applies to the technical report entitled "Amended and Restated NI 43-101 Technical Report on the Vareš Mine, Bosnia" with a report date of 9 June 2025 and an effective date of 1 April 2025 (the "Technical Report").
- I am a Chartered Geologist and Fellow of the Geological Society of London. I am also a Credentialled Specialist in water stewardship with the Alliance for Water Stewardship. I graduated with a Bachelor of Science degree with Honours in Environmental Geoscience in 2003 from the University of Bristol in 2003 and a Master of Science degree in Hydrogeology in 2005 from the University of Birmingham.
- I have 19 years of mining related water management experience, 13 years of which has been in consultancy and 6 years working in the mining industry. My specific areas of expertise include hydrogeological characterisation, mine dewatering, mine site surface water management, water balance modelling, water monitoring and impact assessment, and water stewardship.
- I have read the definition of Qualified Person as set out in National Instrument 43-101 – Standards of Disclosure for Mineral Projects ("NI 43-101") and certify that, by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I am a Qualified Person for the purposes of NI 43-101.
- I am responsible for the preparation of Items 16.2, 16.8.6, 16.12.2, 18.5, 18.9.2 and 20.3.4 of the Technical Report relating to hydrogeology, underground dewatering, water balance and surface water management, and water stewardship, as well as relevant parts in the Executive Summary, Reliance on Other Experts, Conclusions and Recommendations, Risks and Opportunities, References and Date and Signature of the Technical Report, and I accept professional responsibility for those sections of the Technical Report.
- I have not visited the site, however relied upon Ms Harris (named as an expert in the Technical Report) feedback and photos taken during her site visit.
- I am independent (as defined by Section 1.5 of NI 43-101) of Dundee Precious Metals Inc and Adriatic Metals Plc. I have not had prior involvement with the property that is the subject of the Technical Report.
- I have read NI 43-101 and Form 43-101F1 and the Technical Report has been prepared in compliance with that instrument and form.
- As of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed and to make the Technical Report not misleading.

Signed and dated on 9 June 2025 in Cardiff, United Kingdom.

James Bellin

Certificate of Richard Martindale

SRK Consulting (UK) Ltd
5th Floor Churchill House, 17 Churchill Way, Cardiff CF10 2HH, Wales, United Kingdom
rmartindale@srk.co.uk

I, Richard Martindale, do hereby certify that:

- I am Principal Consultant (Tailings and Geotechnical Engineering), employed by SRK Consulting (UK) Ltd since 2012.
- This certificate applies to the technical report entitled "Amended and Restated NI 43-101 Technical Report on the Vareš Mine, Bosnia" with a report date of 9 June 2025 and an effective date of 1 April 2025 (the "Technical Report").
- I am a member and a Chartered Engineer registered with the Institute of Materials, Minerals & Mining, UK. I graduated with a Bachelor of Science degree with Honours 2001 in Geology from The University of Durham and a Master of Science degree with Merit 2002 from the University of Exeter, Camborne School of Mines, in Mining Geology.
- I have worked as an Engineer for a total of 22 years post-graduation and I am experienced in consulting within the Mining, Civil Engineering and Waste Management Sectors. I specialise in; assessment and design of rock and soil slopes; numerical modelling; design and management of ground investigations, and of ground performance monitoring schemes; due diligence; and, audits of slopes and waste storage facilities, technical performance and regulatory compliance.
- I have read the definition of Qualified Person as set out in National Instrument 43-101 – Standards of Disclosure for Mineral Projects ("NI 43-101") and certify that, by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I am a Qualified Person for the purposes of NI 43-101.
- I am responsible for the preparation of selected items under Items 1.12, 18.4, 25.6, 26.7 and 26.8 of the Technical Report relating to geology and Mineral Resource estimation, as well as relevant parts in the Executive Summary, Reliance on Other Experts, Conclusions and Recommendations, Risks and Opportunities, References and Date and Signature of the Technical Report, and I accept professional responsibility for those sections of the Technical Report.
- I am independent (as defined by Section 1.5 of NI 43-101) of Dundee Precious Metals Inc and Adriatic Metals Plc. I have not had prior involvement with the property that is the subject of the Technical Report.
- I visited site on 25 to 26 March 2025.
- I have read NI 43-101 and Form 43-101F1 and the Technical Report has been prepared in compliance with that instrument and form.
- As of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed and to make the Technical Report not misleading.

Signed and dated on 9 June 2025 in Cardiff, United Kingdom.

Richard Martindale

Certificate of Colin Chapman

SRK Consulting (UK) Ltd
5th Floor Churchill House, 17 Churchill Way, Cardiff CF10 2HH, Wales, United Kingdom
cochapman@srk.co.uk

I, Colin Chapman, do hereby certify that:

- I am currently employed as a consulting engineer to the mining and mineral exploration industry, as a Principal Consultant (Mining Infrastructure and Logistics) with SRK Consulting (UK) Ltd, with an office address of 5th Floor Churchill House, 17 Churchill Way, Cardiff, CF10 2HH, UK.
- This certificate applies to the technical report entitled “Amended and Restated NI 43-101 Technical Report on the Vareš Mine, Bosnia” with a report date of 9 June 2025 and an effective date of 1 April 2025 (the “Technical Report”).
- I am a Professional Engineer registered with the Institute of Materials, Minerals & Mining, UK (#460270). I graduated with a Master’s Degree in Applied Environmental Geology from Cardiff University, UK in 2007. I was directly involved in mining operations and exploration prior to my Master’s Degree. Since my master’s degree, I’ve practiced my profession for 18 years with my career focused on civil engineering, geotechnical engineering, and mining project (infrastructure and logistics) related consulting services worldwide. I have been directly involved in technical review and audit, due diligence, and providing various technical services for many base metal, precious metal, bulk commodity and specialist and industrial mineral mines / projects;
- I have read the definition of Qualified Person as set out in National Instrument 43-101 – Standards of Disclosure for Mineral Projects (“NI 43-101”) and certify that, by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I am a Qualified Person for the purposes of NI 43-101.
- I am responsible for the preparation of selected items under Items 1.13, 18 other than 18.4 and 18.5, and further responsible for the preparation 25.8 and 26.10 of the Technical Report relating to surface infrastructure and logistics in the role of independent reviewer of the Project, as well as relevant parts in the Executive Summary, Conclusions and Recommendations, Risks and Opportunities, and I accept professional responsibility for those sections of the Technical Report.
- I am independent (as defined by Section 1.5 of NI 43-101) of Dundee Precious Metals Inc and Adriatic Metals Plc.
- I have not had prior involvement with the property that is the subject of the Technical Report.
- I have not visited the Vareš site.
- I have read NI 43-101 and Form 43-101F1 and the Technical Report has been prepared in compliance with that instrument and form.
- As of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed and to make the Technical Report not misleading.

Signed and dated on 9 June 2025 in Cardiff, United Kingdom.

Colin Chapman

Certificate of Sabine Anderson

SRK Consulting (UK) Ltd
5th Floor Churchill House, 17 Churchill Way, Cardiff CF10 2HH, Wales, United Kingdom
sanderson@srk.co.uk

I, Sabine Anderson, do hereby certify that:

- I am Principal Consultant (Mining Due Diligence), employed by SRK Consulting (UK) Ltd since 2013, and between 2005 and 2011.
- This certificate applies to the technical report entitled "Amended and Restated NI 43-101 Technical Report on the Vareš Mine, Bosnia" with a report date of 9 June 2025 and an effective date of 1 April 2025 (the "Technical Report").
- I am a professional mining engineer having graduated with a Masters in Engineering degree in 1995 in Mining from the Royal School of Mines, Imperial College, London. I have worked on metalliferous underground mines in South Africa, opencast coal mines in Australia, and a tantalite mine in Namibia. Since working for SRK Consulting (UK) Ltd, I have been mostly involved in financial modelling and economic evaluation, managing technical reviews and compiling associated technical reports for M&A, listings, project finance. I have managed a number of scoping through to feasibility studies for various global projects.
- I am a member of the Institute of Materials, Minerals & Mining, member number 0454436. In membership of the IMMM, I have been registered with the Engineering Council as a Chartered Engineer, registration number 584131.
- I have read the definition of Qualified Person as set out in National Instrument 43-101 – Standards of Disclosure for Mineral Projects ("NI 43-101") and certify that, by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I am a Qualified Person for the purposes of NI 43-101.
- I am responsible for the preparation of Items 1.1 – 1.3, 1.9, 1.15 – 1.18, 2 – 6, 12 – 24, 25.1, 25.8 – 25.14, 26.4, 26.11, 26.12 and 27of the Technical Report. I accept professional responsibility for those sections of the Technical Report. I have been the project manager of the review and preparation of the Technical Report.
- I am independent (as defined by Section 1.5 of NI 43-101) of Dundee Precious Metals Inc and Adriatic Metals Plc. I have not had prior involvement with the property that is the subject of the Technical Report.
- I have not visited the Vareš site.
- I have read NI 43-101 and Form 43-101F1 and the Technical Report has been prepared in compliance with that instrument and form.
- As of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed and to make the Technical Report not misleading.

Signed and dated on 9 June 2025 in Cardiff, United Kingdom.

Sabine Anderson

ABBREVIATIONS

ABA	Acid-Base Accounting
ADT	Adriatic Metals Plc
AGL	Avoca Geotech Ltd.
AMC	AMC Consultants Pty Ltd
ARD	Acid Rock Drainage
CAF	Cemented Aggregate Fill
CIM	Canadian Institute of Mining, Metallurgy and Petroleum
DFS	The Ausenco Definitive Feasibility Study
EIA	Environmental Impact Assessment
ESAP	Environmental and Social Action Plan
ESIA	Environmental Social Impact Assessment
FoS	Factor of Safety
FW	Foot Wall
GISTM	Global Industry Standard on Tailings Management
HW	Hanging Wall
IESC	Independent Environmental and Social Consultant
JORC	Joint Ore Reserves Committee
LCT	Locked Cycle Tests
LLHOS	Longitudinal Long Hole Stoping
LoM	Life of Mine
M	Dundee Precious Metals Inc
MCAF	Mechanised Cut and Fill
MRE	Mineral Resource Estimation
MRR	Massive Red Rock
NAG	Net Acid Generation
NAG	Non-Acid-Generating
NAP	Net Acid Production
NSR	Net Smelter Return
P&C	Paterson & Cooke (UK) Ltd
PAF	Paste Aggregate Fill
PAG	Potentially-Acid-Generating
PF	Paste Fill
PFS	Pre-Feasibility Study
QAQC	Quality Assurance Quality Control
QP	Qualified Person
RJB	Rupice-Juraševac-Brestic
RNW	Rupice North West
RoM	Run-of-Mine
RQD	Rock Quality Designation
RUP	Rupice Main
SPLP	Synthetic Precipitation Leaching Procedure
TCLP	Toxicity Characteristic Leaching Procedure
TEM	Technical Economic Model
TLHOS	Transverse Long Hole Open Stoping
TSF	Tailings Storage Facility
UCS	Uni-axial Compressive Strength
URSP	Uphole Recovery of Sill Pillars
USD	United States Dollar
VPP	Vareš Processing Plant
WAI	Wardell Armstrong International
WRD	Waste Rock Dump